

ANNEXE D

Rapport de l'étude géotechnique

Saint-Rémi, June 11, 2010

O/F : G1-09-1532

Mr. John Olson
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Object: **Geotechnical study – Construction of wind energy converters**
Terrains located in the vicinity of the town of Saint-Valentin, Quebec.

Dear Sir,

Following your agreement to our proposal PG1-09-1529-4 dated on April 29, 2010, we herewith transmit to you the geotechnical report of study carried out by our firm for the project quoted in title.

We hope that it will be to your full satisfaction and we thank you for allowing us to take part in the realization of your project.

Do not hesitate to contact us for all additional questions concerning the present study.

Sincerely yours,

Groupe ABS inc.

Ursula Maselbas, Eng., M.A.Sc.
Team leader, geotechnical

Enc. Reports (1 original and 1 copy)

**GEOTECHNICAL STUDY
CONSTRUCTION OF WIND
ENERGY CONVERTERS**
Terrains located in the vicinity of the town
of St-Valentin in Quebec

O/F : G1-09-1532
June 11, 2010

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1. INTRODUCTION

GROUPE ABS INC. services were retained by the company *TRANSALTA CORPORATION* (*hereinafter called client*) to conduct a geotechnical subsoil investigation for 31 proposed wind energy converters to be located in the vicinity of the town of Saint-Valentin, about 50 km south of Montreal in Quebec.

This geotechnical study was performed according to our professional proposal dated April 29, 2010 (PG1-09-1529-04).

The subject properties are located within a 5 km radius from the town of St-Valentin. They are located in an agricultural land with flat topography. Satellite photos showing the configuration of each site are attached in appendix A.

Throughout this report, sites are classified in five (5) groups according to their geographical location (refer to Key-Plan in appendix B of this report):

- Group M includes sites 4, 6, 11, 12 and 14 (5 sites)
- Group N includes sites 8 and 13 (2 sites)
- Group O includes sites 25, 27, 28, 28A, 31 and 31A (6 sites)
- Group P includes sites 5, 7, 9, 10, 16, 17, 18, 20, 21, 22, 23 and 37 (12 sites)
- Group Q includes sites 26, 29, 30, 32, 34 and 35 (6 sites)

A Google satellite photos are enclosed in appendix A. The drilling borehole locations are shown in the plan enclosed in appendix B, the borehole logs are attached in appendix C, the geophysical investigation report is attached in appendix D and the results of the laboratory tests are included in appendix E. Photography of rock cores is presented in appendix F. Finally, miscellaneous documents are attached in appendix G.

2. SCOPE OF THE INVESTIGATION

This geotechnical investigation is primarily aimed at determining the profile and the quality of the subsoil strata as well as the ground water condition by means of boreholes and geophysical methods. The methodology used on-site and in laboratory has allowed the verification of subsoil conditions for the subject sites and the formulation of general recommendations for the project, namely:

- The nature of subsurface materials and their stratigraphic sequence;
- The groundwater level;
- The competent soil/rock starts to receive the anticipated loads;
- Bearing capacity of shallow and deep foundation;
- Soils geotechnical properties;
- Slope stability for temporary excavation;
- General recommendations.

3. FIELD EXPLORATION PROCEDURES

3.1 Fieldwork

As per our professional proposal, the subsoil investigation included two parts: the first part, which is the main one, consisted of drilling boreholes from which disturbed soil and rock samples were retrieved following standard procedures in conjunction with the American Society for Testing and Materials standards (ASTM). The second part of the investigation, the complementary part, consisted in carrying out geophysical surveying for the subject sites.

3.1.1. Boreholes

The first part of the investigation program consisted of drilling a total of thirty-one (31) boreholes (one borehole for each site) advanced to a competent soil or the bedrock. The boreholes are named after their respective site numbers (ex. Borehole 10BH-04 represents site 4 and so forth). The field exploration program was carried out between March 08, 2010 and April 26, 2010 under the constant supervision of our geotechnical personnel and in the presence of the client's representatives.

The boreholes were drilled by means of a track-mounted rotary drill rig, property of the subcontractor, *Explora-Sol Inc.* Soil samples were recovered using a 50 mm OD (outside diameter) split-spoon sampler in conjunction with ASTM D-1586 standard penetration test. This test consists of driving the standard sampler into the soil using a 63.5 kg hammer dropped from a height of 76 cm. The number of blows for each 30 centimetres of penetration named "SPT - N Value" can be correlated to the relative density of the sampled soil.

In the majority of boreholes, the bedrock was cored using a NQ tube core barrel. The length of cored rocks is ± 3 m. In addition, in-situ vane shear test was conducted where clayey soil was encountered.

An observation well was installed on each borehole in order to monitor the groundwater conditions.

3.1.2. Geophysical exploration

The geophysical exploration method used in this project is a seismic method called the Multi-Channel Analysis of surface Waves (MASW). The seismic exploration was carried out by our subcontractor *Geophysics GPR International inc* (*hereinafter called GPR*). Site works were conducted between March 15 and 27, 2010 and on June 2nd, 2010. A detailed description of this method is included in section 3 of the report entitled " Shear wave velocity sounding results – Wind energy converters project, Saint-Valentin, Quebec" produced by GPR (report no. M09789 dated June 2010 – copy attached in appendix E of this report).

3.2 field survey

The locations of boreholes were determined by the client. During the field investigation work, the borehole locations were identified by a pre-installed wooden stick on which the name of the site was written. All borehole locations were confirmed by the client's representative before the undertaking of the drilling works. The geodesic coordination of boreholes were furnished by the client and they are presented in table 1.

Table 1 : geodesic coordinates

Borehole	Longitude X	Latitude Y	Elevation (m)
Group M			
10BH-04	316203	4994292	41.00
10BH-06	316202	4994943	42.00
10BH-11	316592	4994528	43.00
10BH-12	316596	4994055	42.13
10BH-14	316620	4994936	44.00
Group N			
10BH-08	316248	4998369	51.00
10BH-13	316618	4998175	47.92
Group O			
10BH-25	319312	4997246	38.00
10BH-27	319664	4996999	35.00
10BH-28	319665	4997492	35.00
10BH-28A	319414	4997499	-
10BH-31	320095	4997479	34.00
10BH-31A	319926	4997484	-
Group P			
10BH-05	316239	5001777	50.00
10BH-07	316244	5002438	49.00
10BH-09	316478	5001418	50.00
10BH-10	316497	5002120	
10BH-16	316876	5001955	51.00
10BH-17	317102	5001353	50.00
10BH-18	317273	5002650	50.00
10BH-20	317482	5002277	49.00
10BH-21	318008	5002258	48.00
10BH-22	318187	5001293	46.00
10BH-23	318195	5001745	47.00
10BH-37	318483	5001515	-
Group Q			
10BH-26	319774	5001316	40.84
10BH-29	319828	5002096	45.00
10BH-30	320091	5001646	41.00
10BH-32	320241	5002214	43.00
10BH-34	319415	5002922	-
10BH-35	319169	5002673	-

3.3 Laboratory testing

All samples collected during the fieldwork were transported to our laboratory for the purpose of analysis, identification and classification. They all made the subject of a careful visual inspection by a geotechnical engineer. Grain-size distribution analysis, limits of consistency and natural water content determinations as well as unconfined compression strength of rock were performed on selected representative samples. The results of these tests are presented in detail in appendix D.

All samples taken during fieldworks and on which no laboratory tests were performed will be preserved for a period of six (6) months as from the date of this report, afterward; they will be discarded unless otherwise stated.

4. SOIL PROFILE AND PROPERTIES

The soil profile determined by boring is shown in table 2 presented hereinafter. A brief description of soil profile at each group is included in the following subsection 5.1 to 5.4. For detailed description, refer to borehole loges enclosed in appendix C.

Table 2: Soil / Rock Profile

Borehole	Top soil / fill	sand	Cohesive soil	Till	Bedrock
Group M					
10BH-04	-	-	0.00-4.72	4.72-11.53	11.53-14.99
10BH-06	-	0.00-0.71	0.71-3.35	3.35-12.39	12.39-15.80
10BH-11	-	-	0.00-2.44	2.44-12.47	12.47-15.62
10BH-12	0.00-0.61	-	0.61-3.05	3.05-14.43	14.43-17.83
10BH-14	0.00-1.52	1.52-12.80	-	-	12.80-16.10
Group N					
10BH-08	0.00-0.46	-	-	0.46-22.56	-
10BH-13	0.00-0.61	-	-	0.61-30.48	-
Group O					
10BH-25	0.00-0.61	-	0.61-4.72	4.72-7.59	7.59-11.15
10BH-27	0.00-0.10	-	0.10-4.77	4.77-10.52	10.52-14.15
10BH-28	0.00-0.15	-	0.15-5.33	5.33-10.67	10.67-13.72
10BH-28A	0.00-0.13	-	0.13-4.93	4.93-11.91	11.91-15.22
10BH-31	0.00-0.18	-	0.18-5.18	5.18-11.66	11.66-15.04
10BH-31A	0.00-0.15	-	0.15-2.90	2.90-12.60	12.60-15.57

Borehole	Top soil / fill	sand	Cohesive soil	Till	Bedrock
Group P					
10BH-05	0.00-1.52	-	-	1.52-7.62	7.62-10.82
10BH-07	0.00-0.20	-	-	0.20-11.07	11.07-15.24
10BH-09	0.00-0.61	-	-	0.61-7.01	7.01-10.85
10BH-10	0.00-0.61	-	-	0.61-20.88	-
10BH-16	0.00-1.52	-	-	1.52-8.91	8.91-12.09
10BH-17	0.00-0.74	-	0.74-3.35	3.35-19.94	-
10BH-18	0.00-0.20	-	-	0.20-6.05	6.05-9.58
10BH-20	0.00-1.83	-	-	1.83-20.17	-
10BH-21	0.00-0.51	0.51-0.86	0.86-1.83	1.83-11.18	11.18-14.33
10BH-22	0.00-0.25	-	-	0.25-12.95	12.95-16.26
10BH-23	0.00-0.10	-	-	0.10-10.72	10.72-13.72
10BH-37	0.00-0.10	-	-	0.10-7.77	7.77-10.52
Group Q					
10BH-26	0.00-0.61	-	-	0.61-5.41	5.41-8.53
10BH-29	0.00-1.17	-	-	1.17-4.04	4.04-6.71
10BH-30	0.00-0.61	-	-	0.61-6.48	6.48-13.23
10BH-32	0.00-0.61	-	-	0.61-6.40	6.40-9.53
10BH-34	0.00-0.18	-	-	0.18-5.08	5.08-9.73
10BH-35	0.00-0.25	-	-	0.25-10.85	10.85-14.17

Note: depths are described in meter and "0.00" indicates ground surface.

4.1 Group M (sites 4, 6, 11, 12, 14)

The soil profile underlying all sites in this group, except site 14, consists of a 3 to 5 m thick clayey soil underlain by a 7 to 10 m thick till deposit followed by the bedrock. In the site 14, the soil profile is composed mainly by a 12 m thick sand deposit followed by the bedrock. In sites 12 and 14 a fill layer or a remoulded native soil is found on the surface.

The clay layer is characterized by the presence of a thin firm grey to brown clayey silt (types CL or ML) followed by a soft grey clay of high plasticity (type CH).

The natural water content measured in soft clay varies between 56 to 74%, the liquid limit ranges from 52 to 65% and the plastic limit varies from 17 to 26%. The in-situ un-drained shear strength varies between 19 and 31 kPa.

The till deposit is composed of silty and sandy soils (type ML and SM), becoming gravelly (type SP) in the last 3 to 5 m before the bedrock. The natural water content varies between 6 (for gravelly soil) and 19% (for silty soil). The obtained SPT N values imply that the density of this deposit is compact (ML and SM) to dense (SP).

The sand deposit found at site 14 consist of a dense sand (SP) becoming gravel and sand (GP) at about 8m deep.

The bedrock consists of grey limestone. The recovery values (recovered rock / core length) vary between 86 and 100% and the RQD values range from 37% (borehole 11) and 100%. The unconfined compressive strength of rock varies between 90 and 117 MPa (106 MPa in average). Based on these results the quality of the bedrock ranges from good to excellent. At borehole 10BH-014 the rock is fractured at surface.

4.2 Group M (sites 8, 13)

The soil profile in this group consists primarily of top soil underlain by a sandy silty till deposit (SM and ML). At about 18 to 20 m deep the till deposit is composed of boulders. The two boreholes were terminated in the till deposit. The density of the first 18 to 20 m of this deposit could be qualified as loose to dense.

4.3 Group O (sites 25, 27, 28, 28A, 31, 31A)

The soil profile at these sites consists of top soil underlain by ± 5 m thick clayey soil underlain by a ± 6 m thick till deposit followed by the bedrock.

The clay layer is composed of a thin stiff grey to brown silty clay (ML-CL) crust followed by a firm grey clay of high plasticity (type CH). The natural water content measured in soft clay varies between 30 to 58%, the liquid limit ranges from 49 to 59% and the plastic limit varies from 15 to 29%. The in-situ un-drained shear strength varies between 22 and 75 kPa.

The till deposit is composed mainly of sand and silt (type ML and SM), becoming gravelly (type SP or GP) with cobbles and boulders in some boreholes. The natural water content varies between 7 to 15%. The density of the till deposit can be qualified as compact to dense.

The bedrock consists of grey to black limestone. The recovery values vary between 69 and 100% and the RQD values range from 13% (borehole 28) and 100%. The unconfined compressive strength of rock varies between 80 and 109 MPa (96 MPa in average). In general, the quality of the bedrock ranges from fair to excellent. At borehole 10BH-28 the rock is fractured through the entire recovered core.

4.4 Group P (sites 5, 7, 9, 10, 16, 17, 18, 20, 21, 22, 23, 37)

The soil profile at the majority of these sites is composed of 6 to 12 m thick till deposit followed by the bedrock. At sites 10, 17 and 20 the boreholes were terminated in the till deposit at about 20 m deep. At sites 17 and 21 the till deposit was overlain by a thin clayey soil layer. In all boreholes top soil/fill layer are topping the soil profile.

The till deposit consists mainly of sand and silt (type ML and SM), becoming gravelly (type SP or GP) with cobbles and boulders in some boreholes. The natural water content of this deposit is $\pm 10\%$. The density of the till deposit can be qualified as loose to dense.

The bedrock consists of grey to black limestone and shale. The recovery values vary between 41 and 100% and the RQD values range from 20% (borehole 5) and 95%. The unconfined compressive strength of rock varies between 68 and 165 MPa (71 MPa in average). In general, the quality of the bedrock ranges from fair to excellent.

4.5 Group Q (sites 26, 29, 30, 32, 34, 35)

The soil profile at the majority of these sites consists of a till deposit followed by the bedrock. At sites 35 the thickness of till deposit is about 10m while in the remaining sites of this group its thickness is about 5m. In all boreholes top soil/fill layer are topping the soil profile.

The till deposit consists mainly of sand and silt (type ML and SM), becoming gravelly with cobbles and boulders in some boreholes. The natural water content of this deposit is $\pm 10\%$. The density of the till deposit can be qualified as compact to dense.

The bedrock consists of black limestone and shale. The recovery values vary between 0 and 100% and the RQD values range from 0% (borehole 30) and 100%. The unconfined compressive strength of rock varies between 75 and 85 MPa (79 MPa in average). In general, in all boreholes except 10BH-30, the quality of the bedrock ranges from fair to excellent. At site 30 the rock was fractured through the entire recovered core.

5. GROUNDWATER OBSERVATION

The following table resumes the groundwater levels measured in boreholes.

Table 3 : Summary of groundwater level

Borehole	Depth (m)	Elevation (m)	Recording date
Group M			
10BH-04	0.00	41.00	April 12, 2010
10BH-06	1.32	40.68	April 12, 2010
10BH-11	0.74	42.26	April 12, 2010
10BH-12	1.00	41.13	April 12, 2010
10BH-14	1.13	42.87	April 12, 2010
Group N			
10BH-08	5.35	45.65	May 6, 2010

Borehole	Depth (m)	Elevation (m)	Recording date
10BH-13	2.55	45.37	May 6, 2010
Group O			
10BH-25	0.92	37.08	April 26, 2010
10BH-27	1.28	33.72	April 26, 2010
10BH-28	0.87	34.13	April 26, 2010
10BH-28A	1.30	-	April 26, 2010
10BH-31	0.26	33.74	April 26, 2010
10BH-31A	0.78	-	April 26, 2010
Group P			
10BH-05	0.00	50.00	April 26, 2010
10BH-07	0.30	48.70	April 26, 2010
10BH-09	0.60	49.40	April 26, 2010
10BH-10	0.00	50.00	April 26, 2010
10BH-16	1.45	49.55	April 26, 2010
10BH-17	0.75	49.25	April 26, 2010
10BH-18	0.00	50.00	April 26, 2010
10BH-20	0.00	49.00	April 26, 2010
10BH-21	0.51	47.49	April 26, 2010
10BH-22	0.80	45.20	April 26, 2010
10BH-23	0.25	46.75	April 26, 2010
10BH-37	0.68	-	April 26, 2010
Group Q			
10BH-26	2.46	38.38	April 26, 2010
10BH-29	1.00	44.00	April 26, 2010
10BH-30	1.65	39.35	April 26, 2010
10BH-32	1.57	41.43	April 26, 2010
10BH-34	0.72	-	April 26, 2010
10BH-35	0.64	-	April 26, 2010

The groundwater conditions depend on different factors, such as seasonal fluctuations, precipitations and modifications made to the physical environment. Therefore, during the excavation works, water inflow could be encountered at levels different from those mentioned in table 3.

6. CONCLUSIONS AND RECOMMANDATIONS

6.1 General comments

It is our understanding that the project includes the construction of 31 energy wind converters. According to the foundation data sheets furnished by the client (copy attached in appendix G), a ring footing is to be used to transmit the converter's loads onto soil mass. The minimum required soil bearing pressure is 242 kPa for a ring foundation of 16.8 m in diameter with buoyancy, and 412 kPa for a ring foundation of 14.2 m in diameter without buoyancy. The differential settlement should not exceed 40 mm.

The depth of groundwater level measured in the majority of boreholes ranges from 0.0 to 2.5 m. These measurement were conducted at spring time (April and May 2010) where the water table is on its highest level (snow melting, precipitation) therefore, it is possible that the water level will drop beneath the footing base (2.85 m according to data sheets) during dry seasons. As a result, the "without buoyancy" load case is considered in the shallow foundation design.

In general, the seismic investigation carried out on the subject sites (MASW tests) yields the same results as the conventional borehole investigation.

Based upon the information gathered from boreholes and seismic investigations, the geotechnical recommendations for the proposed construction are presented in the following sections.

6.2 Foundation design

Based on the geotechnical properties of soil and rock underlying the proposed constructions, the depth of the competent soil is determined for each site. The depth of the competent soil is defined as the depth, measured from the ground surface, at which the anticipated pressure (412 kPa) can be transferred to the soil mass/rock without causing a shear failure in the soil mass or/and excessive settlement caused by static or dynamic loads (<40 mm). A factor of safety of 3 (FS = 3) is considered against shear failure. The type of foundation (shallow or deep) is determined based on the depth of the competent strata.

Table 4 : Depth of competent soil and type of foundation

Site	Competent soil / rock		Foundation type
	Type	Depth (m)	
Group M			
4	Bedrock	±13	Deep foundation
6	Bedrock	±13	Deep foundation
11	Bedrock	±13	Deep foundation
12	Bedrock	±15	Deep foundation
14	Bedrock	±13	Deep foundation
Group N			
8	Till deposit	±17	Deep foundation
13	Till deposit	±17	Deep foundation

Site	Competent soil / rock		Foundation type
	Type	Depth (m)	
Group O			
25	Bedrock	±8	Deep foundation
27	Bedrock	±11	Deep foundation
28	Bedrock	±11	Deep foundation
28a	Bedrock	±12	Deep foundation
31	Bedrock	±12	Deep foundation
31a	Bedrock	±13	Deep foundation
Group P			
5	Bedrock	±10	Deep foundation
7	Bedrock	±13	Deep foundation
9	Bedrock	±8	Deep foundation
10	Till deposit	±12	Deep foundation
16	Bedrock	±12	Deep foundation
17	Till deposit	±10	Deep foundation
18	Till deposit	±5	Shallow foundation
20	Till deposit	±15	Deep foundation
21	Bedrock	±11	Deep foundation
22	Bedrock	±13	Deep foundation
23	Till deposit	±5	Shallow foundation
37	Till deposit	±5	Shallow foundation
Group Q			
26	Bedrock	±5	Shallow foundation
29	Till deposit	±3	Shallow foundation
30	Till deposit	±3	Shallow foundation
32	Till deposit	±5	Shallow foundation
34	Bedrock	±5	Shallow foundation
35	Bedrock	±12	Deep foundation

6.2.1 Shallow foundation

All compressible soils (CH or CL), organic soil and fill must be removed from within the footprints of proposed footings. The foundations must be placed under a minimum of 1.5 m earth cover in order to be adequately protected against frost effects.

For some sites the depth of competent soil/rock is located at about 5m. For these sites, it is possible to elevate the competent soil surface level to the desired elevation.

This should be carried out using a well graded granular materials complying with the grain size distribution given in table 5, compacted to 98% of Standard Proctor maximum dry density and placed in 300 mm lift thickness.

Table 5 : Grain size distribution

Grain size (mm)	% passing
31.5	100
20	90 -100
14	68 - 93
5	35 – 60
1.25	19 – 38
0.315	9 – 17
0.080	2 – 7

6.2.2 Deep foundation

As illustrated in table 5, twenty-three (23) out of thirty-one (31) wind energy converters are to be supported by a deep foundation system. Based on the geotechnical properties of subsoil encountered at these sites, driven steel H-piles end-bearing on the surface of good quality bedrock or into a very dense till deposit could be used for this purpose. A cast steel drive shoes should be used to protect the toe of pile when driving through boulders.

For sites where piles are to be driven to bedrock. The ultimate axial capacity of bedrock is estimated at 5000 kPa. The estimated capacity includes a factor of safety of 3. The settlement for pile driven into sound bedrock is normally negligible providing that the contact between pile toe and rock is assured.

For sites 8, 13, 10, 17 and 20 the anticipated load will be transferred by means of end-bearing piles driven into the till deposit. The values of estimated ultimate axial capacity of till deposit at the piles toe level is shown in table 6.

Table 6 : Allowable bearing capacity of pile toe end-bearing on till deposit

Site	Estimated depth of competent soil (till deposit)	Allowable bearing pressure of pile toe (kPa)
8	±17	3000
13	±17	3000
10	±12	2000
17	±10	1750
20	±15	2600

The toe of pile should be driven at least six (6) times its diameter into the competent soil in order to mobilize the full axial end-bearing capacity mentioned in the table 6. The estimated capacity includes a factor of safety of 3.

The lateral capacity of piles can be determined using Broms' method. This method is presented in section 18.4.1 of the Canadian Foundation Engineering Manual. The Broms' method estimates the ultimate lateral resistance of piles using graphical charts (copies are enclosed in appendix G). The soil parameters mentioned in tables 8 to 12 could be used for this matter. A reduction factor should be applied for pile group.

Table 7 : Reduction factor for lateral resistance

Pile spacing (center to center)	Reduction factor
8b	1,0
6b	0,8
4b	0,5
3b	0,4

b = pile diameter

The ultimate loads capacity of piles must be verified by means of static and dynamic load tests as per ASTM procedures.

6.3 soils geotechnical properties

The geotechnical properties for subsoil underlying the subject sites are determined based on the information obtained from boreholes and seismic investigations. They are presented in the following tables.

Table 8 : Soil properties – Group M (Sites 4, 6, 11, 12 and 14)

Parameter/soil	Clay	Till	Sand
Total unit weight γ (kN/m ³)	18	18	18
Submerged unit weight γ' (kN/m ³)	8	8	8
Effective friction angle ϕ' (°)	25	28	30
Effective cohesion C' (kPa)	5	0	0
Un-drained shear strength C_u (kPa)	See logs	0	0
Poisson's ratio ν	0.35	0.25	0.25
Elastic stiffness modulus E (MPa)	10	15	20
Shear modulus G (MPa)	3.7	6	8

Table 9 : Soil properties – Group N (Sites 8 and 13)

Parameter/soil	Clay	Till From 0 to 17m	Till >17m
Total unit weight γ (kN/m ³)	-	18	20
Submerged unit weight γ' (kN/m ³)	-	8	10
Effective friction angle ϕ' (°)	-	28	34
Effective cohesion C' (kPa)	-	0	0
Un-drained shear strength C_u (kPa)	-	0	0
Poisson's ratio ν	-	0.25	0.25
Elastic stiffness modulus E (MPa)	-	15	100
Shear modulus G (MPa)	-	6	40

Table 10 : Soil properties – Group O (Sites 25, 27, 28, 28A, 31 and 31A)

Parameter/soil	Clay	Till	Sand
Total unit weight γ (kN/m ³)	18	18	
Submerged unit weight γ' (kN/m ³)	8	8	-
Effective friction angle ϕ' (°)	25	30	-
Effective cohesion C' (kPa)	5	0	-
Un-drained shear strength C_u (kPa)	See logs	0	-
Poisson's ratio ν	0.35	0.25	-
Elastic stiffness modulus E (MPa)	10	35	-
Shear modulus G (MPa)	3.7	14	-

Table 11: Soil properties – Group P (Sites 5, 7, 9, 10, 16, 17, 18, 20, 21, 22, 23 and 37)

Parameter/soil	Clay	Till From 0 to ±5 m	Till >5m
Total unit weight γ (kN/m ³)	18	18	18
Submerged unit weight γ' (kN/m ³)	8	8	8
Effective friction angle ϕ' (°)	25	28	32
Effective cohesion C' (kPa)	5	0	0

Parameter/soil	Clay	Till From 0 to ±5 m	Till >5m
Un-drained shear strength C_u (kPa)	See logs	0	0
Poisson's ratio ν	0.35	0.25	0.25
Elastic stiffness modulus E (MPa)	10	15	40
Shear modulus G (MPa)	3.7	6	16

Table 12 : Soil properties – Group Q (Sites 26, 29, 30, 32, 34 and 35)

Parameter/soil	Clay	Till	Sand
Total unit weight γ (kN/m³)	-	18	-
Submerged unit weight γ' (kN/m³)	-	8	-
Effective friction angle ϕ' (°)	-	32	-
Effective cohesion C' (kPa)	-	0	-
Un-drained shear strength C_u (kPa)	-	0	-
Poisson's ratio ν	-	0.25	-
Elastic stiffness modulus E (MPa)	-	40	-
Shear modulus G (MPa)	-	16	-

6.4 Temporary excavation and drainage

According to the stratigraphy identified in the boreholes carried out at subject sites, for an excavation of about 3 to 5 m in depth, the excavation will take place mainly in the soft clay layer or the loose to compact till or sand layers. Therefore, temporary slopes must be shaped with inclinations of 1.0 vertically to 3.0 horizontally (1V : 3H) or flatter, depending on density and/or consistency of materials to be encountered.

Moreover, based on measured water level (see table 3) groundwater will seep into the excavations. In addition, the bottom and slopes of excavation in the majority of subject sites is composed of a loose saturated fine silty soil. This type of soil is very sensitive against remoulding and it could lose significant amount of its strength if remoulded. Therefore, in order to maintain a stable bottom and slope of the excavation, water level must be lowered to at least **0.60 m** below the bottom of excavation grade. The contractor must consider the use of a proper pumping system in order to eliminate the surface and seepage water to avoid its accumulation at the bottom of excavation; allowing working in a dry environment.

It is very important to underline that the contractor is **solely responsible** for the design of such pumping system that is capable of maintaining a dry bottom excavation as described in the aforementioned paragraph.

6.5 site classification for seismic site response

Based on the seismic investigation carried at the subject sites (see appendix E), the majority of sites is classified as class C. The following table summarises sites classes.

Table 13 : Site classification for seismic site response

Sites	Class
29, 30, 32, 34 and 37	B
All remaining sites	C
6	D

7. LIMITATIONS OF THE STUDY

Soil description and properties presented in the preceding sections and boreholes log reports, are valid only where the boreholes were performed. Therefore, it is very possible that soil found during execution of work may vary from those studied; any notable variation or discrepancy between descriptions provided in this report and those found must be reported to Groupe ABS Inc. promptly.

Prepared by : Ibrahim Ja'far, Eng., M.Eng.

Verified by: Ursula Maselbas, Eng., M.A.Sc.

IJ/UM//sm

Appendix A

Google satellite photos

TRANSALTA CORPORATION

Geotechnical study – Construction of wind energy converters

Terrains located in the vicinity of the town of St-Valentin in Quebec

O/F : G1-09-1532



© 2010 Google

Figure 1 : Satellite photo – Group M

TRANSALTA CORPORATION

Geotechnical study – Construction of wind energy converters

Terrains located in the vicinity of the town of St-Valentin in Quebec

O/F : G1-09-1532



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Figure 1 : Satellite photo – Group N

TRANSALTA CORPORATION

Geotechnical study – Construction of wind energy converters

Terrains located in the vicinity of the town of St-Valentin in Quebec

O/F : G1-09-1532



© 2010 Google

Figure 1 : Satellite photo – Group O

TRANSALTA CORPORATION

Geotechnical study – Construction of wind energy converters

Terrains located in the vicinity of the town of St-Valentin in Quebec

O/F : G1-09-1532



© 2010 Google

Figure 1 : Satellite photo – Group P

TRANSALTA CORPORATION

Geotechnical study – Construction of wind energy converters

Terrains located in the vicinity of the town of St-Valentin in Quebec

O/F : G1-09-1532



© 2010 Google

Figure 1 : Satellite photo – Group Q

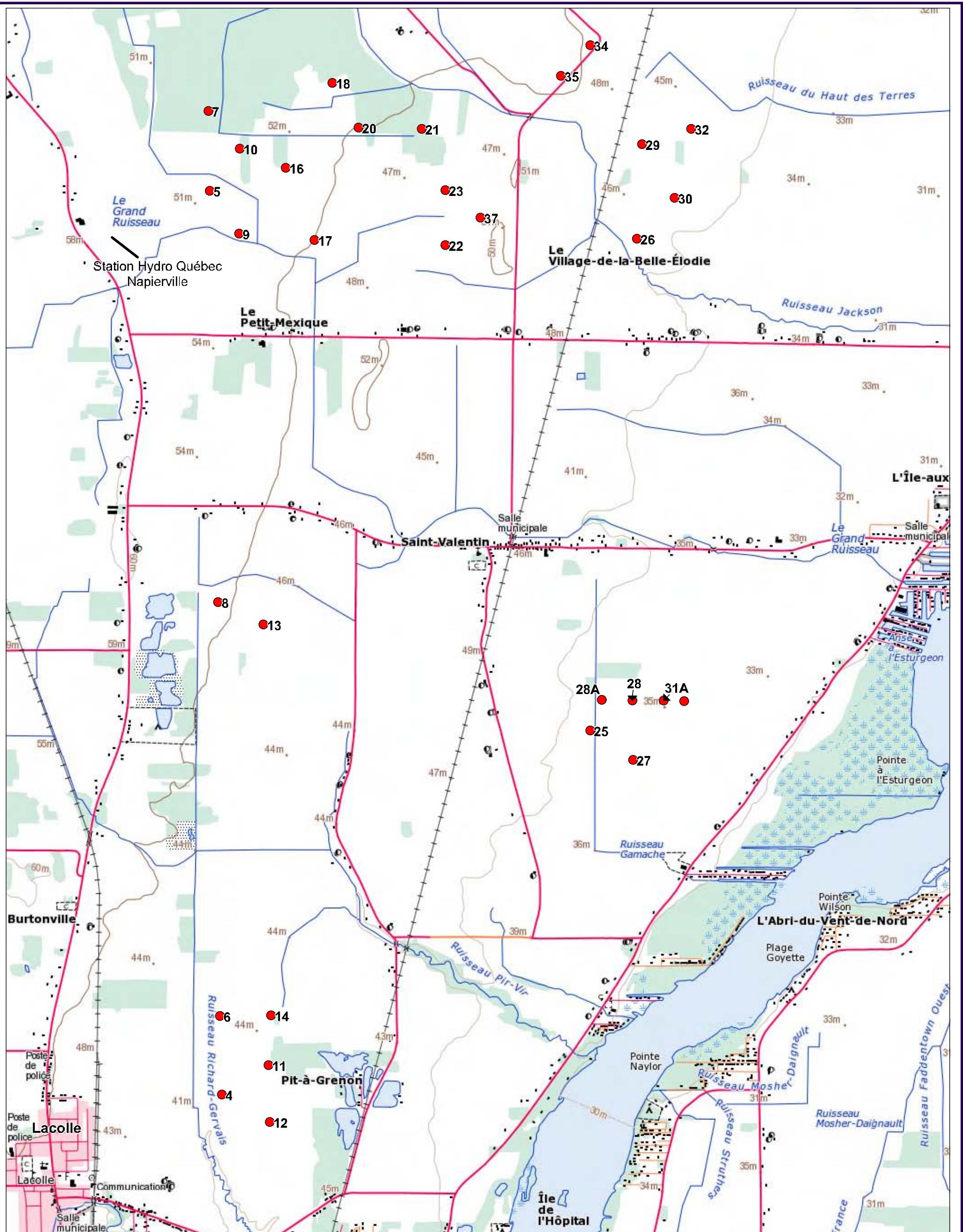
TRANSALTA CORPORATION

Geotechnical study – Construction of wind energy converters
Terrains located in the vicinity of the town of St-Valentin in Quebec

June 11, 2010
O/F : G1-09-1532

Appendix B

Key-Plan



VENTERRE

Parc Éolien Saint-Valentin
Québec
MRC Haut-Richelieu

Geo Technical Study

Légende

● Drill locations



Échelle:
1:40 000
(sur 11 x 17)

UTM NAD 83 Zone 18
STV_M136_CPK 14/06/2010

Appendix C

Borehole logs

Borehole N°
10BH-07

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **316244**
 Y: **5002438**

 Drilling contractor : **Explora-sol inc.**

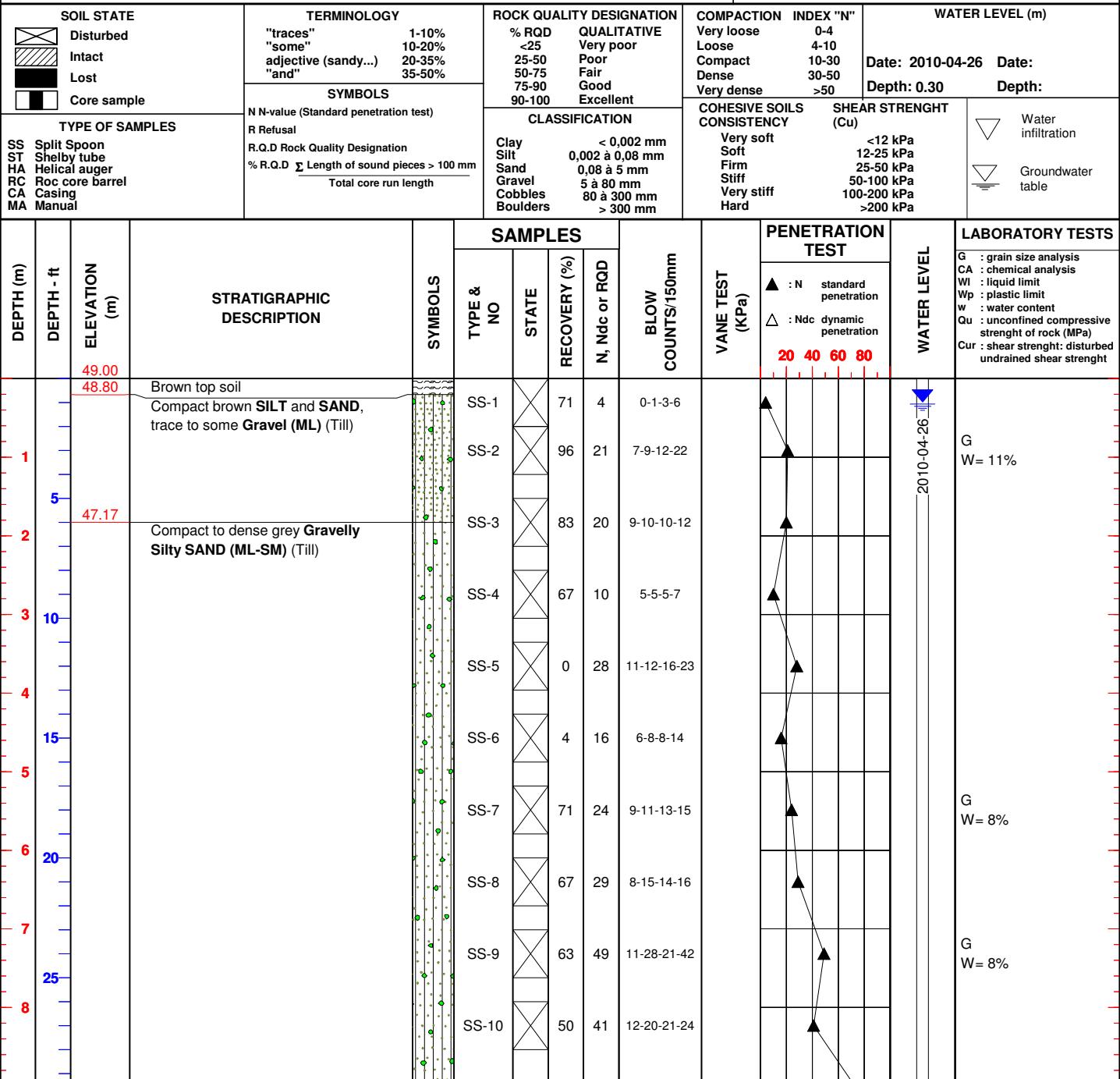
 Date of drilling : **2010-04-01**

 Drilling type : **Casing**
 Diameter : **76,2 mm**

 Drilling depth (m) : **15.24**

 Field technician : **Karim Boudalja, géo.**

Prepared by : Sébastien Veillette, dess.



Remark(s):

BOREHOLE REPORT

Borehole N°

10BH-07

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			BLOW COUNTS/150mm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)					
-10												
35		37.93										
11			Bedrock: Black LIMESTONE, poor to excellent quality		SS-11	☒	80	84	-34-50 / 10 cm			
12					SS-12	☒	100	83	-33-50 / 10 cm			
40					RC-13	☒	41	35				
13					RC-14	☒	60	61				
45					RC-15	☒	98	94				
14		33.76	END OF BOREHOLE									Qu= 165
15												
16												
17												
18												
19												
20												
21												
22												
23												
24												
25												

Borehole N°
10BH-04

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **316203**
 Y: **4994292**

 Drilling contractor : **Explora-sol inc.**

 Date of drilling : **2010-03-10**

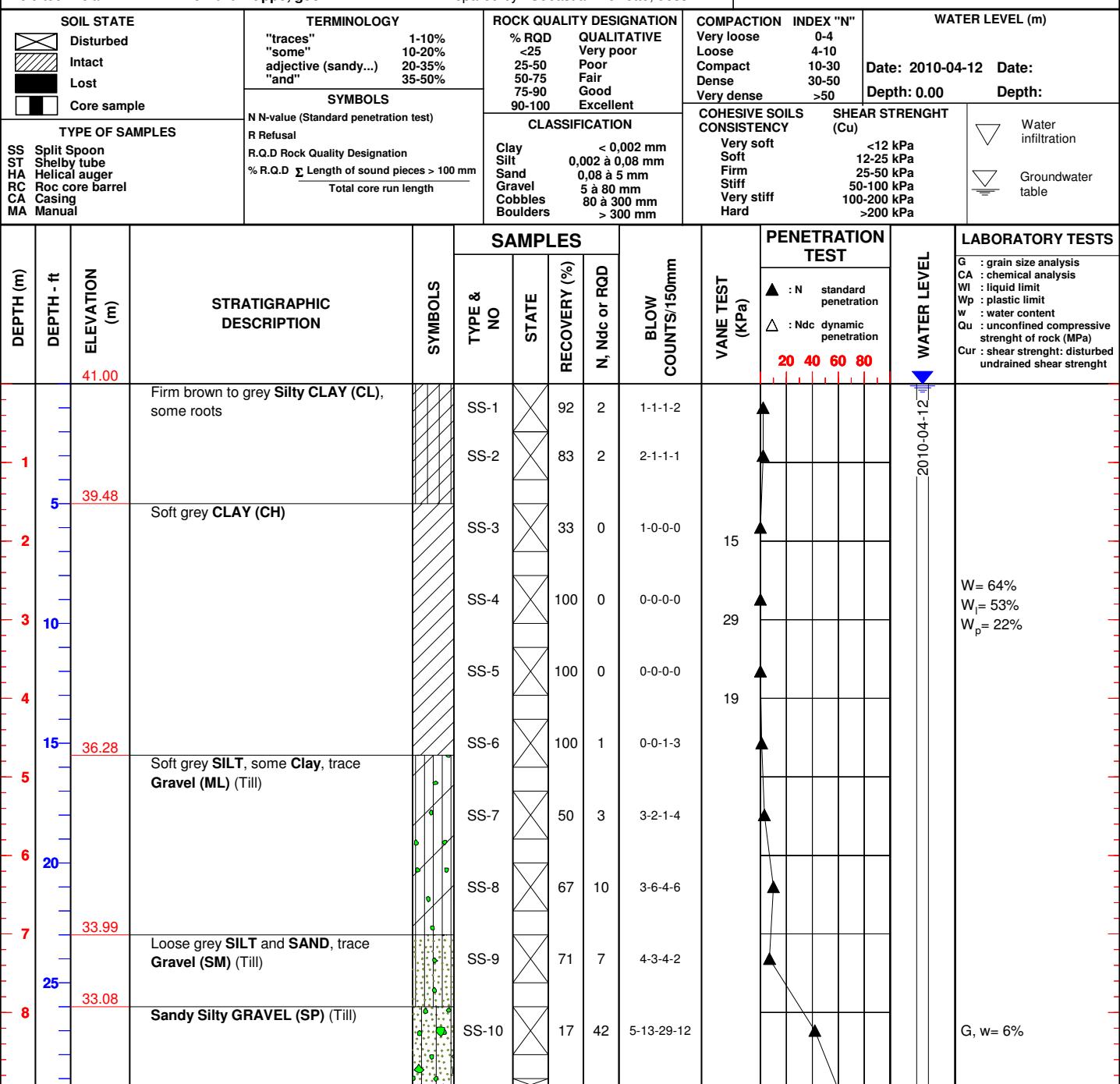
 Drilling type : **Casing**

 Drilling depth (m) : **14.99**

 Diameter : **76,2 mm**

 Field technician : **Bernard Huppé, géo.**

Prepared by : Sébastien Veillette, dess.



Remark(s):

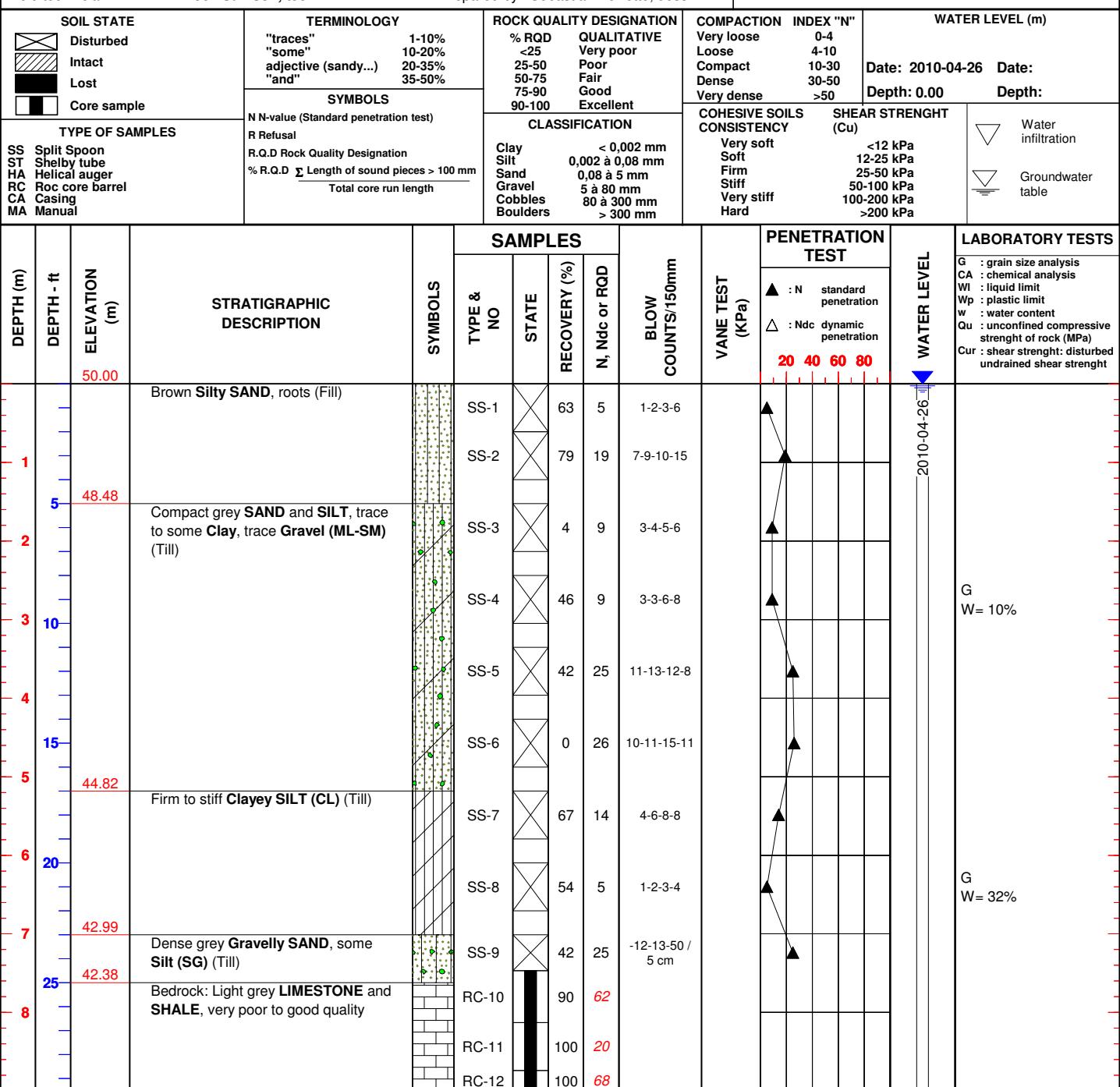
BOREHOLE REPORT

Borehole N°
10BH-04

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)			
10					SS-11		29	62	-43-19-50 / 13 cm	
11					SS-12		54	40	22-20-20-27	
12					SS-13		75	69	-19-50	
13					RC-14		100	93		
14					RC-15		100	79		
15		26.01	END OF BOREHOLE							Qu = 113
16										
17										
18										
19										
20										
21										
22										
23										
24										
25										

Borehole N°
10BH-05

Project :	Wind Energy Converters (WEC)	O/F :	G1-09-1532
Client :	TRANSALTA		
Location :	Saint-Valentin, Québec	Geodesic coordinates (NAD-1983)	X: 316239 Y: 5001777
Drilling contractor :	Explora-sol inc.		
Drilling type :	Casing	Date of drilling :	2010-03-31
Diameter :	76,2 mm	Drilling depth (m) :	10.82
Field technician :	Rock Samson, tech.	Prepared by : Sébastien Veillette, dess.	



Remark(s):

BOREHOLE REPORT

Borehole N°
10BH-05

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)			
10										
35		39.18	END OF BOREHOLE		RC-13		100	83		
40										
45										
50										
55										
60										
65										
70										
75										
80										
85										
90										
95										
100										
105										
110										
115										
120										
125										
130										
135										
140										
145										
150										
155										
160										
165										
170										
175										
180										
185										
190										
195										
200										
205										
210										
215										
220										
225										
230										
235										
240										
245										
250										

Borehole N°
10BH-06

Project : **Wind Energy Converters (WEC)**

O/F : **G1-09-1532**

Client : **TRANSALTA**

Location : **Saint-Valentin, Québec**

Geodesic coordinates (NAD-1983) X: **316202**
Y: **4994943**

Drilling contractor : **Explora-sol inc.**

Date of drilling : **2010-03-11**

Drilling type : **Casing**

Drilling depth (m) : **15.80**

Diameter : **76,2 m**

Field technician : **Bernard Huppé, géo.**

Prepared by : Sébastien Veillette, dess.

SOIL STATE		TERMINOLOGY		ROCK QUALITY DESIGNATION		COMPACTION INDEX "N"		WATER LEVEL (m)	
		"traces" "some" adjective (sandy...)		1-10% 10-20% 20-35%		% RQD <25 25-50 50-75 75-90 90-100		QUALITATIVE Very poor Poor Fair Good Excellent	
		"and"		35-50%		Very loose Loose Compact Dense Very dense		0-4 4-10 10-30 30-50 >50	
		SYMBOLS		CLASSIFICATION		COHESIVE SOILS CONSISTENCY		SHEAR STRENGTH (Cu)	
TYPE OF SAMPLES		N N-value (Standard penetration test) R Refusal		Clay Silt Sand Gravel Cobbles Boulders		< 0,002 mm 0,002 à 0,08 mm 0,08 à 5 mm 5 à 80 mm 80 à 300 mm > 300 mm		<12 kPa 12-25 kPa 25-50 kPa 50-100 kPa 100-200 kPa 	
SS Split Spoon ST Shelby tube HA Helical auger RC Roc core barrel CA Casing 		R.Q.D Rock Quality Designation % R.Q.D Σ Length of sound pieces > 100 mm Total core run length							
DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES	PENETRATION TEST	LABORATORY TESTS		
					TYPE & NO	STATE	RECOVERY (%)	N, Ndc or RQD	
		42.00							
1		41.29	Brown SAND, trace Silt (SP)		SS-1		75	24	1-7-17-9
2		38.65	Soft grey CLAY (CH)		SS-2		79	5	3-2-3-3
3					SS-3		100	0	0-0-0-1
4					SS-4		100	0	0-0-0-0
5					SS-5		75	9	2-4-5-7
6					SS-6		71	14	6-7-7-11
7					SS-7		67	15	6-7-8-10
8					SS-8		75	13	6-5-8-9
9					SS-9		75	10	5-5-5-5
10					SS-10		58	28	6-9-19-36
		33.16							
<p>W = 56% W_f = 52% W_p = 17%</p> <p>G, w = 19%</p>									
<p>Remark(s):</p>									

P:\Multi-Partage Groupe ABS\Géotechs\Fichier de style LOG GÉOTECH\log_forage_ABS_Anglais_elevation.sty

Verified by: Ibrahim Ja'far, ing.M.Ing.

Approved by : Ursula Maselbas, ing.M.Sc.A.

Date of report 2010-06-09

BOREHOLE REPORT

Borehole N°
10BH-06

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			BLOW COUNTS/150mm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)					
-10			Compact grey SILT, some Gravel and Sand (ML) (Till)		SS-11		4	19	7-8-11-10			
-11					SS-12		4	11	6-6-5-10			
-12					SS-13		4	17	12-10-7-10			
-13		29.61			RC-14		100	100				G, w= 15%
-14			Bedrock: Grey LIMESTONE, fair to excellent quality		RC-15		86	70				
-15					RC-16		100	90				
-16		26.20	END OF BOREHOLE									Qu= 106
-17												
-18												
-19												
-20												
-21												
-22												
-23												
-24												
-25												

Borehole N°
10BH-08

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **316248**
 Y: **4998369**

 Drilling contractor : **Explora-sol inc.**

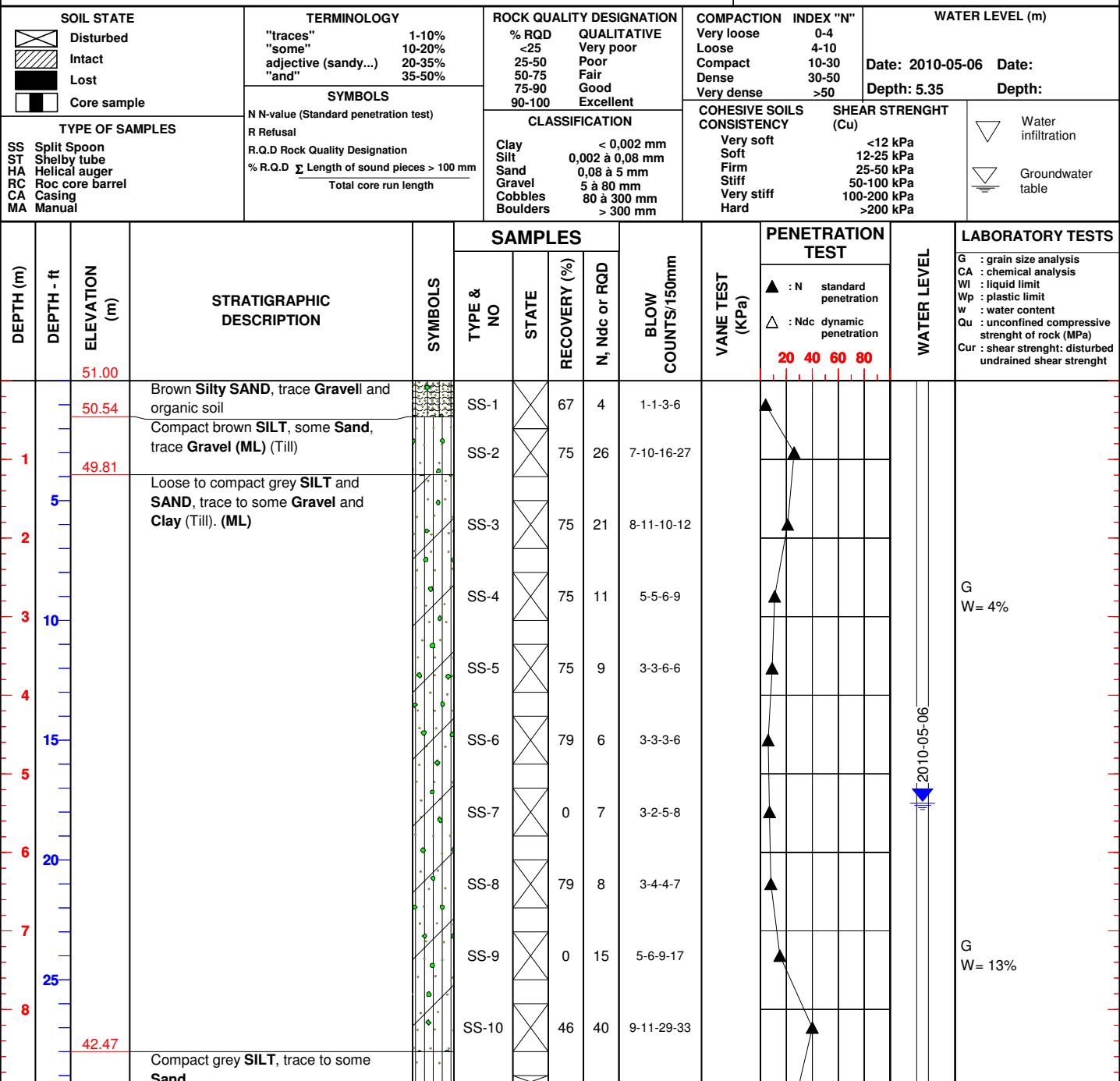
 Date of drilling : **2010-03-17**

 Drilling type : **Casing**
 Diameter : **76,2 mm**

 Drilling depth (m) : **22.56**

 Field technician : **Bernard Huppé, géo.**

Prepared by : Sébastien Veillette, dess.



Remark(s):

BOREHOLE REPORT

Borehole N°
10BH-08

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%) N, Ndc or RQD			
10					SS-11		75	27	11-12-15-19	
35					SS-12		79	23	8-10-13-17	
11	39.88		Loose to compact grey Sandy SILT , some Gravel and Clay (SM) (Till)		SS-13		63	13	6-7-6-20	G W= 16%
12	40				SS-14		71	33	14-15-18-19	
13	45				SS-15		58	3	5-1-2-5	
14	50				SS-16		79	21	13-9-12-24	
15	55	34.24	Very dense grey SILT , some Sand . Presence of Cobbles (ML)		SS-17		80	50	/ 13 cm	G W= 8%
16	60				SS-18		40	50	/ 13 cm	
17	65	31.62	BOULDERS: Over consolidated till		RC-19		100	61		
18	70				RC-20		100	82		
19	75				RC-21		100	90		
20	80	28.45	END OF BOREHOLE							
21										
22										
23										
24										
25										

Borehole N°
10BH-09

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **316478**
 Y: **5001418**

 Drilling contractor : **Explora-sol inc.**

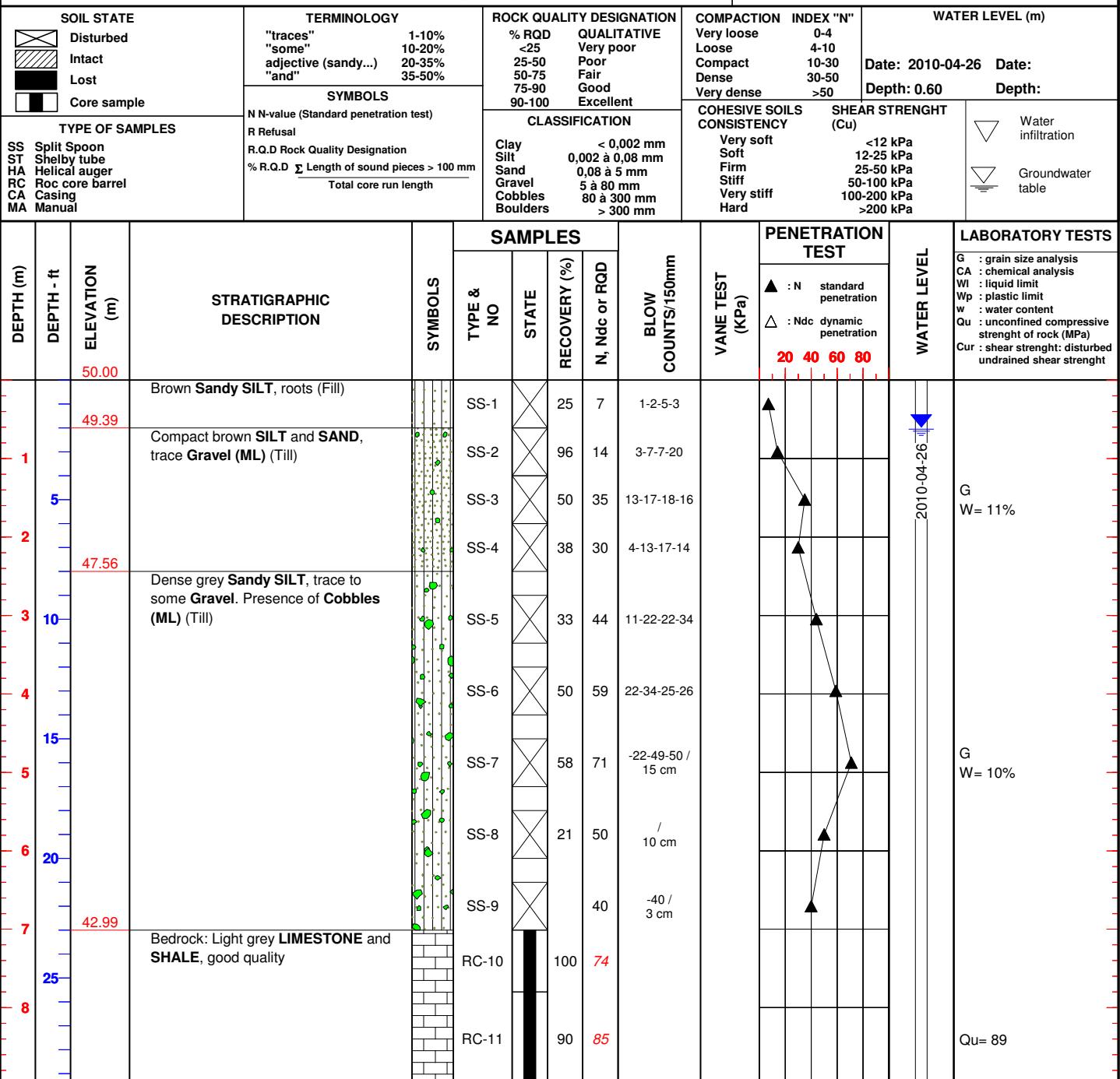
 Date of drilling : **2010-03-29**

 Drilling type : **Casing**
 Diameter : **76,2 mm**

 Drilling depth (m) : **10.85**

 Field technician : **Rock Samson, tech.**

Prepared by : Sébastien Veillette, dess.



Remark(s):

BOREHOLE REPORT

Borehole N°
10BH-09

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)			
10										
35		39.15	END OF BOREHOLE		RC-12		90	86		
40										
45										
50										
55										
60										
65										
70										
75										
80										
85										
90										
95										
100										
105										
110										
115										
120										
125										
130										
135										
140										
145										
150										
155										
160										
165										
170										
175										
180										
185										
190										
195										
200										
205										
210										
215										
220										
225										
230										
235										
240										
245										
250										

Borehole N°
10BH-10

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **316497**
 Y: **5002120**

 Drilling contractor : **Explora-sol inc.**

 Date of drilling : **2010-03-30**

 Drilling type : **Casing**
 Diameter : **76,2 mm**

 Drilling depth (m) : **20.88**

 Field technician : **Karim Boudalia, géo.**

Prepared by : Sébastien Veillette, dess.

SOIL STATE		TERMINOLOGY		ROCK QUALITY DESIGNATION		COMPACTION INDEX "N"		WATER LEVEL (m)	
	Disturbed	"traces"	1-10%	% RQD	QUALITATIVE	Very loose	0-4	Date: 2010-04-26	Date:
	Intact	"some"	10-20%	<25	Very poor	Loose	4-10	Depth: 0.00	Depth:
	Lost	adjective (sandy...)	20-35%	25-50	Poor	Compact	10-30		
	Core sample	"and"	35-50%	50-75	Fair	Dense	30-50		
		SYMBOLS		90-100		Excellent			
TYPE OF SAMPLES		N N-value (Standard penetration test)		CLASSIFICATION		COHESIVE SOILS CONSISTENCY		SHEAR STRENGTH (Cu)	
SS	Split Spoon	R Refusal		Clay	< 0,002 mm	Very soft	<12 kPa		Water infiltration
ST	Shelby tube	R.Q.D Rock Quality Designation		Silt	0,002 à 0,08 mm	Soft	12-25 kPa		
HA	Helical auger	% R.Q.D Σ Length of sound pieces > 100 mm	Total core run length	Sand	0,08 à 5 mm	Firm	25-50 kPa		
RC	Roc core barrel			Gravel	5 à 80 mm	Stiff	50-100 kPa		
CA	Casing			Cobbles	80 à 300 mm	Very stiff	100-200 kPa		
MA	Manual			Boulders	> 300 mm	Hard	>200 kPa		
50.00	49.39	47.56	44.69	50.00	49.39	47.56	44.69	20 40 60 80	2010-04-26
DEPTH (m)	DEPTH - ft	ELEVATION (m)	ELEVATION (ft)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
						TYPE & NO	STATE		
						N, Ndc or RQD	RECOVERY (%)		
1	5			SS-1		83	7	2-3-4-10	
2	10			SS-2		83	28	16-11-17-36	
3	15			SS-3		83	22	16-13-9-12	
4	20			SS-4		71	6	2-3-3-6	
5	25			SS-5		71	8	3-3-5-9	
6	30			SS-6		75	27	5-17-10-16	
7	35			SS-7		20	50	/ 13 cm	
8	40			SS-8		71	31	10-15-16-35	
9	45			SS-9		88	78	26-32-46-50 / 15 cm	
10	50			SS-10		91	82	-32-50 / 15 cm	

Remark(s):

BOREHOLE REPORT

Borehole N°
10BH-10

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			BLOW COUNTS/150mm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)					
10					SS-11	+	100	86	-36-50 / 10 cm			
11					SS-12	+	70	90	-40-50 / 10 cm			
12					SS-13	+	100	85	-35-50 / 13 cm			
13					SS-14	+	100	83	-33-50 / 13 cm			
14					SS-15	+	80	50	/ 10 cm			
15					SS-16	+	88	46	-16-30-50 / 13 cm			
16					SS-17	+	0	50	/ 8 cm			
17					SS-18	+	0	50	/ 5 cm			
18					RC-19		42	31				
19		30.82	BOULDERS									G W = 8%
20												
21		29.12	END OF BOREHOLE									
22												
23												
24												
25												

Borehole N°
10BH-11

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **316592**
 Y: **4994528**

 Drilling contractor : **Explora-sol inc.**

 Date of drilling : **2010-03-08**

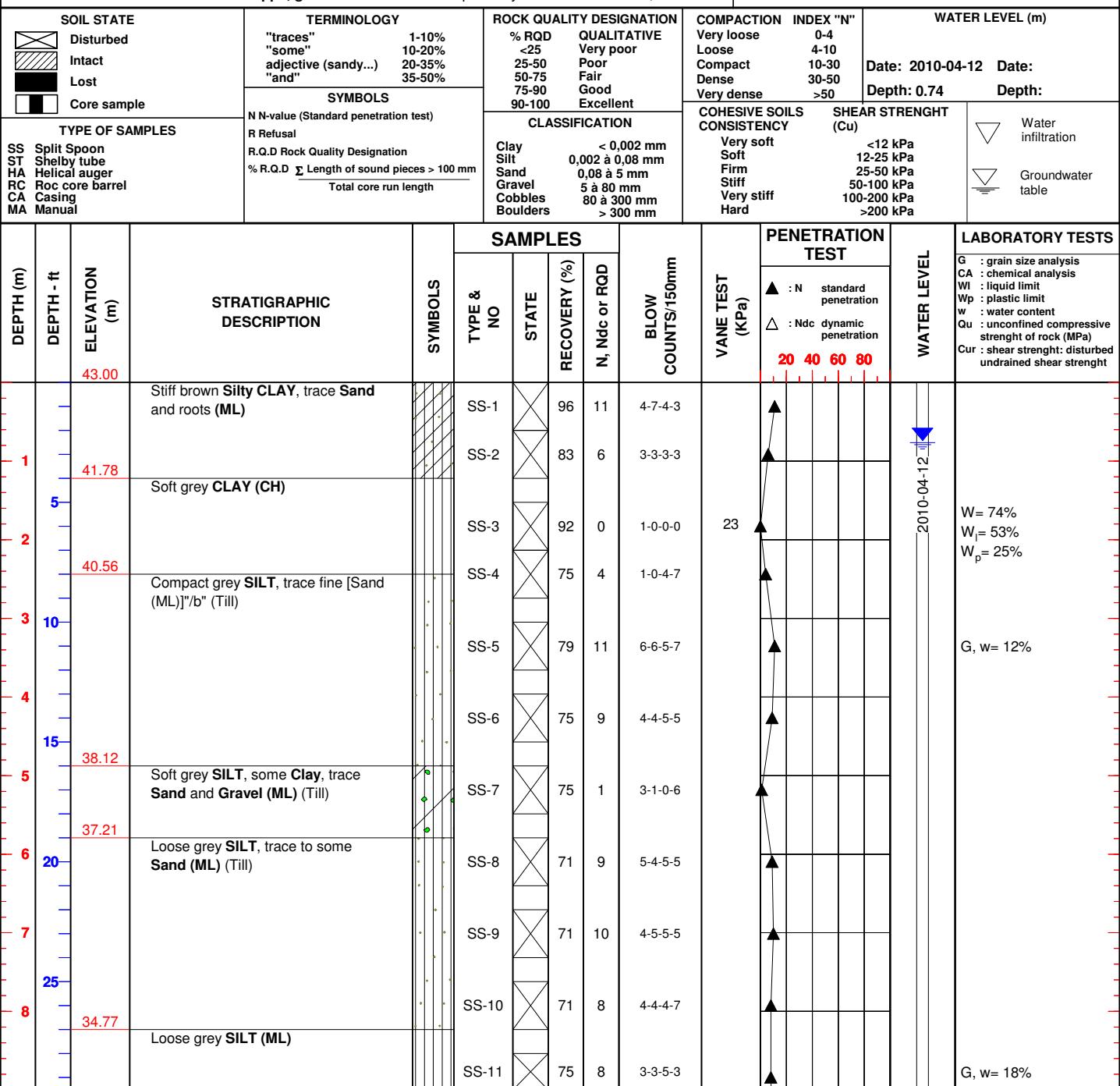
 Drilling type : **Casing**

 Drilling depth (m) : **15.62**

 Diameter : **76,2 mm**

 Field technician : **Bernard Huppé, géo.**

Prepared by : Sébastien Veillette, dess.



Remark(s):

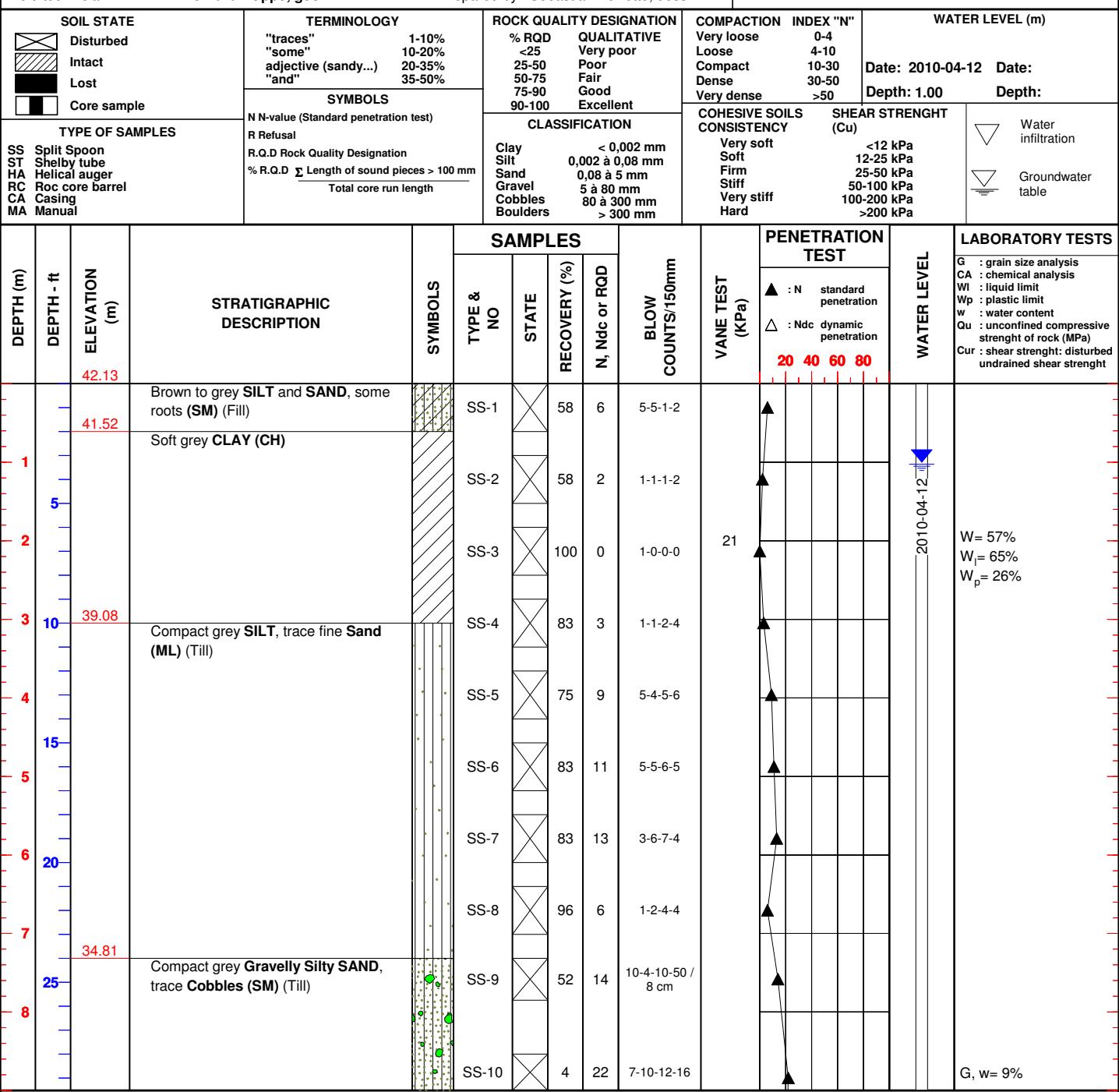
BOREHOLE REPORT

Borehole N°
10BH-11

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			RECOVERY (%)	N, Ndc or RQD	BLOW COUNTS/150mm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)							
35	32.33	Compact grey Sandy GRAVEL, some Silt and Cobbles (SP) (Till)		SS-12	SS-12		71	9	3-2-7-13			▲ : N standard penetration △ : Ndc dynamic penetration 20 40 60 80		G, w= 6%
40	30.53	Bedrock: Grey LIMESTONE, poor to excellent quality		SS-13	SS-13		21	25	19-15-10-15					
45				SS-14	SS-14		73			-12-50 / 13 cm				
50				RC-15	RC-15		100	66						
55				RC-16	RC-16		100	37						
60				RC-17	RC-17		100	100						
65			END OF BOREHOLE											
70														
75														
80														
85														
90														
95														
100														
105														
110														
115														
120														
125														
130														
135														
140														
145														
150														
155														
160														
165														
170														
175														
180														
185														
190														
195														
200														
205														
210														
215														
220														
225														
230														
235														
240														
245														
250														

Borehole N°
10BH-12

Project :	Wind Energy Converters (WEC)	O/F :	G1-09-1532
Client :	TRANSALTA		
Location :	Saint-Valentin, Québec	Geodesic coordinates (NAD-1983)	X: 316596 Y: 4994055
Drilling contractor :	Explora-sol inc.		
Drilling type :	Casing	Date of drilling :	2010-03-09
Diameter :	76,2 mm	Drilling depth (m) :	17.83
Field technician :	Bernard Huppé, géo.	Prepared by :	Sébastien Veillette, dess.



Remark(s):

BOREHOLE REPORT

Borehole N°
10BH-12

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES		RECOVERY (%)	N, Ndc or RQD	BLOW COUNTS/150mm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE							
10					SS-11		0	21	12-11-10-14				
11					SS-12		63	13	5-4-9-13				
12					SS-13		82	25	15-11-14-50 / 10 cm				
13					SS-14		73	68	25-24-44-50 / 10 cm				
14					RC-15		100	82					
15			Bedrock: Grey LIMESTONE, good to excellent quality		RC-16		98	83					Qu = 90
16					RC-17		100	90					
17			END OF BOREHOLE										
18		24.29											
19													
20													
21													
22													
23													
24													
25													

Borehole N°
10BH-13

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **316618**
 Y: **4998175**

 Drilling contractor : **Explora-sol inc.**

 Date of drilling : **2010-03-18**

 Drilling type : **Casing**
 Diameter : **76,2 mm**

 Drilling depth (m) : **30.48**

 Field technician : **Bernard Huppé, géo.**

Prepared by : Sébastien Veillette, dess.

SOIL STATE		TERMINOLOGY		ROCK QUALITY DESIGNATION		COMPACTION INDEX "N"		WATER LEVEL (m)		
		"traces" "some" adjective (sandy...)		1-10% 10-20% 20-35%		% RQD <25 25-50 50-75 75-90 90-100		QUALITATIVE Very poor Poor Fair Good Excellent		
		"and"		35-50%		Very loose Loose Compact Dense Very dense		0-4 4-10 10-30 30-50 >50		
		SYMBOLS		N N-value (Standard penetration test)		CLASSIFICATION		COHESIVE SOILS CONSISTENCY		
TYPE OF SAMPLES		R Refusal		Clay		< 0,002 mm		SHEAR STRENGTH (Cu)		
SS Split Spoon		R.Q.D Rock Quality Designation		Silt		0,002 à 0,08 mm		<12 kPa		
ST Shelby tube		% R.Q.D Σ Length of sound pieces > 100 mm		Sand		0,08 à 5 mm		12-25 kPa		
HA Helical auger		Total core run length		Gravel		5 à 80 mm		25-50 kPa		
RC Roc core barrel		Boulders		Cobbles		80 à 300 mm		50-100 kPa		
CA Casing				Boulders		> 300 mm		100-200 kPa		
MA Manual								>200 kPa		
DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES	TYPE & NO	STATE	RECOVERY (%)	PENETRATION TEST	WATER LEVEL
47.92						N, Ndc or RQD			▲ : N standard penetration △ : Ndc dynamic penetration	
47.31			Brown SAND, some Silt and organic matter		SS-1		71	7	20 40 60 80	
47.31			Compact brown Silty SAND, some Gravel (ML) (Till)		SS-2		100	30	20 40 60 80	2010-05-06
46.09			Loose grey Sandy SILT, trace to some Gravel (ML) (Till)		SS-3		92	19	20 40 60 80	
46.09					SS-4		83	10	20 40 60 80	
46.09					SS-5		79	11	20 40 60 80	
46.09					SS-6		88	4	20 40 60 80	
46.09					SS-7		46	4	20 40 60 80	
46.09					SS-8		58	5	20 40 60 80	
46.09					SS-9		75	7	20 40 60 80	
46.09					SS-10		88	7	20 40 60 80	
Remark(s):										

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Verified by: Ibrahim Ja'far, ing.M.Ing.

Approved by : Ursula Maslebas, ing.M.Sc.A.

Date of report 2010-06-09

BOREHOLE REPORT

Borehole N°
10BH-13

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			BLOW COUNTS/150mm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%) N, Ndc or RQD					
35	37.26	Compact grey SILT, trace Sand (ML) (Till)			SS-11		100	9	2-3-6-10			
45	34.21	Compact grey Silty SAND, some Gravel (SM) (Till)			SS-12		0	5	2-2-3-6			
55	30.25	BOULDERS: Over consolidated till.			SS-13		0	19	6-9-10-13			
65					SS-14		92	9	4-5-4-8			
70					SS-15		33	50	/ 8 cm			
75					SS-16		71	33	7-13-20-37			
80					SS-17		50	50	/ 15 cm			
85					RC-18		100	86				G W = 16%
90					RC-19		100	90				
95					RC-20		100	85				
100					RC-21		100	86				
105					RC-22		100	52				
110					RC-23		100	0				
115					RC-24		0	0				

BOREHOLE REPORT

Borehole N°
10BH-13

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			RECOVERY (%)	N, Ndc or RQD	BLOW COUNTS/150mm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)							
26	85				RC-25		100	79						
27	90				RC-26		100	56						
28					RC-27		100	91						
29	95													
30														
31														
32	105													
33														
34														
35	115													
36														
37														
38	125													
39														
40														
41	135													
END OF BOREHOLE														

Borehole N°
10BH-14

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **316620**
 Y: **4994936**

 Drilling contractor : **Explora-sol inc.**

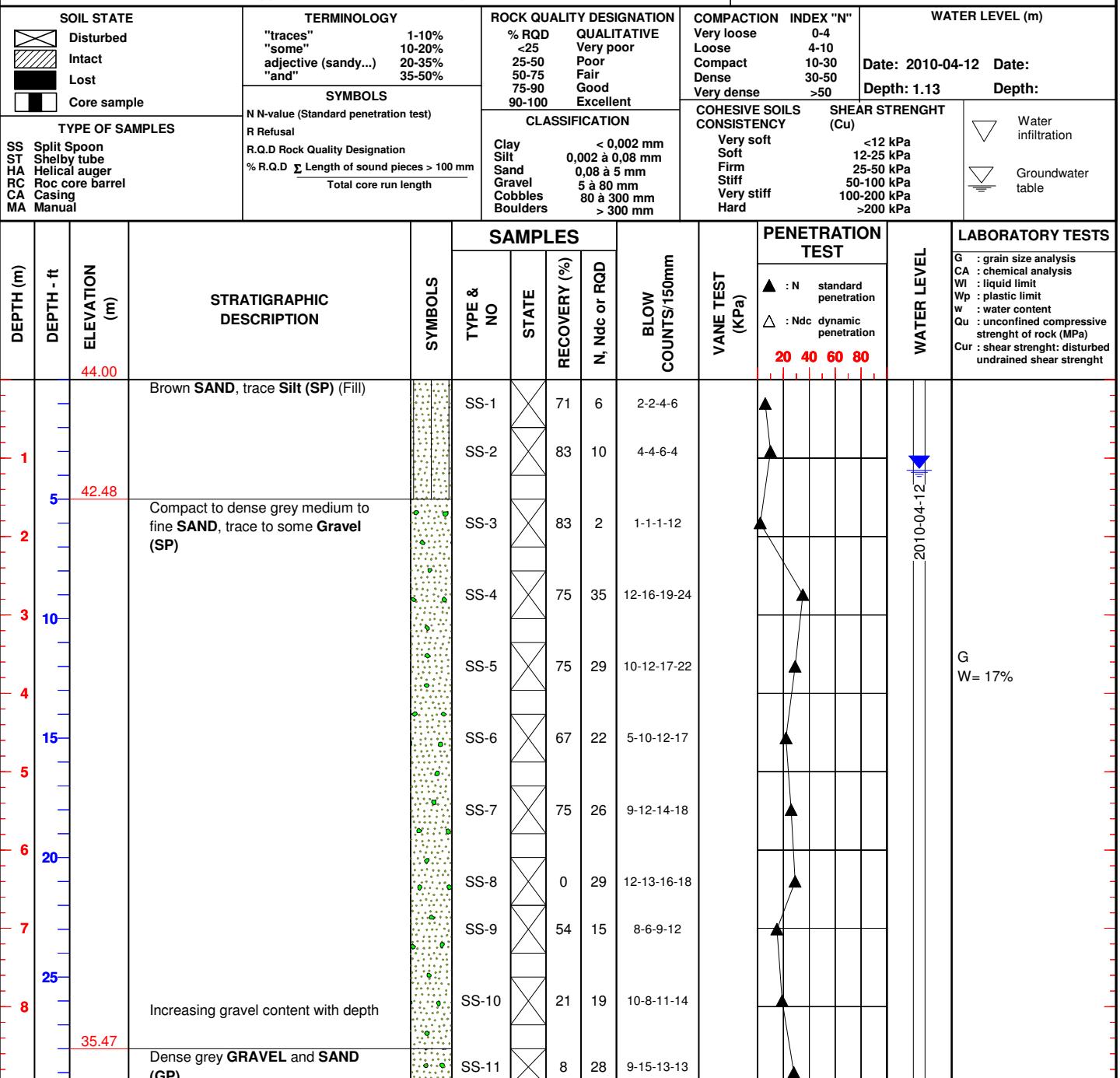
 Date of drilling : **2010-03-12**

 Drilling type : **Casing**
 Diameter : **76,2 mm**

 Drilling depth (m) : **16.10**

 Field technician : **Bernard Huppé, géo.**

Prepared by : Sébastien Veillette, dess.



Remark(s):

BOREHOLE REPORT

Borehole N°
10BH-14

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)	N, Ndc or RQD		
10					SS-12		4	33	15-15-18-23	G
35					SS-13		21	37	16-17-20-24	W = 10%
11					SS-14		29	21	8-8-13-10	
12					RC-15		100	100		
40					RC-16		100	100		
31.20			Bedrock: Grey LIMESTONE, excellent quality		RC-17		100	94		
13										Qu = 105
45										
14										
50										
15										
27.90			END OF BOREHOLE							
55										
16										
60										
17										
65										
18										
70										
19										
75										
20										
80										
21										
22										
23										
24										
25										

Borehole N°
10BH-16

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **316876**
 Y: **5001955**

 Drilling contractor : **Explora-sol inc.**

 Date of drilling : **2010-03-29**

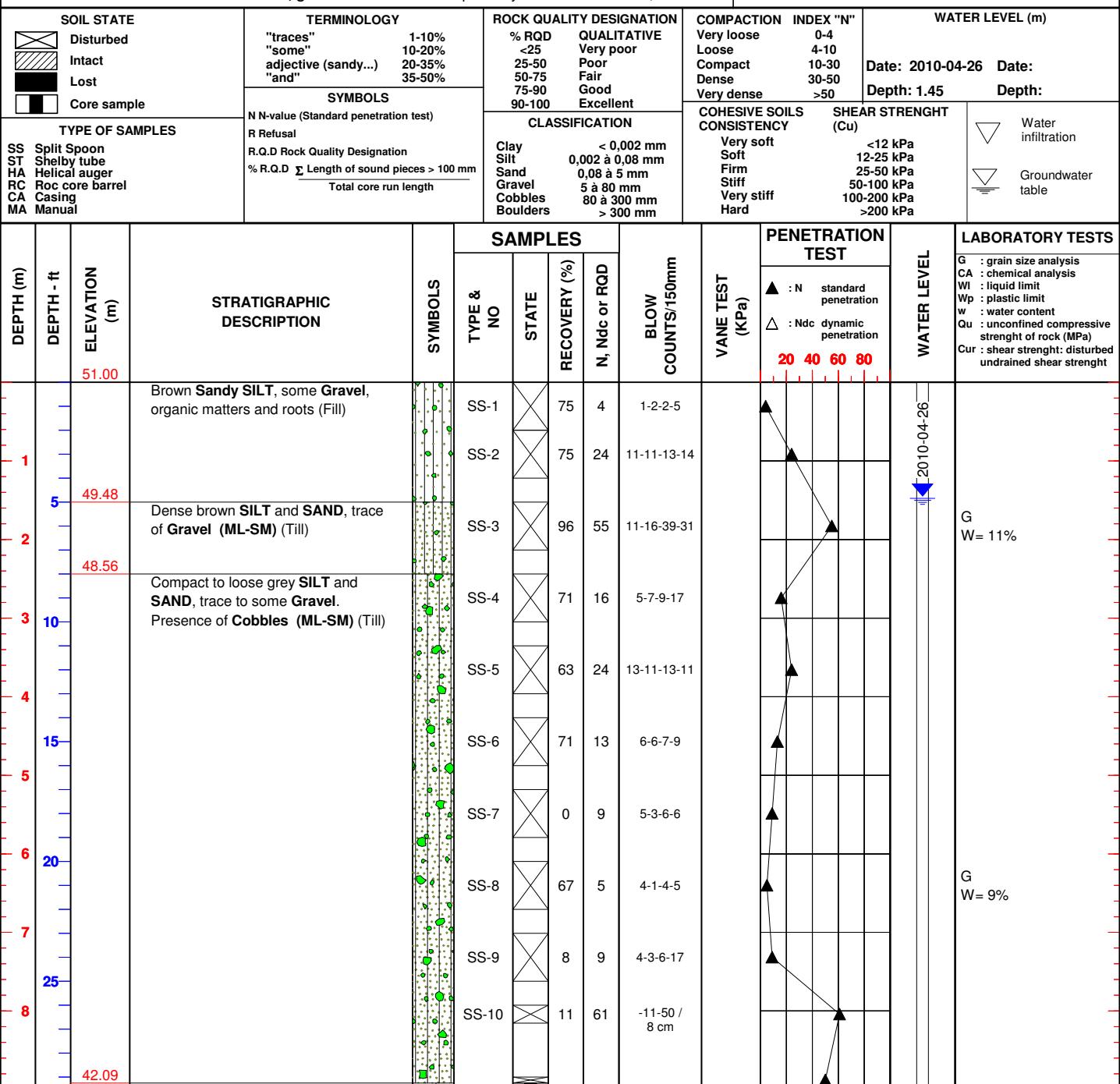
 Drilling type : **Casing**

 Drilling depth (m) : **12.09**

 Diameter : **76,2 mm**

 Field technician : **Karim Boudalia, géo.**

Prepared by : Sébastien Veillette, dess.



Remark(s):

BOREHOLE REPORT

Borehole N°
10BH-16

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			BLOW COUNTS/150mm -50 / 8 cm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%) N, Ndc or RQD					
10			Bedrock: Black LIMESTONE, good quality	SS-11			0 50			▲ : N standard penetration		
11				RC-12			97 86			△ : Ndc dynamic penetration		
12		38.91	END OF BOREHOLE	RC-13			97 90			20 40 60 80		Qu= 55
13												
14												
15												
16												
17												
18												
19												
20												
21												
22												
23												
24												
25												

Borehole N°
10BH-17A

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **317102**
 Y: **5001353**

 Drilling contractor : **Explora-sol inc.**

 Date of drilling : **2010-03-25**

 Drilling type : **Casing**

 Diameter : **76,2 mm**

 Drilling depth (m) : **19.94**

 Field technician : **Rock Samson, tech.**

Prepared by : Sébastien Veillette, dess.

SOIL STATE		TERMINOLOGY		ROCK QUALITY DESIGNATION		COMPACTION INDEX "N"		WATER LEVEL (m)	
		"traces" "some" adjective (sandy...)		1-10% 10-20% 20-35%		% RQD <25 25-50 50-75 75-90 90-100		QUALITATIVE Very poor Poor Fair Good Excellent	
		"and"		35-50%		Very loose Loose Compact Dense Very dense		0-4 4-10 10-30 30-50 >50	
		SYMBOLS		N N-value (Standard penetration test)		COHESIVE SOILS		WATER LEVEL (m)	
TYPE OF SAMPLES		R Refusal		CLASSIFICATION		CONSISTENCY		Date: 2010-04-26	
SS Split Spoon		R.Q.D Rock Quality Designation		Clay		< 0,002 mm		Date:	
ST Shelby tube		% R.Q.D Σ Length of sound pieces > 100 mm		Silt		0,002 à 0,08 mm		Depth: 0.75	
HA Helical auger		Total core run length		Sand		0,08 à 5 mm		Depth:	
RC Roc core barrel				Gravel		5 à 80 mm			
CA Casing				Cobbles		80 à 300 mm			
MA Manual				Boulders		> 300 mm			
DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS	
50.00					TYPE & NO	STATE	RECOVERY (%)	N, Ndc or RQD	
1		49.26	Brown Silty SAND (Fill)		SS-1		0	8	2-4-4-8
2		46.65	Soft grey Silty CLAY (CL)		SS-2		67	3	3-1-2-3
3		42.08	Loose to compact grey SILT and SAND, trace Gravel (ML-SM) (Till)		SS-3		75	1	1-0-1-0
4					SS-4		46	1	1-0-1-2
5					SS-5		63	9	1-4-5-7
6					SS-6		42	23	6-11-12-15
7					SS-7		83	4	1-2-2-3
8			Compact grey SILT and SAND, trace Gravel (ML-SM) (Till)		SS-8		50	6	2-3-3-4
9					SS-9		50	20	2-5-15-14
10					SS-10		75	29	10-15-14-10

Remark(s):

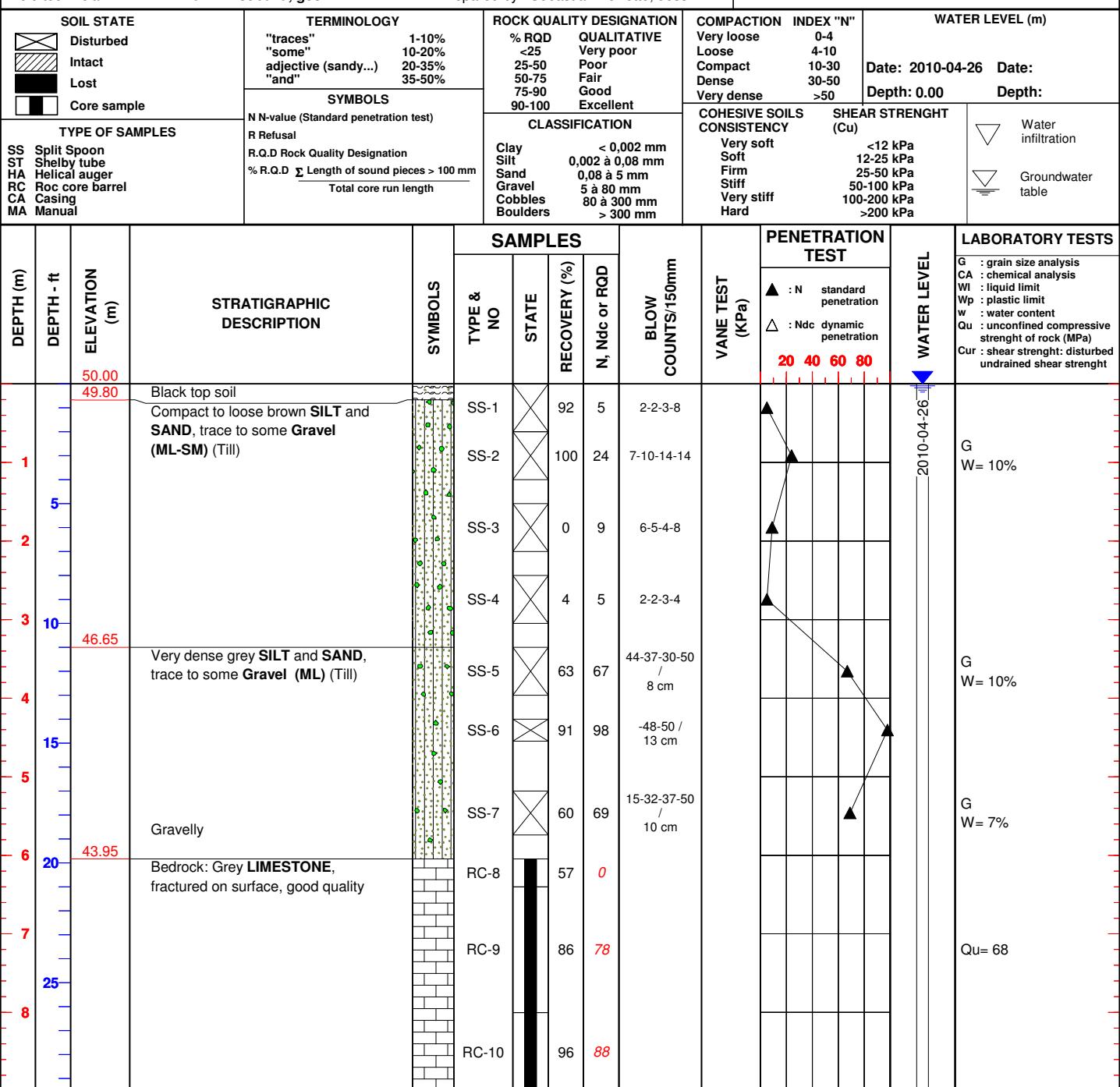
BOREHOLE REPORT

Borehole N°
10BH-17A

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			BLOW COUNTS/150mm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%) N, Ndc or RQD					
40.25			Very dense grey Sandy SILT, trace Gravel. Presence Cobbles (ML) (Till)		SS-11		100	50	-50 / 10 cm			G W = 9%
10					SS-12	+	100	73	-35-38-50 / 10 cm			
35					SS-13	+	100	84	-34-50 / 25 cm			
11					SS-14	+	50	67	-27-40-50 / 10 cm			
12					SS-15	+	100	50	/ 10 cm			
40					SS-16	+	100	90	-40-50 / 13 cm			
13					SS-17	+	80	50	/ 13 cm			
45					SS-18	+	25	50	/ 10 cm			
14					SS-19	+	100	50	/ 13 cm			
15					SS-20	+	13	50	/ 13 cm			
50					RC-21	+						
16			BOULDERS and COBBLES									
55												
17												
60												
18												
65		30.06										
19			END OF BOREHOLE									
20												
21												
22												
23												
24												
25												

Borehole N°
10BH-18

Project :	Wind Energy Converters (WEC)	O/F :	G1-09-1532
Client :	TRANSALTA		
Location :	Saint-Valentin, Québec	Geodesic coordinates (NAD-1983)	X: 317273 Y: 5002650
Drilling contractor :	Explora-sol inc.		
Drilling type :	Casing	Date of drilling :	2010-04-02
Diameter :	76,2 mm	Drilling depth (m) :	9.58
Field technician :	Karim Boudalia, géo.	Prepared by :	Sébastien Veillette, dess.



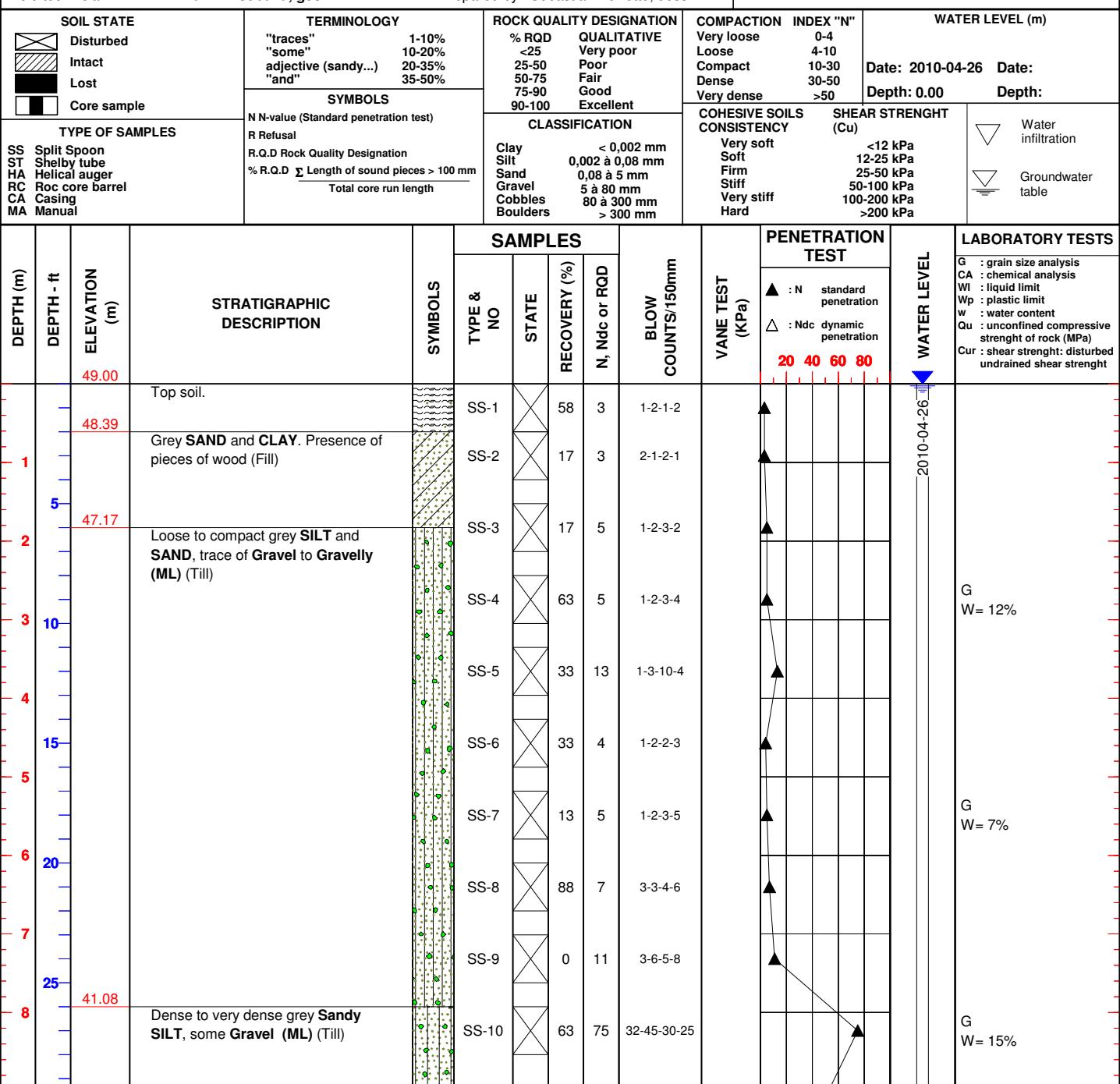
BOREHOLE REPORT

Borehole N°
10BH-18

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			RECOVERY (%)	N, Ndc or RQD	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)					
40.42			END OF BOREHOLE							▲ : N standard penetration △ : Ndc dynamic penetration 20 40 60 80		
10												
11												
12												
13												
14												
15												
16												
17												
18												
19												
20												
21												
22												
23												
24												
25												

Borehole N°
10BH-20

Project :	Wind Energy Converters (WEC)	O/F :	G1-09-1532
Client :	TRANSALTA		
Location :	Saint-Valentin, Québec	Geodesic coordinates (NAD-1983)	X: 317482 Y: 5002277
Drilling contractor :	Explora-sol inc.		
Drilling type :	Casing	Date of drilling :	2010-04-02
Diameter :	76,2 mm	Drilling depth (m) :	20.17
Field technician :	Karim Boudalia, géo.	Prepared by :	Sébastien Veillette, dess.



Remark(s):

BOREHOLE REPORT

Borehole N°
10BH-20

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)			
39.25			Zone of COBBLES and BOULDERS		SS-11		63	39	17-25-14-15	
10										
35										
11										
12										
36.81			Compact to very dense Gravelly SAND, trace of Silt. Presence of Cobbles and Boulders (SP)		SS-12		50	11	7-6-5-11	
13										
40										
14										
36.81										
15										
45										
16										
32.74			BOULDERS.		SS-13		100	65	-15-50 / 10 cm	
17										
55										
18										
60										
19										
65										
20										
28.83			END OF BOREHOLE		RC-15		37	0	/ 13 cm	
21										
70										
22										
75										
23										
80										
24										
25										

Borehole N°
10BH-21

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **318008**
 Y: **5002258**

 Drilling contractor : **Explora-sol inc.**

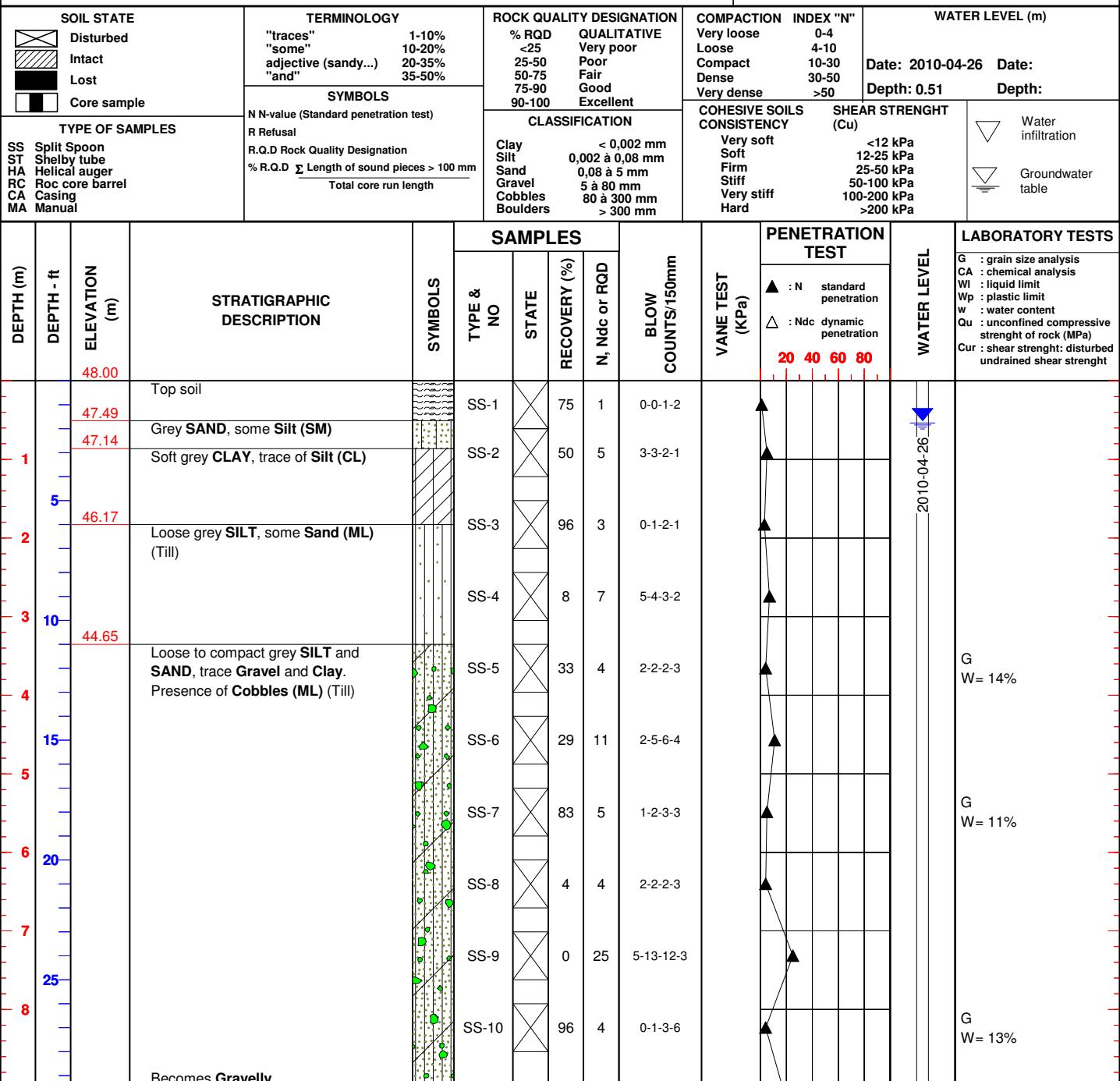
 Date of drilling : **2010-04-07**

 Drilling type : **Casing**
 Diameter : **76,2 mm**

 Drilling depth (m) : **14.33**

 Field technician : **Karim Boudalja, géo.**

Prepared by : Sébastien Veillette, dess.



Remark(s):

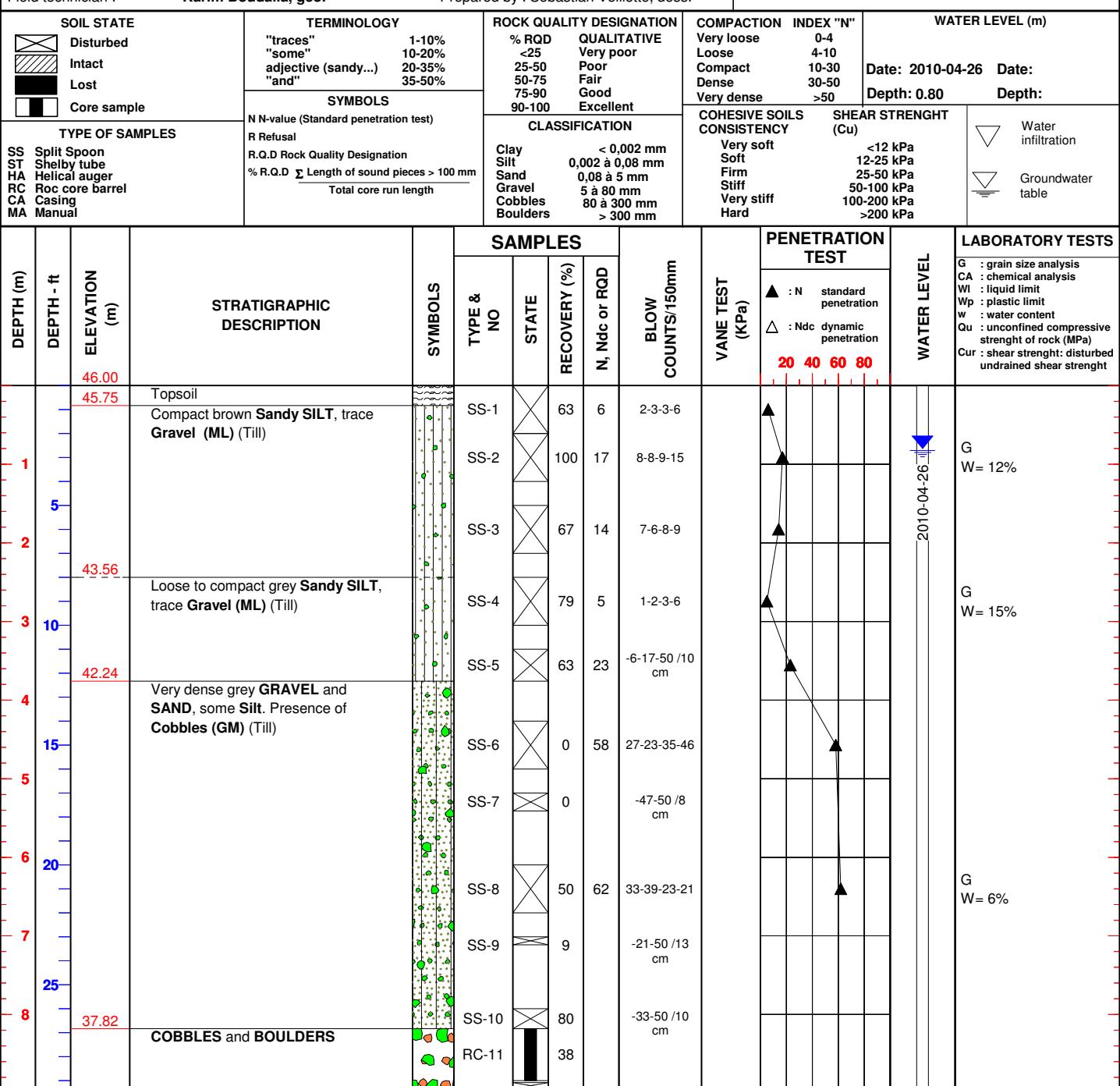
BOREHOLE REPORT

Borehole N°
10BH-21

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)			
10					SS-11		29	25	8-13-12-20	G W = 10%
11		36.82	Bedrock: Black and grey LIMESTONE, excellent quality		SS-12		92	65	-23-42-50 / 3 cm	
12					RC-13		90	93		Qu = 79
13					RC-14		98	95		
14		33.67	END OF BOREHOLE							
15										
16										
17										
18										
19										
20										
21										
22										
23										
24										
25										

Borehole N°
10BH-22

Project :	Wind Energy Converters (WEC)	O/F :	G1-09-1532
Client :	TRANSALTA		
Location :	Saint-Valentin, Québec	Geodesic coordinates (NAD-1983)	X: 318187 Y: 5001293
Drilling contractor :	Explora-sol inc.		
Drilling type :	Casing	Date of drilling :	2010-04-13
Diameter :	76,2 mm	Drilling depth (m) :	16.26
Field technician :	Karim Boudalia, géo.	Prepared by :	Sébastien Veillette, dess.



Remark(s):

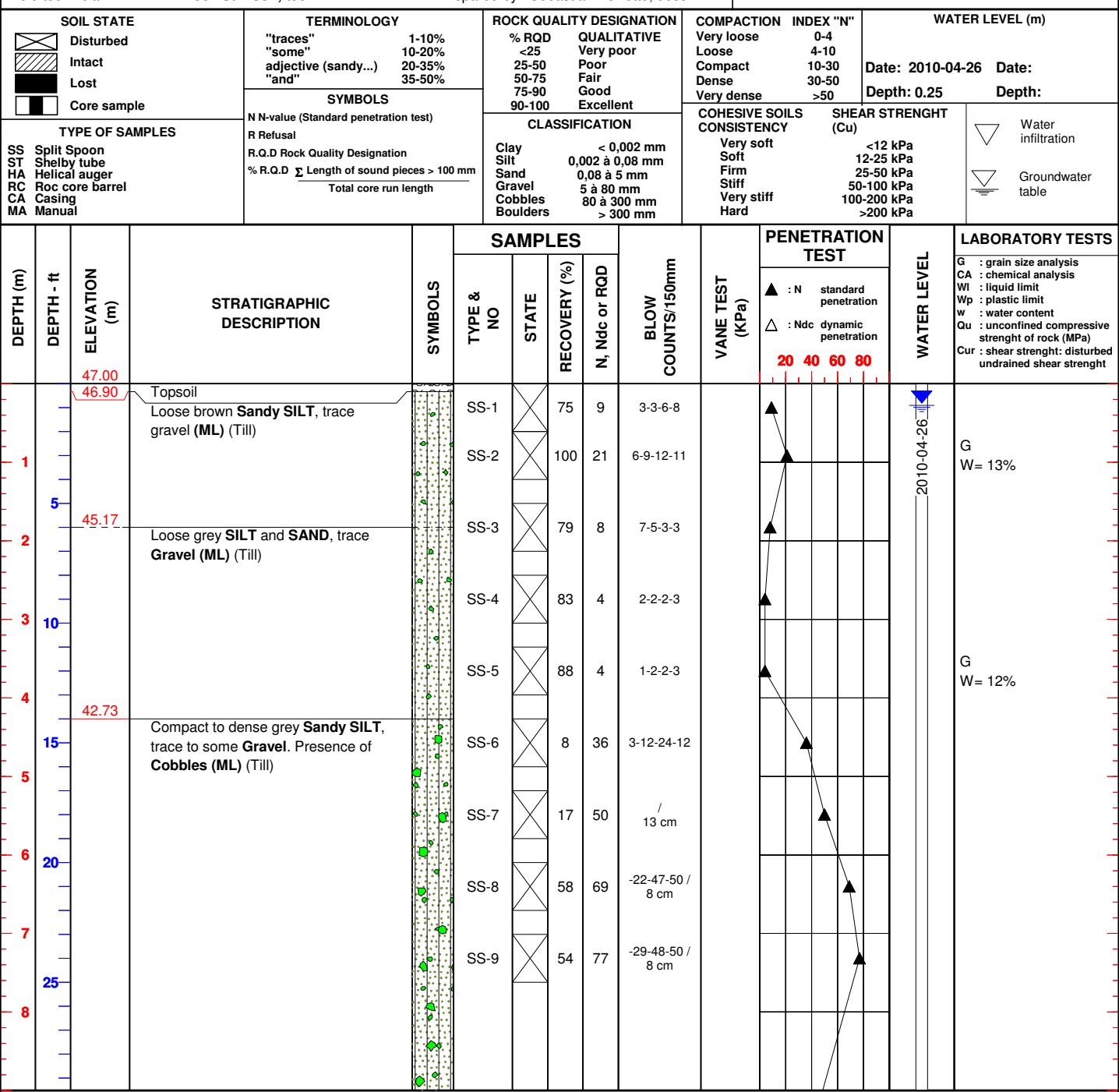
BOREHOLE REPORT

Borehole N°
10BH-22

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			N, Ndc or RQD	BLOW COUNTS/150mm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)						
-10					SS-12		67						
35					RC-13		42						
11					RC-14		5						
12					RC-15		62						
40					RC-16		57						
13	33.05		Bedrock: Black LIMESTONE, good quality		RC-17		97	88					
45					RC-18		97	84					
14					RC-19		83	75					
50			END OF BOREHOLE										Qu = 123
29.74													
16													
55													
17													
60													
18													
65													
19													
70													
20													
75													
21													
80													
22													
75													
23													
80													
24													
80													
25													

Borehole N°
10BH-23

Project :	Wind Energy Converters (WEC)	O/F :	G1-09-1532
Client :	TRANSALTA		
Location :	Saint-Valentin, Québec	Geodesic coordinates (NAD-1983)	X: 318195 Y: 5001745
Drilling contractor :	Explora-sol inc.		
Drilling type :	Casing	Date of drilling :	2010-04-13
Diameter :	76,2 mm	Drilling depth (m) :	13.72
Field technician :	Rock Samson, tech.	Prepared by : Sébastien Veillette, dess.	



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Verified by: Ibrahim Ja'far, ing.M.Ing.

Approved by : Ursula Maselbas, ing.M.Sc.A.

Date of report 2010-06-09

BOREHOLE REPORT

Borehole N°
10BH-23

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)			
10										
35	36.28		Bedrock: Grey LIMESTONE with SHALE, fair to good quality		SS-10	+	75	41	10-20-21-41	G W = 14%
40					RC-11	+	100	63		
45	33.28		END OF BOREHOLE		RC-12	+	100	90		Qu = 73
50										
55										
60										
65										
70										
75										
80										
85										
90										
95										
100										
105										
110										
115										
120										
125										
130										
135										
140										
145										
150										
155										
160										
165										
170										
175										
180										
185										
190										
195										
200										
205										
210										
215										
220										
225										
230	75									
235										
240	80									
245										
250	85									
255										

Borehole N°
10BH-25

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **319312**
 Y: **4997246**

 Drilling contractor : **Explora-sol inc.**

 Date of drilling : **2010-03-16**

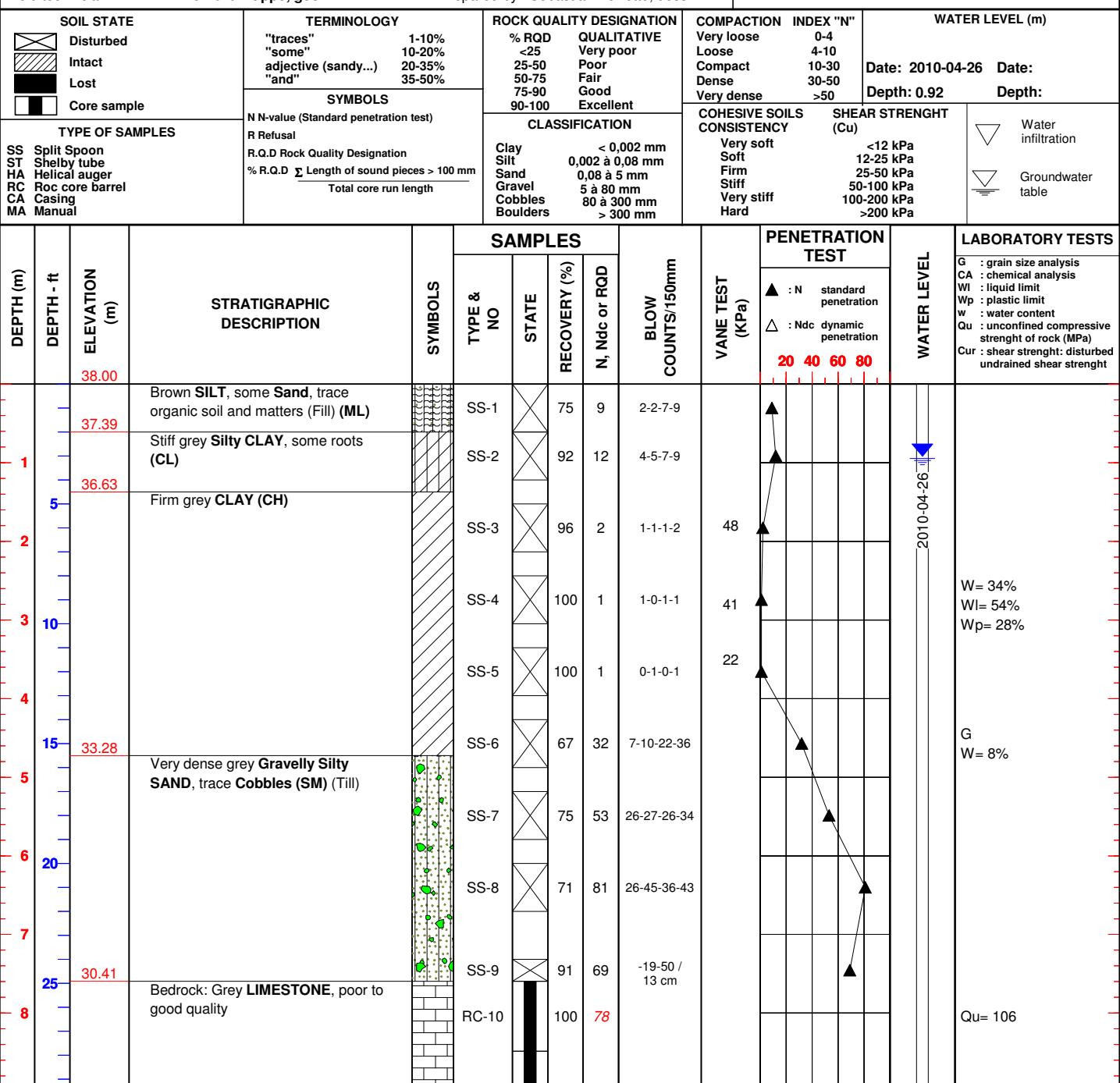
 Drilling type : **Casing**

 Drilling depth (m) : **11.15**

 Diameter : **76,2 mm**

 Field technician : **Bernard Huppé, géo.**

Prepared by : Sébastien Veillette, dess.



Remark(s):

BOREHOLE REPORT

Borehole N°
10BH-25

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%) N, Ndc or RQD			
10										
11	35	26.85	END OF BOREHOLE		RC-11		100 39			
12	40				RC-12		100 79			
13	45									
14	50									
15	55									
16	60									
17	65									
18	70									
19	75									
20	80									
21										
22										
23										
24										
25										

Borehole N°
10BH-26

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **319774**
 Y: **5001316**

 Drilling contractor : **Explora-sol inc.**

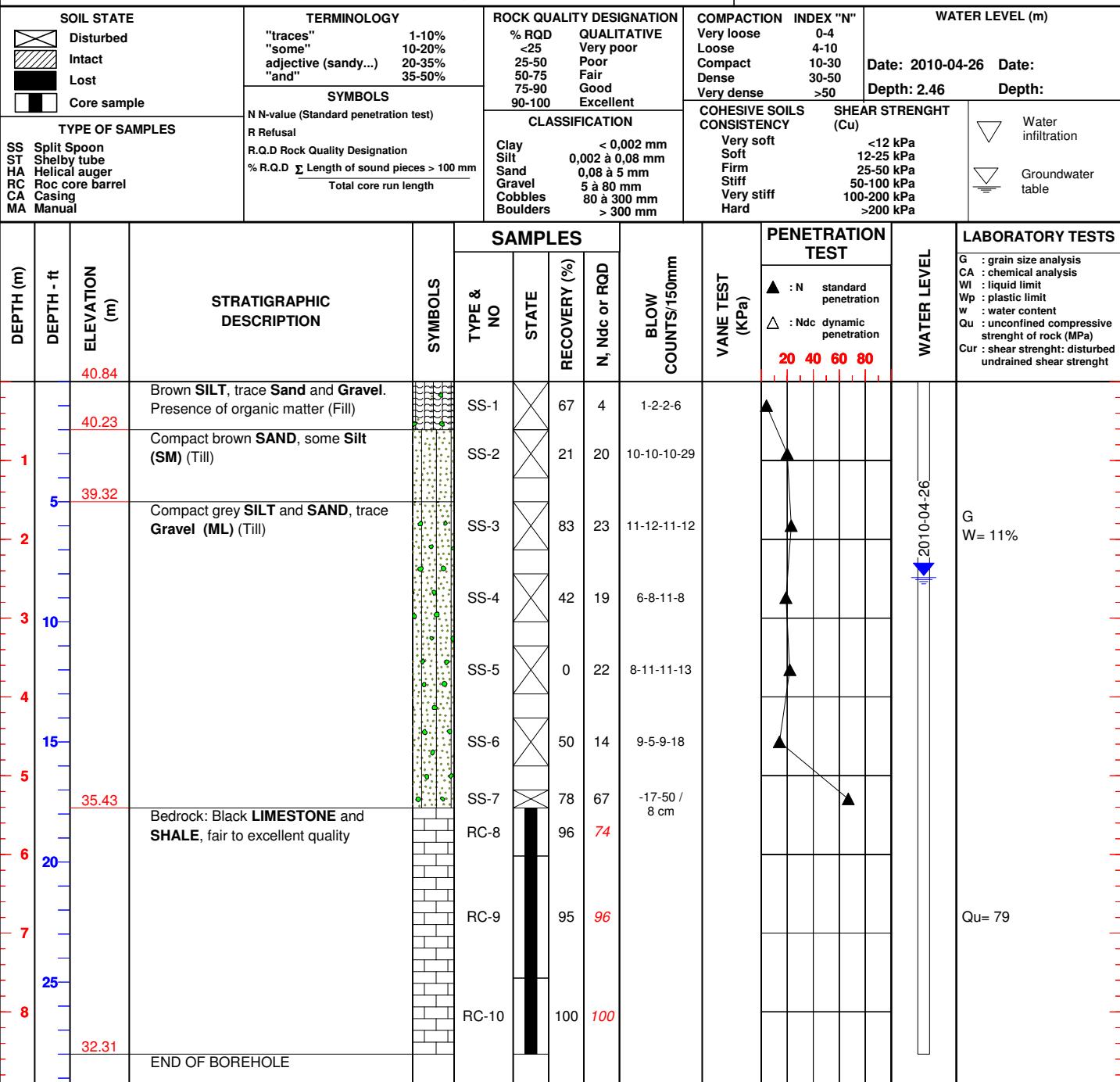
 Date of drilling : **2010-03-25**

 Drilling type : **Casing**
 Diameter : **76,2 mm**

 Drilling depth (m) : **8.53**

 Field technician : **Karim Boudalja, géo.**

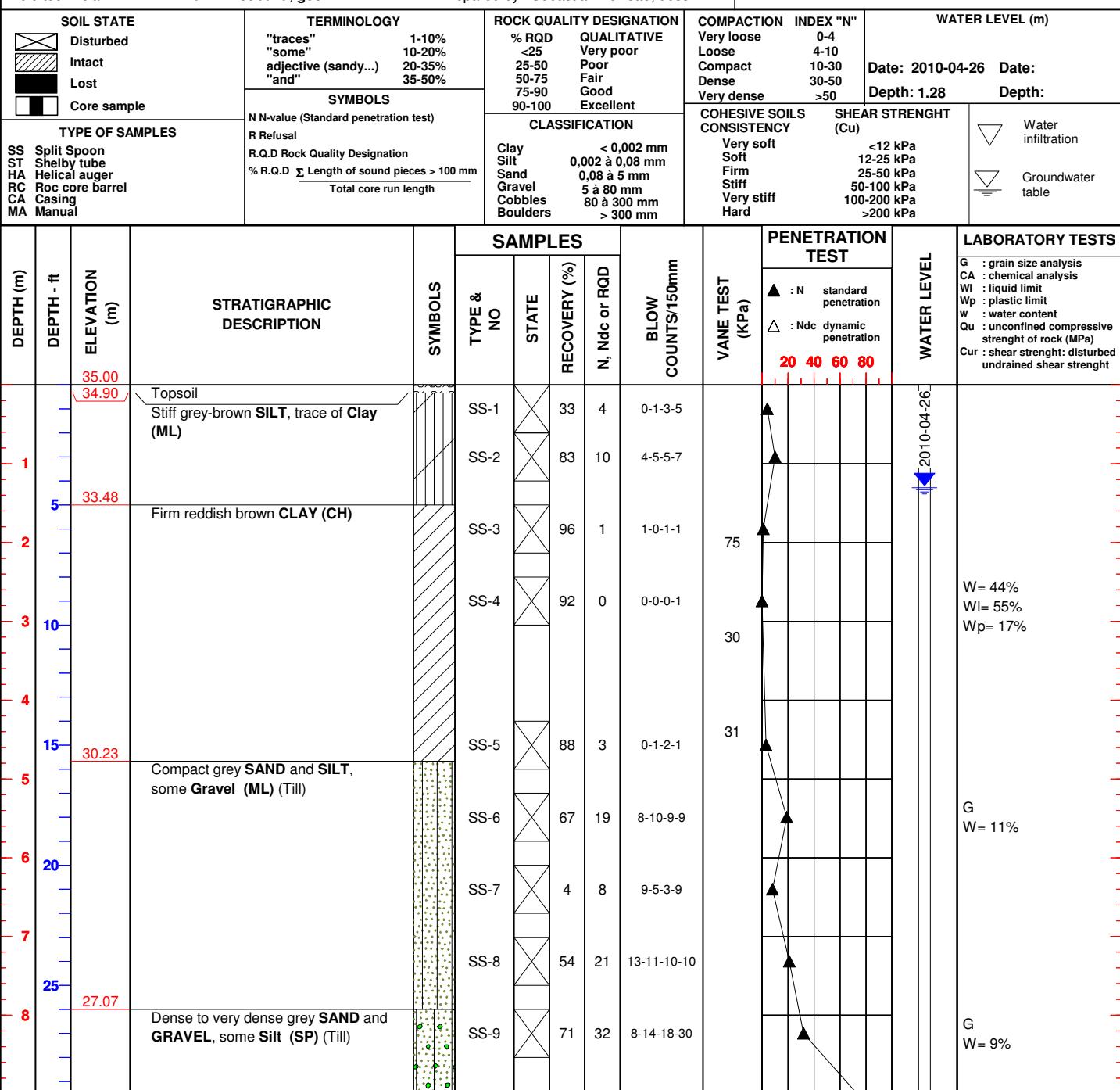
Prepared by : Sébastien Veillette, dess.



Remark(s):

Borehole N°
10BH-27

Project :	Wind Energy Converters (WEC)	O/F :	G1-09-1532
Client :	TRANSALTA		
Location :	Saint-Valentin, Québec	Geodesic coordinates (NAD-1983)	X: 319664 Y: 4996999
Drilling contractor :	Explora-sol inc.		
Drilling type :	Casing	Date of drilling :	2010-04-19
Diameter :	76,2 mm	Drilling depth (m) :	14.15
Field technician :	Karim Boudalja, géo.	Prepared by :	Sébastien Veillette, dess.



Remark(s):

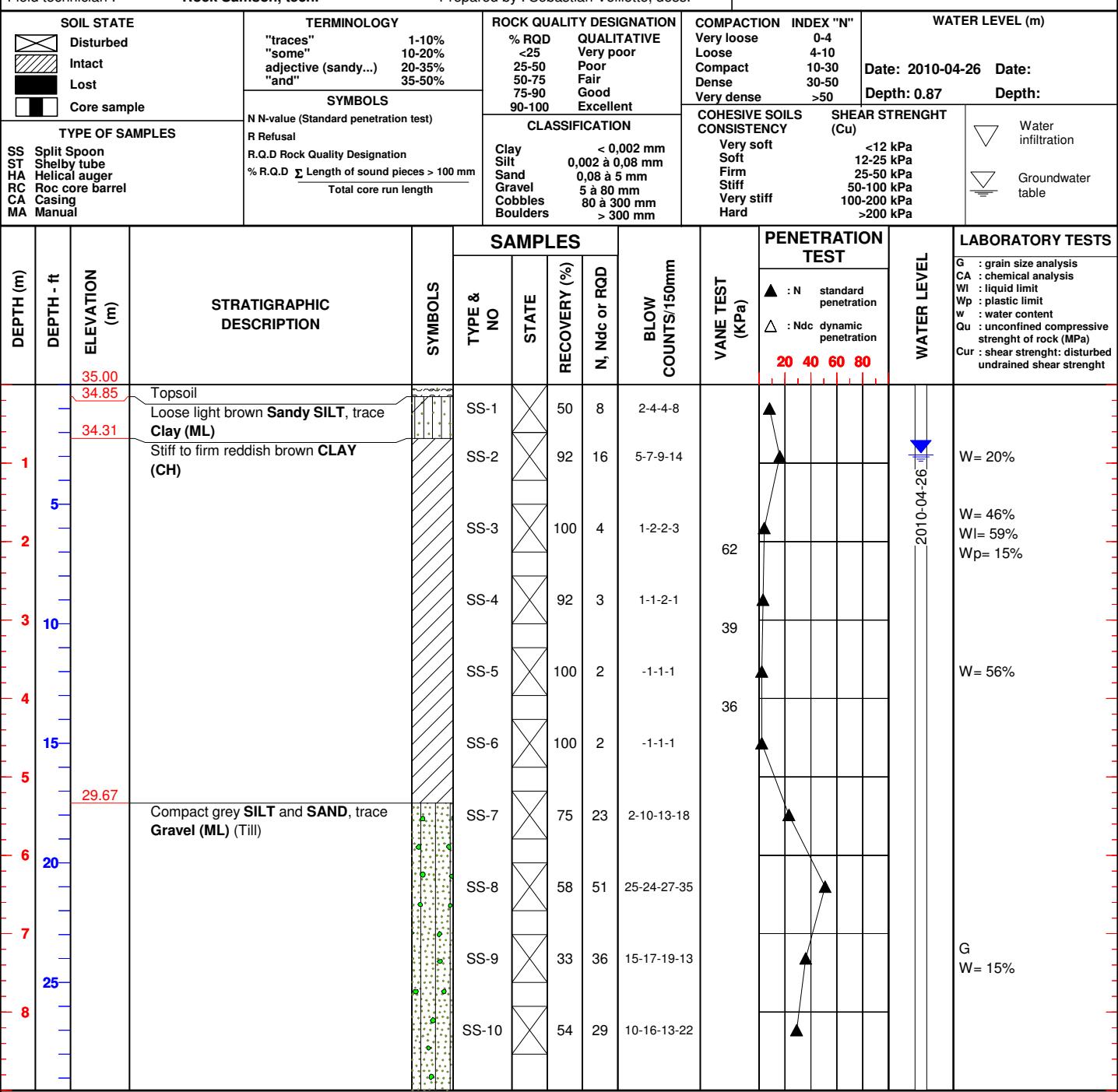
BOREHOLE REPORT

Borehole N°
10BH-27

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)			
10										
24.48										
35			Bedrock: Black LIMESTONE, fair to excellent quality		SS-10		83	97	26-49-48-50 / 13 cm	
40					SS-11		75		-50 / 10 cm	
45					RC-12		92	56		
20.85			END OF BOREHOLE		RC-13		100	100		
50					RC-14		97	70		
55										Qu= 109
60										
65										
70										
75										
80										
85										
90										
95										
100										
105										
110										
115										
120										
125										
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185										
190										
195										
200										
205										
210										
215										
220										
225										
230										
235										
240										
245										
250										

Borehole N°
10BH-28

Project :	Wind Energy Converters (WEC)	O/F :	G1-09-1532
Client :	TRANSALTA		
Location :	Saint-Valentin, Québec	Geodesic coordinates (NAD-1983)	X: 319665 Y: 4997492
Drilling contractor :	Explora-sol inc.		
Drilling type :	Casing	Date of drilling :	2010-04-15
Diameter :	76,2 mm	Drilling depth (m) :	13.72
Field technician :	Rock Samson, tech.	Prepared by : Sébastien Veillette, dess.	



BOREHOLE REPORT

Borehole N°

10BH-28

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			N, Ndc or RQD	BLOW COUNTS/150mm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)						
25.78			Cobbles and Boulders		SS-11		13		-50 / 8 cm				
24.33			Bedrock: Black LIMESTONE, poor quality		RC-12		30						
21.28			END OF BOREHOLE		RC-13		100	13					Qu= 80
					RC-14		100	35					
25													

Borehole N°
10BH-28A

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **319414**
 Y: **4997499**

 Drilling contractor : **Explora-sol inc.**

 Date of drilling : **2010-04-15**

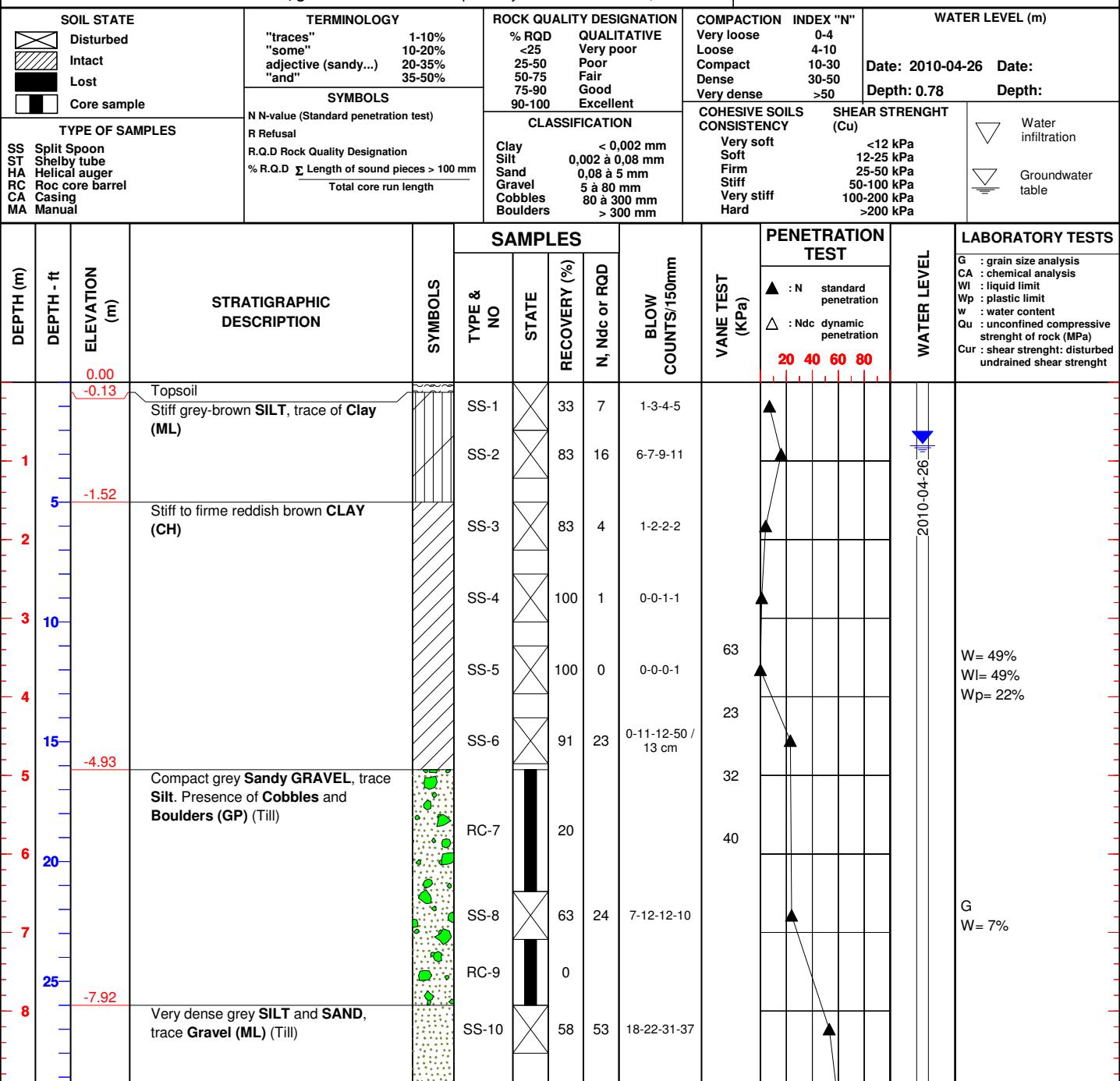
 Drilling type : **Casing**

 Drilling depth (m) : **15.22**

 Diameter : **76,2 mm**

 Field technician : **Karim Boudalja, géo.**

Prepared by : Sébastien Veillette, dess.



Remark(s):

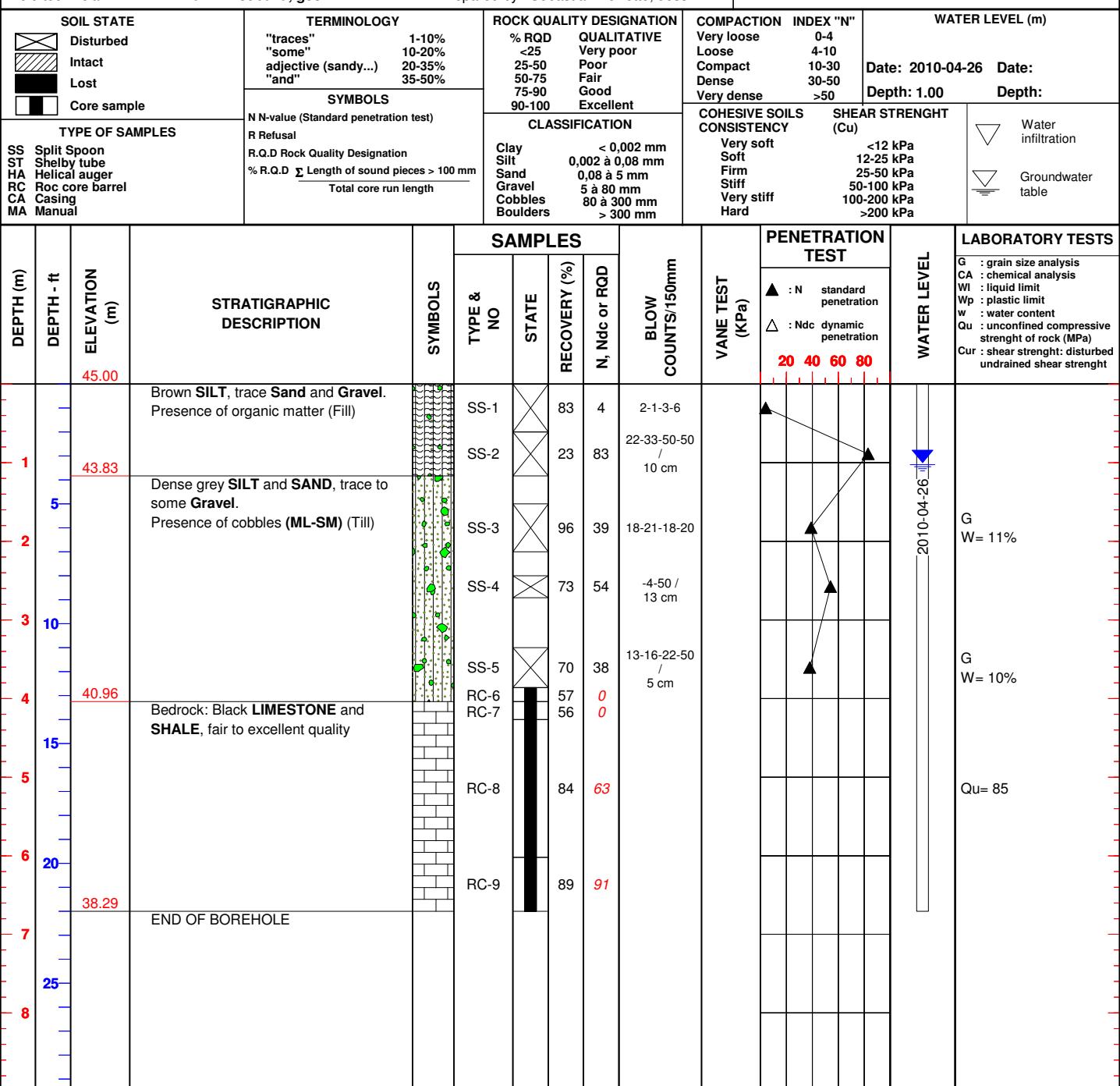
BOREHOLE REPORT

Borehole N°
10BH-28A

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			N, Ndc or RQD	BLOW COUNTS/150mm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS	
					TYPE & NO	STATE	RECOVERY (%)							
-10					SS-11		67	62	15-32-30-31					G W = 14%
-11					SS-12		96	58	15-24-34-44					
-12	-35	-11.91	Bedrock: Black LIMESTONE, poor to excellent quality		SS-13		0			-50 / 3 cm				
-13	-40				RC-14		88	43						Qu = 103
-14	-45				RC-15		100	60						
-15	-50	-15.22	FIN DU FORAGE		RC-16		94	91						
-16														
-17														
-18														
-19														
-20														
-21														
-22														
-23														
-24														
-25														

Borehole N°
10BH-29

Project :	Wind Energy Converters (WEC)	O/F :	G1-09-1532
Client :	TRANSALTA		
Location :	Saint-Valentin, Québec	Geodesic coordinates (NAD-1983)	X: 319828 Y: 5002096
Drilling contractor :	Explora-sol inc.		
Drilling type :	Casing	Date of drilling :	2010-03-25
Diameter :	76,2 mm	Drilling depth (m) :	6.71
Field technician :	Karim Boudalja, géo.	Prepared by :	Sébastien Veillette, dess.



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Remark(s):

Borehole N°
10BH-30

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **320091**
 Y: **5001646**

 Drilling contractor : **Explora-sol inc.**

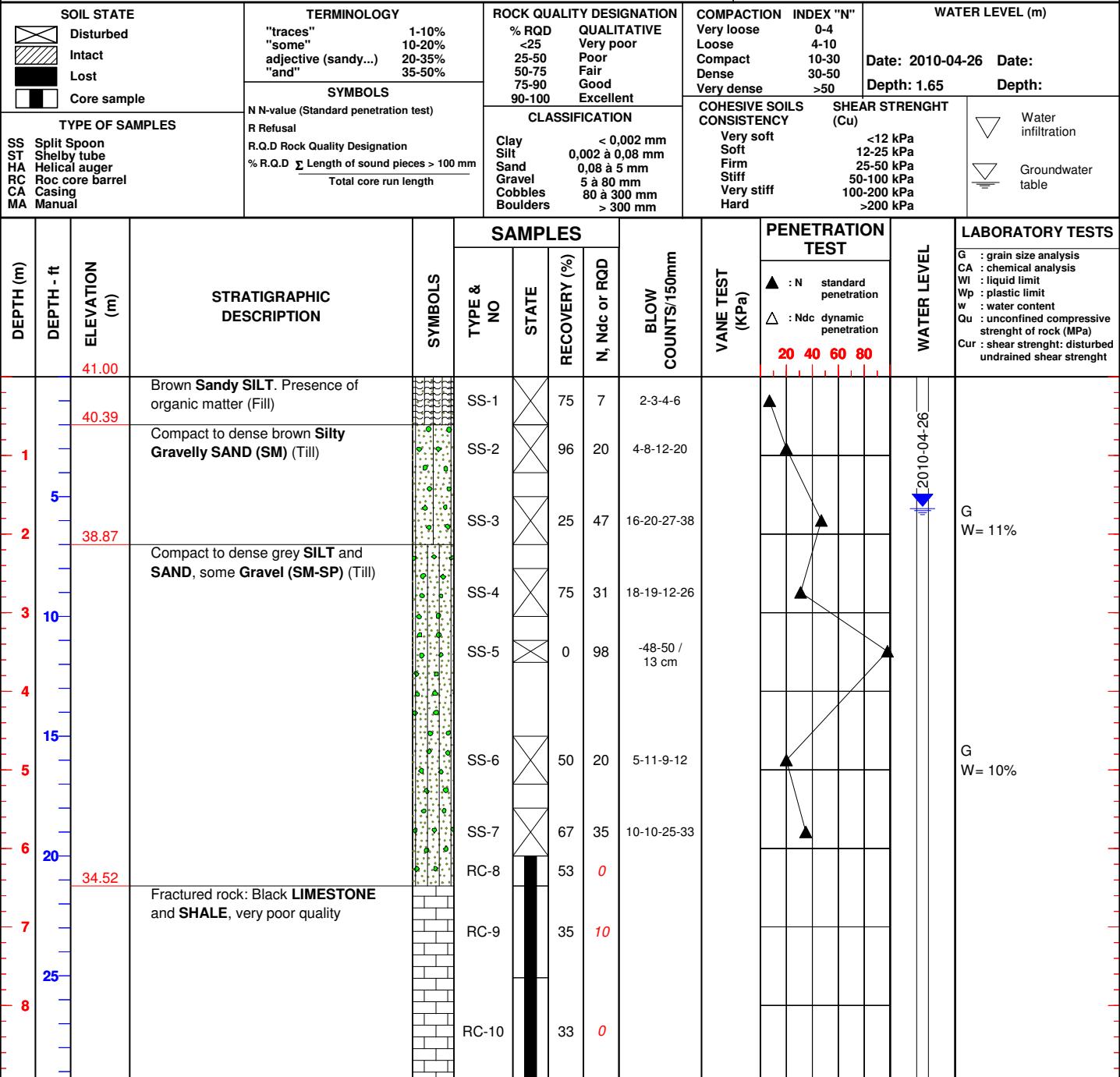
 Drilling type : **Casing**

 Diameter : **76,2 mm**

 Date of drilling : **2010-03-22**

 Field technician : **Karim Boudalia, géo.**

Prepared by : Sébastien Veillette, dess.

 Drilling depth (m) : **13.23**


Remark(s):

BOREHOLE REPORT

Borehole N°
10BH-30

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES		RECOVERY (%)	N, Ndc or RQD	BLOW COUNTS/150mm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE							
10					RC-11		60	0					
11					RC-12		61	0					
12					RC-13		43	0					
13					RC-14		55	0					
14					RC-15		75	0					
15					RC-16		71	10					
16													
17													
18													
19													
20													
21													
22													
23													
24													
25													
		27.77	END OF BOREHOLE										

Borehole N°
10BH-31

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **320095**
 Y: **4997479**

 Drilling contractor : **Explora-sol inc.**

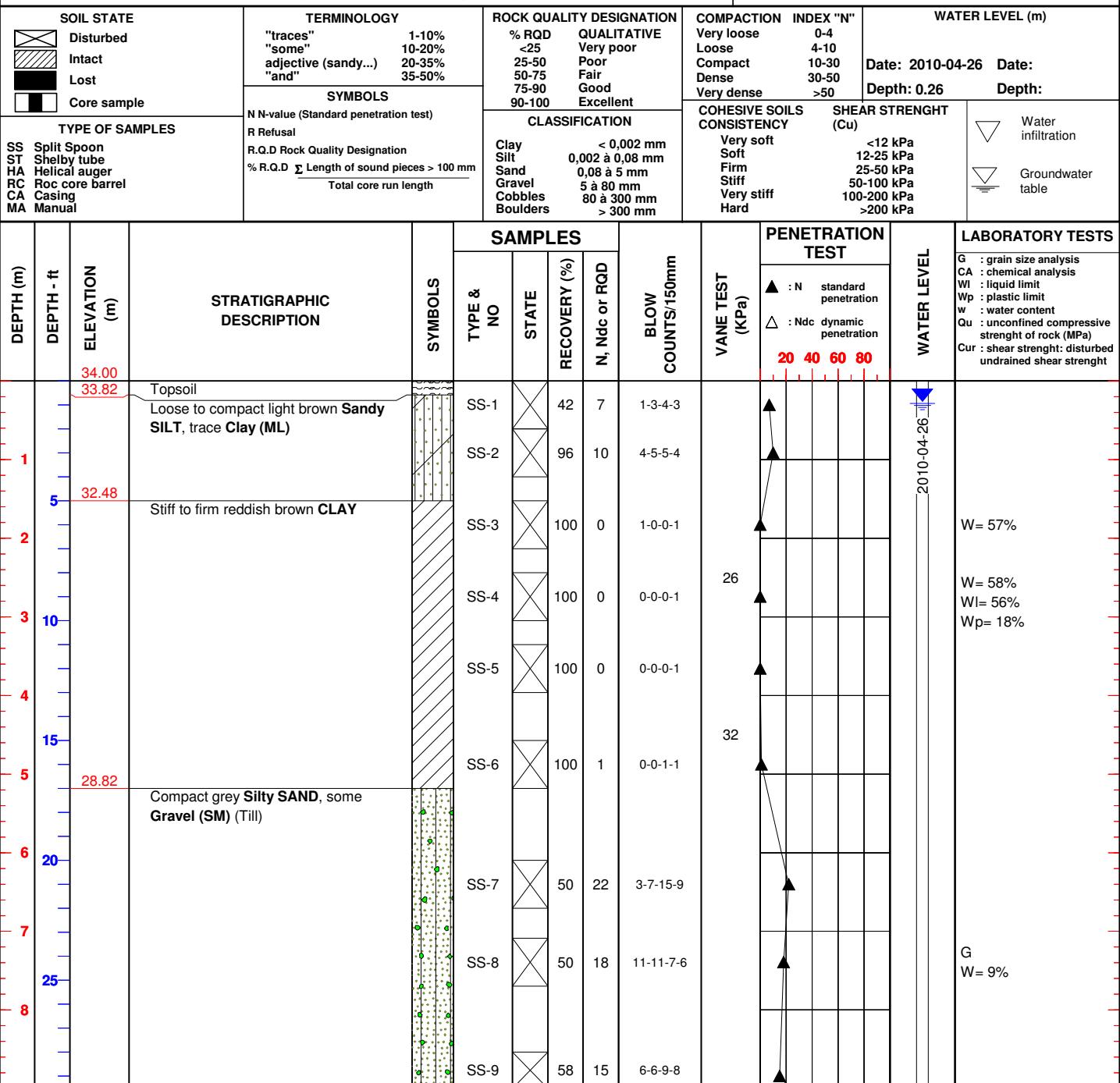
 Date of drilling : **2010-04-14**

 Drilling type : **Casing**
 Diameter : **76,2 mm**

 Drilling depth (m) : **15.04**

 Field technician : **Karim Boudalja, géo.**

Prepared by : Sébastien Veillette, dess.



Remark(s):

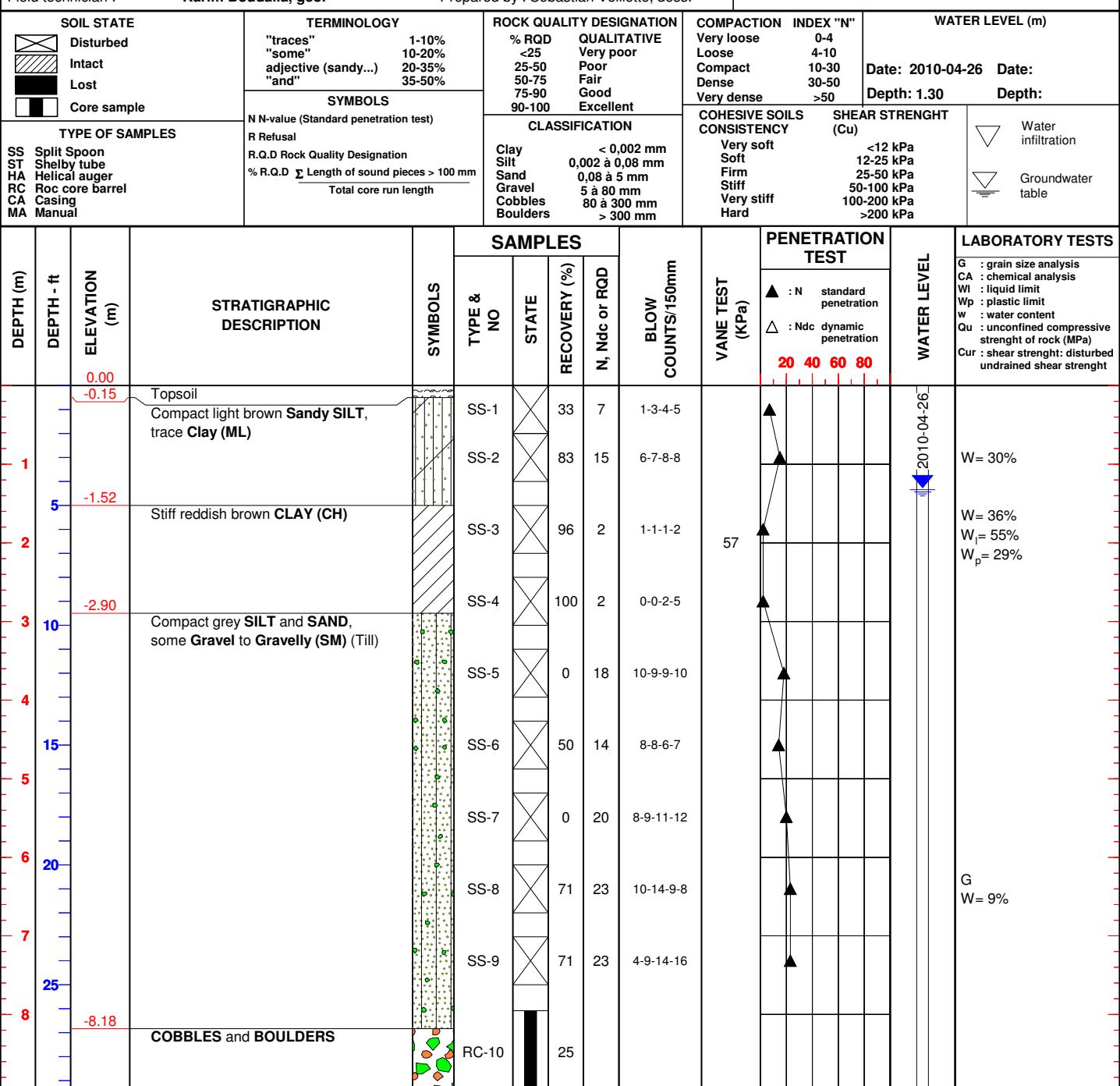
BOREHOLE REPORT

Borehole N°
10BH-31

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			RECOVERY (%)	N, Ndc or RQD	BLOW COUNTS/150mm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)							
24.55			Very dense grey Gravelly SAND, trace Silt. Presence of Cobbles (SP) (Till)		SS-10		83	59	26-30-29-32					
10					SS-11		50			-50 / 15 cm				
35					RC-12		82	60						
11					RC-13		69	51						
22.34			Bedrock: Black LIMESTONE, fair to excellent quality		RC-14		95	97						Qu= 82
12														
40														
13														
45														
14														
15		18.96	FIN DU FORAGE											
16														
17														
18														
19														
20														
21														
22														
23														
24														
25														

Borehole N°
10BH-31A

Project :	Wind Energy Converters (WEC)	O/F :	G1-09-1532
Client :	TRANSALTA		
Location :	Saint-Valentin, Québec	Geodesic coordinates (NAD-1983)	X: 319926 Y: 4997484
Drilling contractor :	Explora-sol inc.		
Drilling type :	Casing	Date of drilling :	2010-04-14
Diameter :	76,2 mm	Drilling depth (m) :	15.57
Field technician :	Karim Boudalia, géo.	Prepared by :	Sébastien Veillette, dess.



BOREHOLE REPORT

Borehole N°
10BH-31A

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			N, Ndc or RQD	BLOW COUNTS/150mm	VANE TEST (kPa)	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)						
-10													
35													
11													
12													
40													
-12.60			Bedrock: Black LIMESTONE, good to excellent quality										
13													
45													
14													
15													
50													
-15.57			FIN DU FORAGE										
16													
55													
17													
60													
18													
65													
20													
21													
70													
22													
75													
23													
80													
24													
85													
25													

Borehole N°
10BH-32

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **320241**
 Y: **5002214**

 Drilling contractor : **Explora-sol inc.**

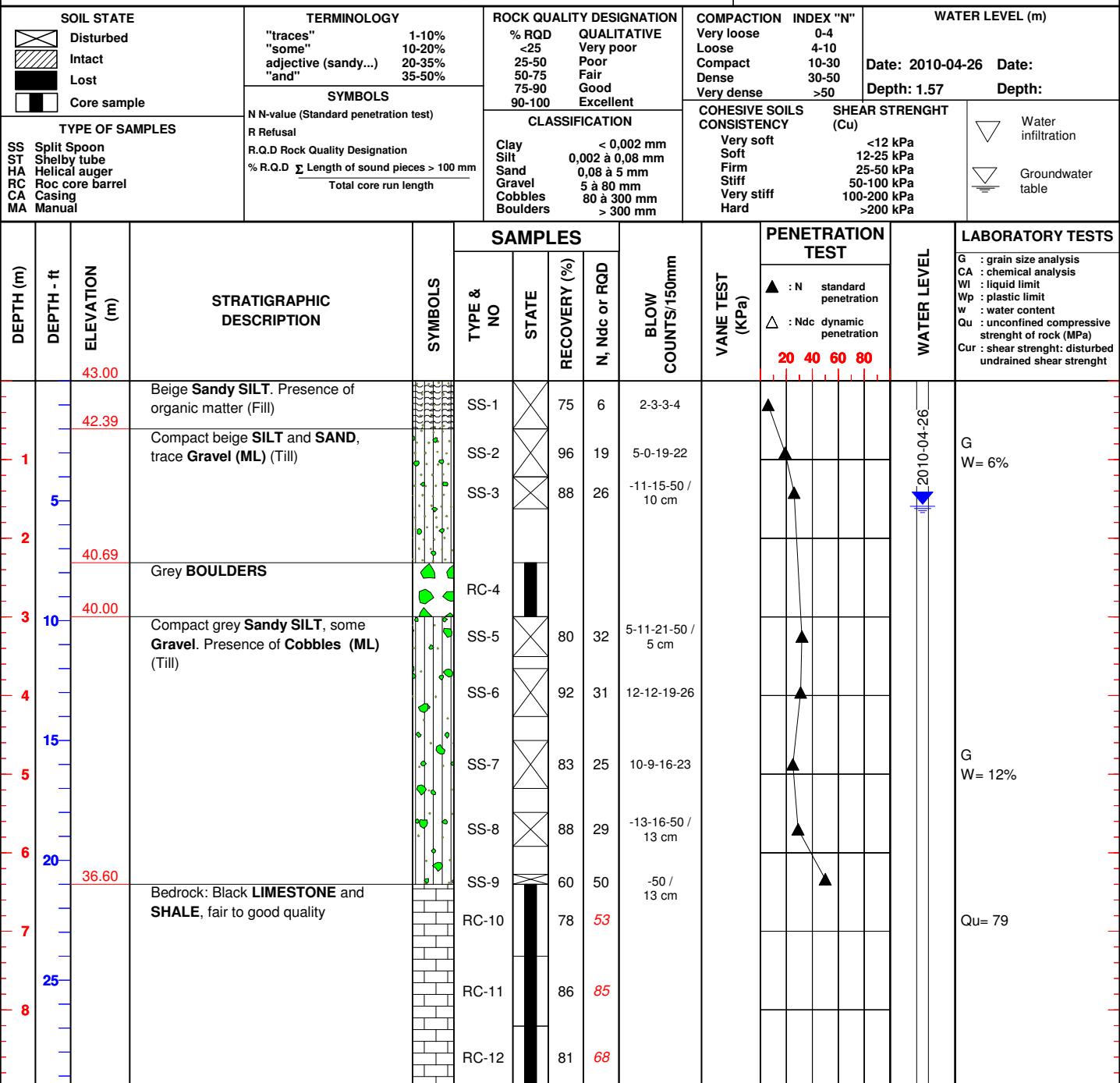
 Date of drilling : **2010-03-24**

 Drilling type : **Casing**
 Diameter : **76,2 mm**

 Drilling depth (m) : **9.53**

 Field technician : **Karim Boudalia, géo.**

Prepared by : Sébastien Veillette, dess.



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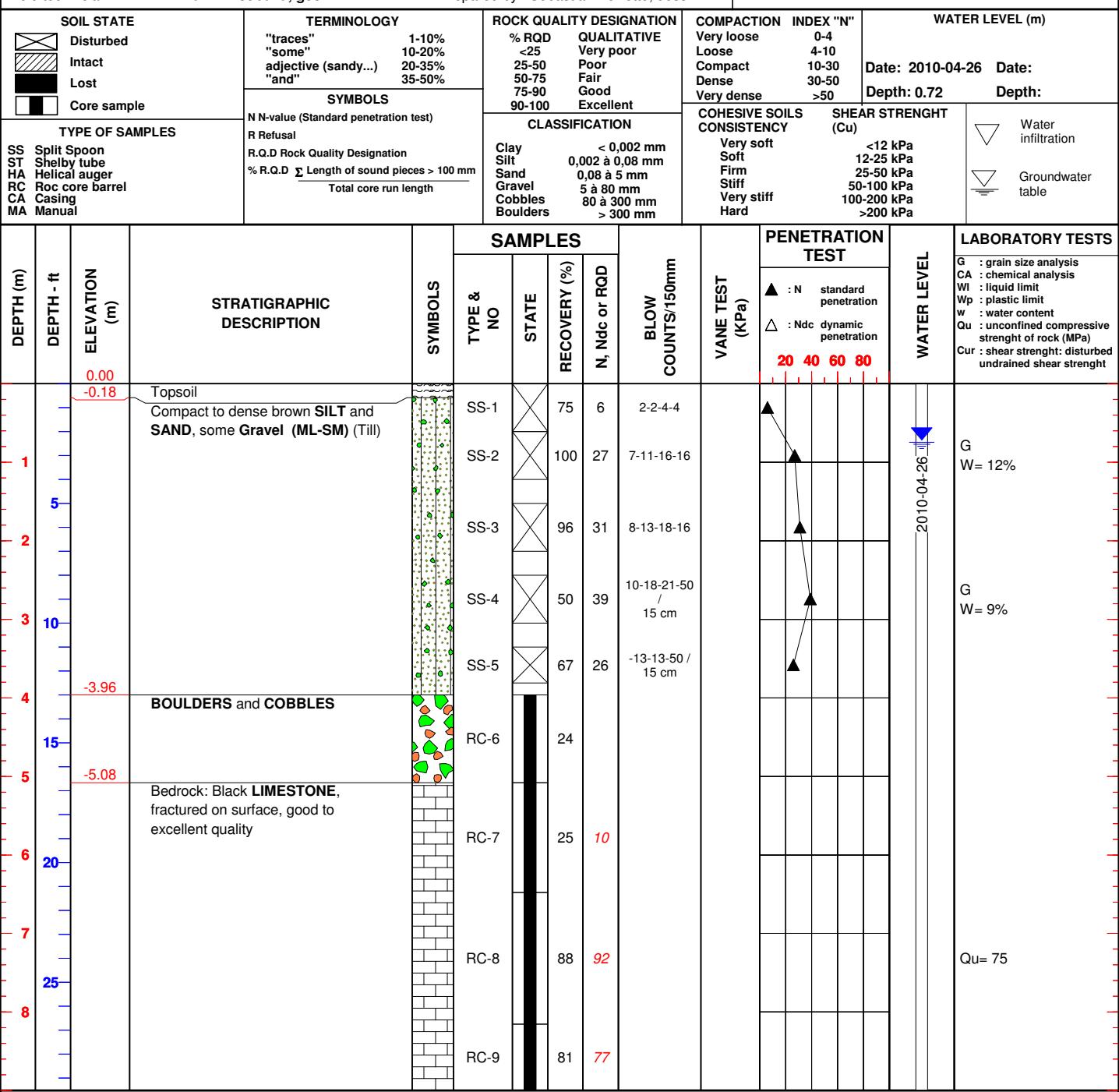
BOREHOLE REPORT

Borehole N°
10BH-32

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			RECOVERY (%)	N, Ndc or RQD	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)					
33.48			END OF BOREHOLE									
10												
11												
12												
13												
14												
15												
16												
17												
18												
19												
20												
21												
22												
23												
24												
25												

Borehole N°
10BH-34

Project :	Wind Energy Converters (WEC)	O/F :	G1-09-1532
Client :	TRANSALTA		
Location :	Saint-Valentin, Québec	Geodesic coordinates (NAD-1983)	X: 319415 Y: 5002922
Drilling contractor :	Explora-sol inc.		
Drilling type :	Casing	Date of drilling :	2010-04-08
Diameter :	76.2 mm	Drilling depth (m) :	9.73
Field technician :	Karim Boudalia, géo.	Prepared by :	Sébastien Veillette, dess.



BOREHOLE REPORT

Borehole N°
10BH-34

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			RECOVERY (%)	N, Ndc or RQD	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)					
-9.73			END OF BOREHOLE							▲ : N standard penetration △ : Ndc dynamic penetration 20 40 60 80		
10												
11												
12												
13												
14												
15												
16												
17												
18												
19												
20												
21												
22												
23												
24												
25												

Borehole N°

10BH-35

 Project : **Wind Energy Converters (WEC)**

 O/F : **G1-09-1532**

 Client : **TRANSALTA**

 Location : **Saint-Valentin, Québec**

 Geodesic coordinates (NAD-1983) X: **319169**
Y: **5002673**

 Drilling contractor : **Explora-sol inc.**

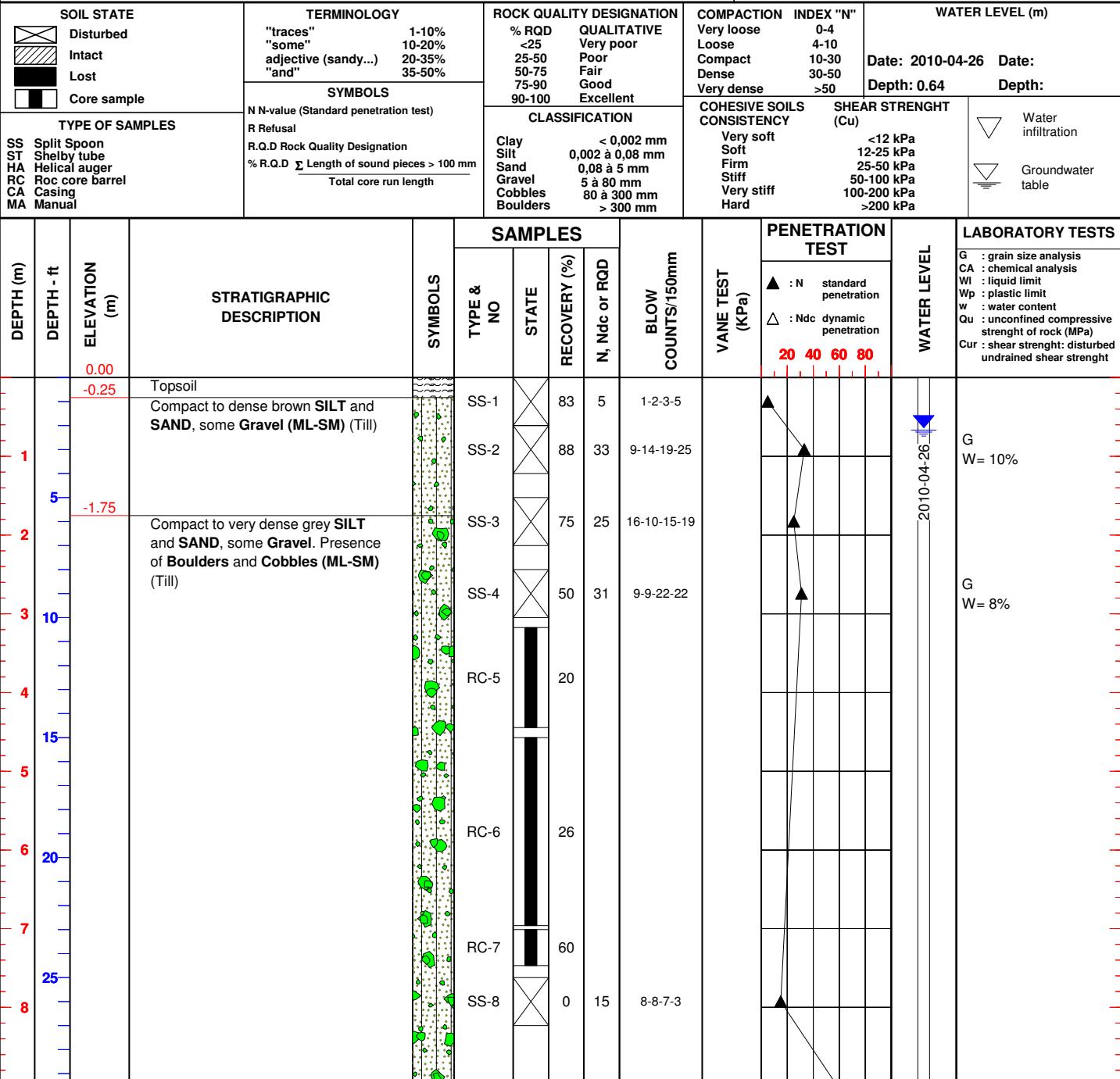
 Date of drilling : **2010-04-08**

 Drilling type : **Casing**
Diameter : **76,2 mm**

 Drilling depth (m) : **14.17**

 Field technician : **Karim Boudalja, géo.**

Prepared by : Sébastien Veillette, dess.



Remark(s):

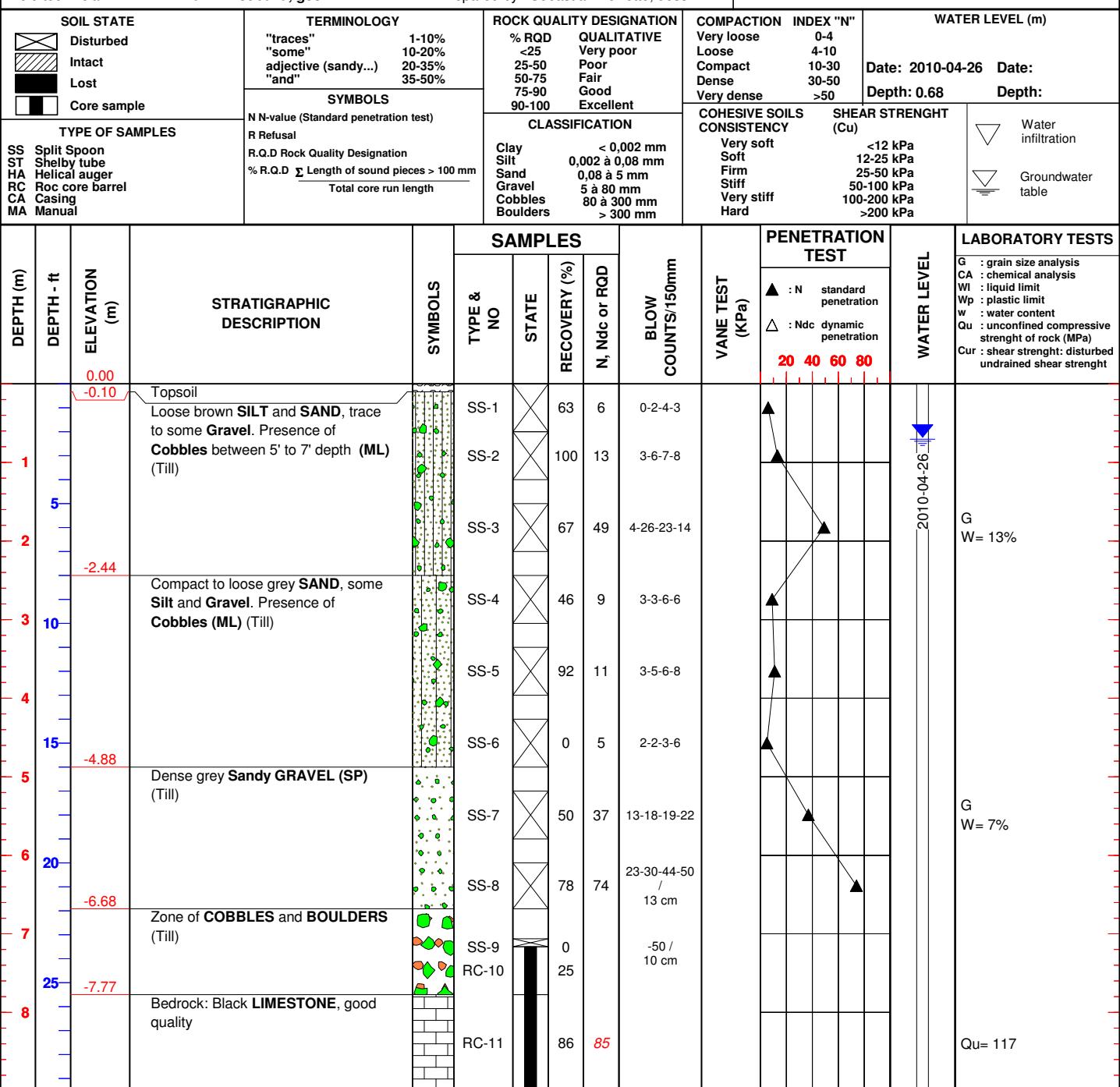
BOREHOLE REPORT

Borehole N°
10BH-35

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)			
-10					SS-9		88	77	22-38-39-37	
35	-10.85				SS-10		86	78	-28-50 / 3 cm	
40			Bedrock: Black LIMESTONE, fair to excellent quality		RC-11		77	55		
45					RC-12		97	100		
11					RC-13		94	93		
12										
13										
14										
15										
16										
17										
18										
19										
20										
21										
22										
23										
24										
25			END OF BOREHOLE							
										Qu= 76

Borehole N°
10BH-37

Project : Wind Energy Converters (WEC)		O/F : G1-09-1532
Client : TRANSALTA		
Location :	Saint-Valentin, Québec	Geodesic coordinates (NAD-1983) X: 318483 Y: 5001515
Drilling contractor :	Explora-sol inc.	Date of drilling : 2010-04-23
Drilling type :	Casing	Drilling depth (m) : 10.52
Diameter :	76,2 mm	
Field technician :	Karim Boudalia, géo.	Prepared by : Sébastien Veillette, dess.



Remark(s):

BOREHOLE REPORT

Borehole N°
10BH-37

DEPTH (m)	DEPTH - ft	ELEVATION (m)	STRATIGRAPHIC DESCRIPTION	SYMBOLS	SAMPLES			RECOVERY (%)	N, Ndc or RQD	PENETRATION TEST	WATER LEVEL	LABORATORY TESTS
					TYPE & NO	STATE	RECOVERY (%)					
-10												
-10.52			END OF BOREHOLE		RC-12		92	87				
35												
40												
45												
50												
55												
60												
65												
70												
75												
80												
85												
90												
95												
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225												
230												
235												
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250												

Appendix D

Laboratory tests

SOIL PLASTICITY CHART

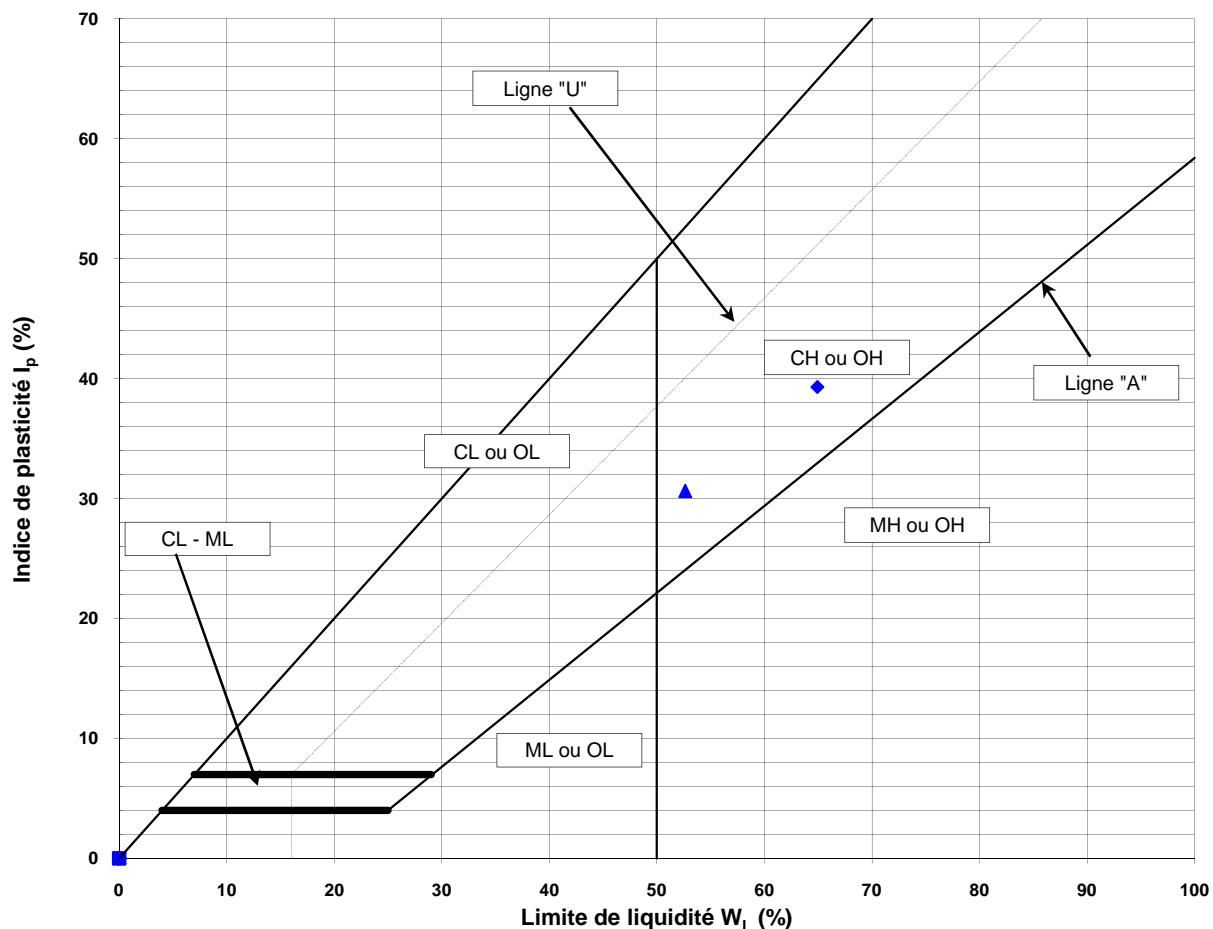
CLIENT TransAlta

N/D: G1-09-1532

PROJECT Geotechnical study - wind energy converters (WEC)

LOCATION St-Valentin, Québec

PAGE 1 de 1



Selon ASTM D-2487

RÉSULTATS

Legend	Boring	Simple n°	Depth (m)	W_n	W_L	W_p	I_p	I_L	Classification
▲	10BH-04	SS-04	2,44 - 3,05	64%	53%	22%	31%	1,4	CH
◆	10BH-12	SS-03	2,13 - 2,74	57%	65%	26%	39%	0,8	CH

SOIL PLASTICITY CHART

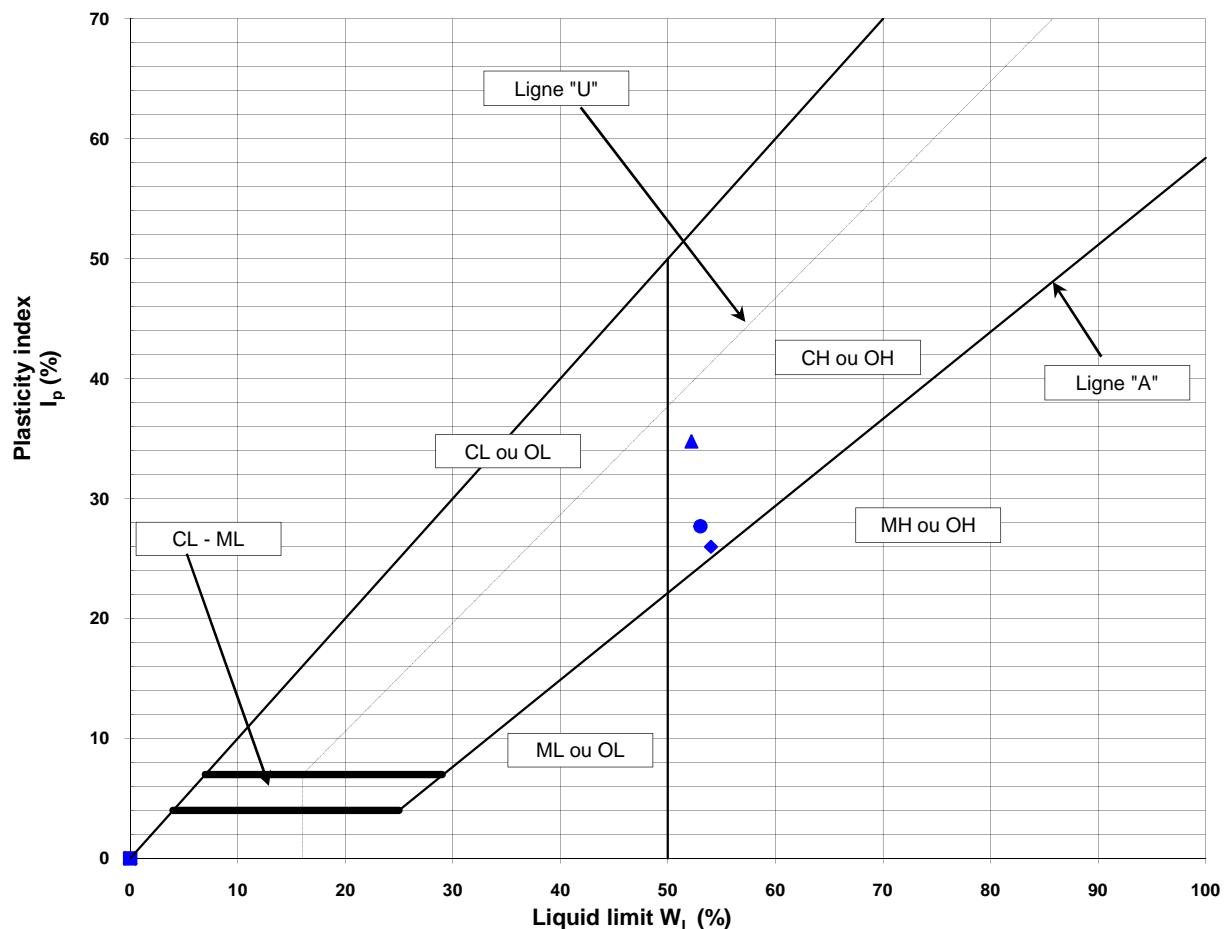
CLIENT TransAlta

N/D: G1-09-1532

PROJECT Geotechnical study - Wind energy converters (WEC)

LOCATION St-Valentin (Québec)

PAGE 1 de 1



according to ASTM D-2487

RESULTS INTERPRETATION

Legend	Boring	Sample n°	Depth (m)	W_n	W_L	W_p	I_p	I_L	Classification
▲	10BH-06	SS-03	1,52 - 2,13	56%	52%	17%	35%	1,1	CH
◆	10BH-25	SS-04	2,44 - 3,05	34%	54%	28%	26%	0,2	CH
●	10BH-11	SS-03	1,52 - 2,13	74%	53%	25%	28%	1,8	CH

Prepared by

Daniel Fleury, tech.

Approved by

Ibrahim Ja'far, ing.

Date 2010-04-08

SOIL PLASTICITY CHART

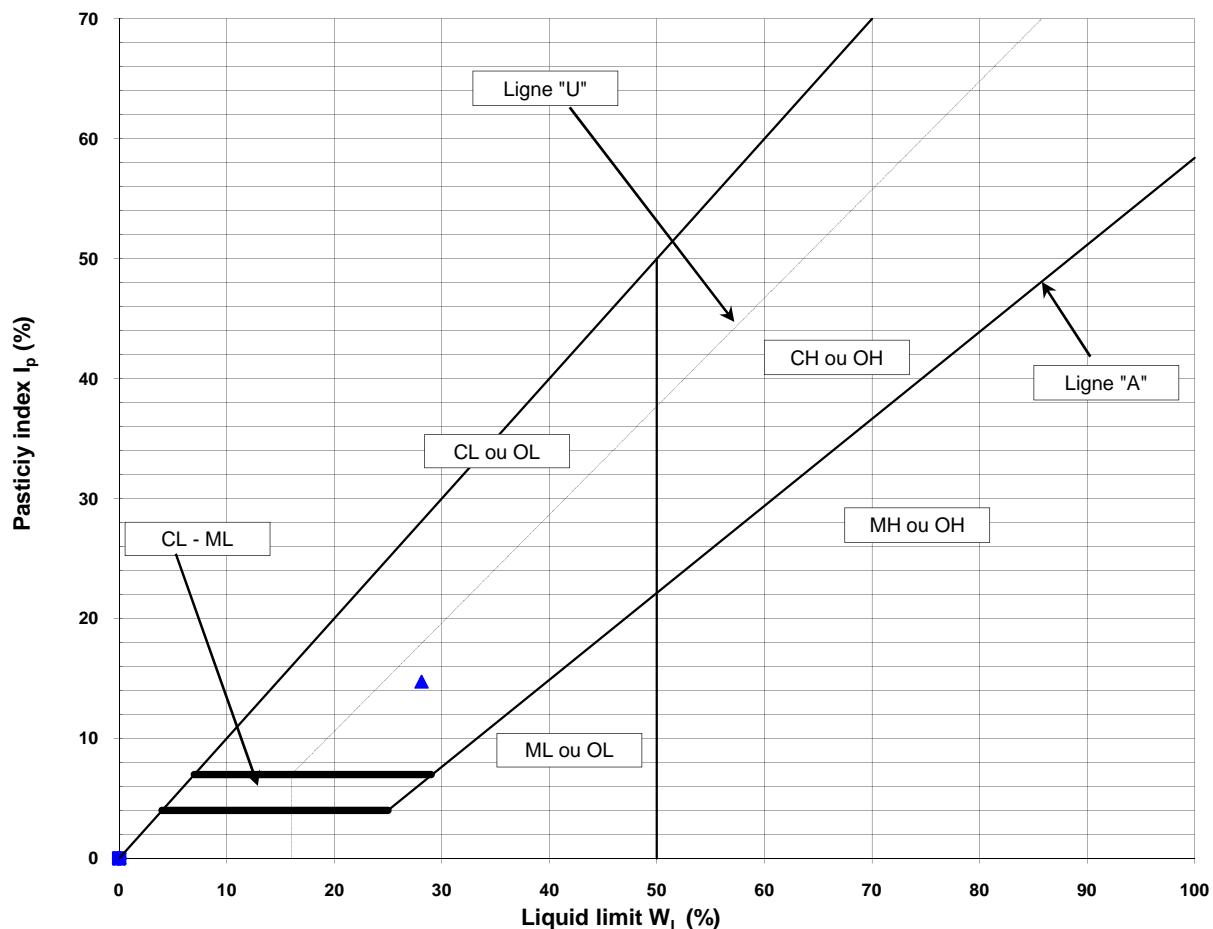
CLIENT TransAlta

N/D: G1-09-1532

PROJECT Geotechnical study - wind energy converters (WEC)

LOCATION St-Valentin (Québec)

PAGE 1 de 1



ACCORDING TO ASTM D-2487

RESULTS INTERPRETATION

Legend	Boring	Sample n°	Dept (m)	W_n	W_L	W_p	I_p	I_L	Classification
▲	10BH-17A	SS-03	1,52 - 2,13 m	52%	28%	13%	15%	2,6	CL

SOIL PLASTICITY CHART

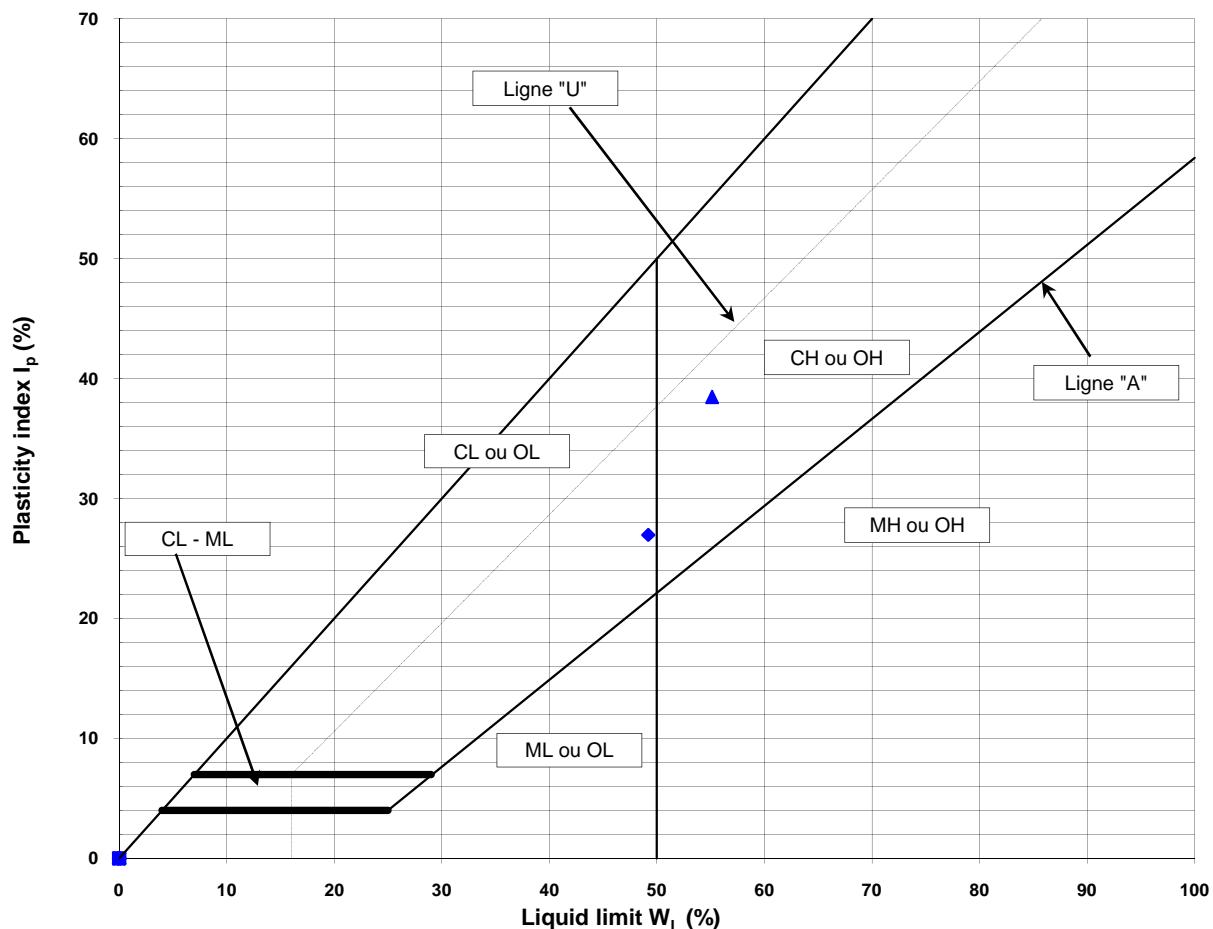
CLIENT TransAlta

N/D: G1-09-1532

PROJET Geotechnical study - Wind energy converters (WEC)

ENDROIT St-Valentin (Québec)

PAGE 1 de 1



according to ASTM D-2487

RESULTS INTERPRETATION

Legend	Boring	Sample n°	Depth (m)	W_n	W_L	W_p	I_p	I_L	Classification
▲	10BH-27	SS-04	2,44 - 3,05	44%	55%	17%	38%	0,7	CH
◆	10BH-28A	SS-05	3,35 - 3,96	49%	49%	22%	27%	1,0	CH

SOIL PLASTICITY CHART

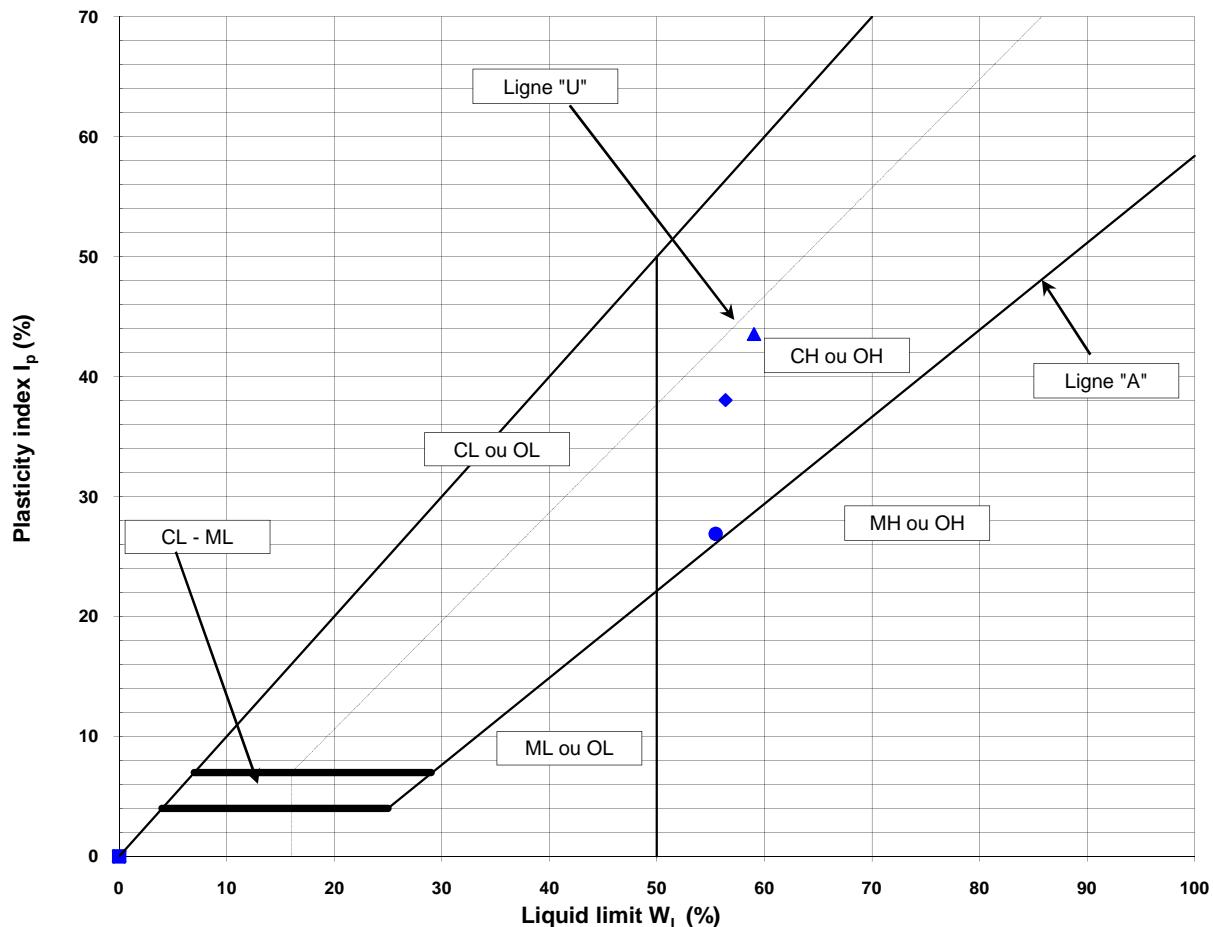
CLIENT TransAlta

N/D: G1-09-1532

PROJECT Geotechnical study - Wind energy converters (WEC)

LOCATION St-valentin (Québec)

PAGE 1 de 1

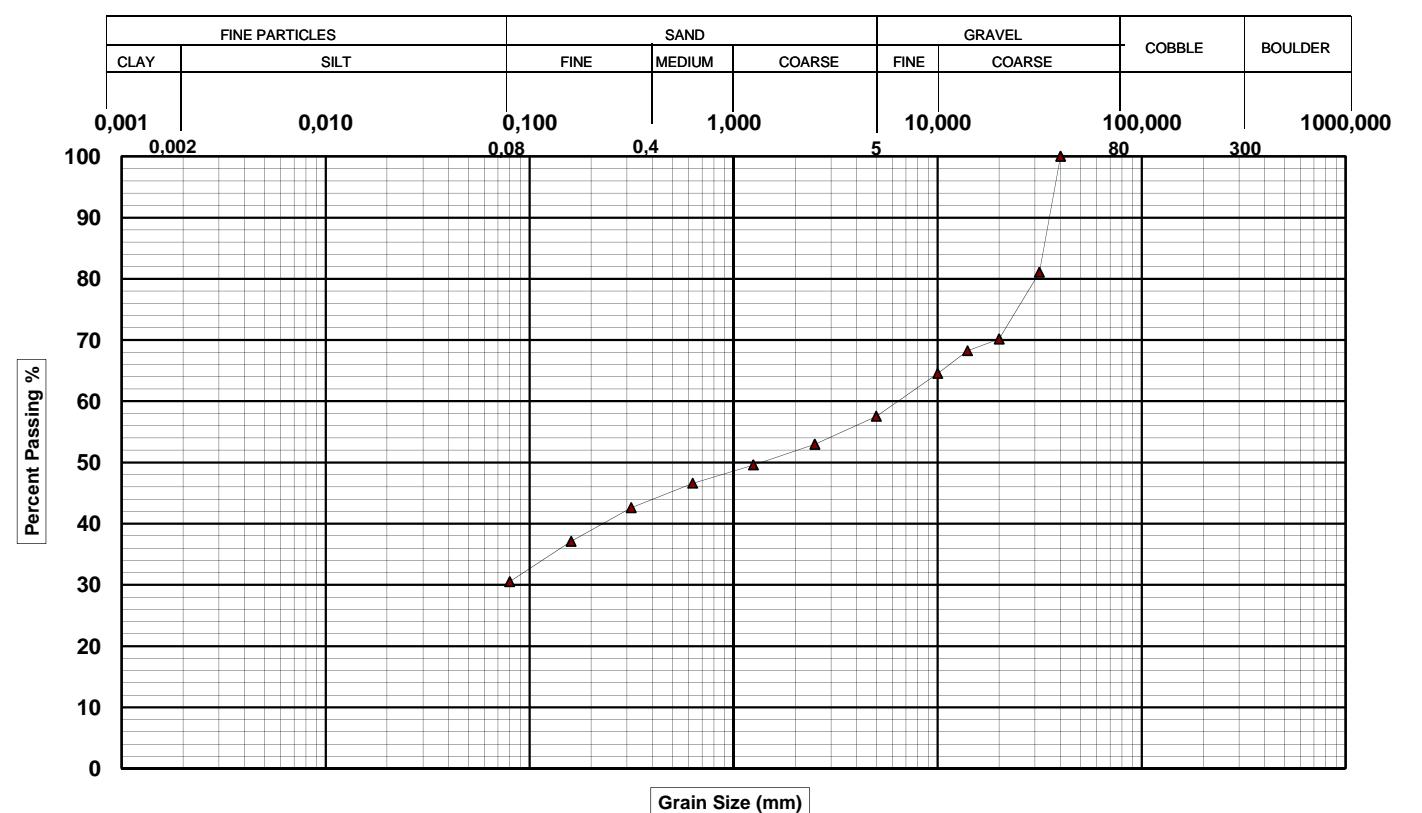


ACCORDING TO ASTM D-2487

RESULTS INTERPRETATION

Legend	Boring	Simple n°	Depth (m)	W_n	W_L	W_p	I_p	I_L	Classification
▲	10BH-28	SS-3	1,52 - 2,13	46%	59%	15%	44%	0,7	CH
◆	10BH-31	SS-04	2,44 - 3,05	58%	56%	18%	38%	1,0	CH
●	10BH-31A	SS-03	1,52 - 2,13	36%	55%	29%	27%	0,3	CH

CLIENT	TransAlta	N/D G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)	
LOCATION	St-Valentin, Québec	NO. LAB. 36370



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	30,5	27,0	42,5	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	6,50	N/A	N/A	6

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	53		
56,00	100	1,250	50		
40,00	100	0,630	47		
31,50	81	0,315	43		
20,00	70	0,160	37		
14,00	68	0,080	30,5		
10,00	65				
5,00	58				

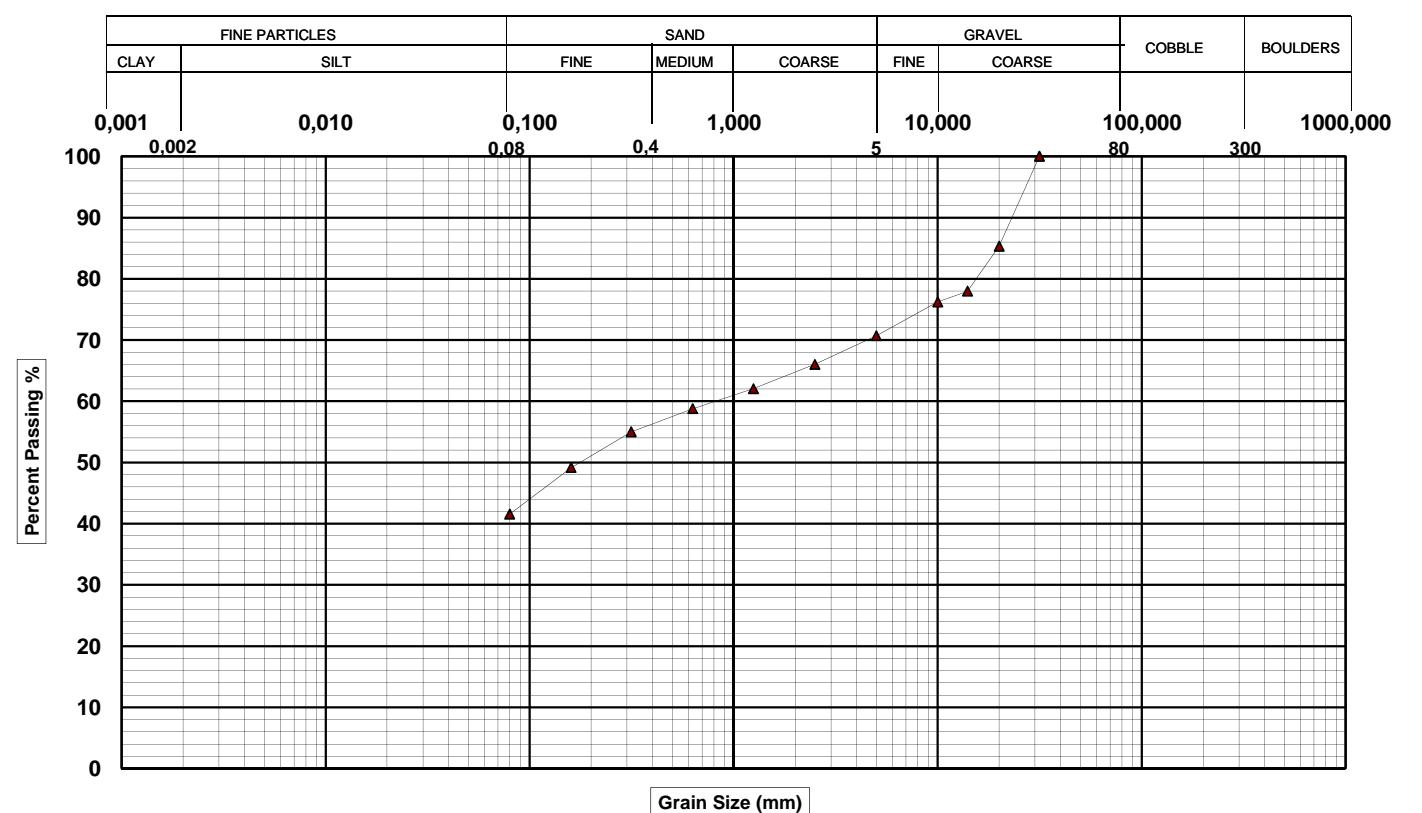
SAMPLE IDENTIFICATION										
Sample	10BH-04 (SS-10)									
Depth	7,92 - 8,53 m									
Soil Description										
Sandy silty gravel										

Prepared by Benoit St-Pierre, tech.

Approved by Ibrahim Ja'far, ing.

Date 2010-04-01

CLIENT	TransAlta	N/D G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)	
LOCATION	St-Valentin, Québec	NO. LAB. 36373



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	41,6	29,1	29,3	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,84	N/A	N/A	9

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	66		
56,00	100	1,250	62		
40,00	100	0,630	59		
31,50	100	0,315	55		
20,00	85	0,160	49		
14,00	78	0,080	41,6		
10,00	76				
5,00	71				

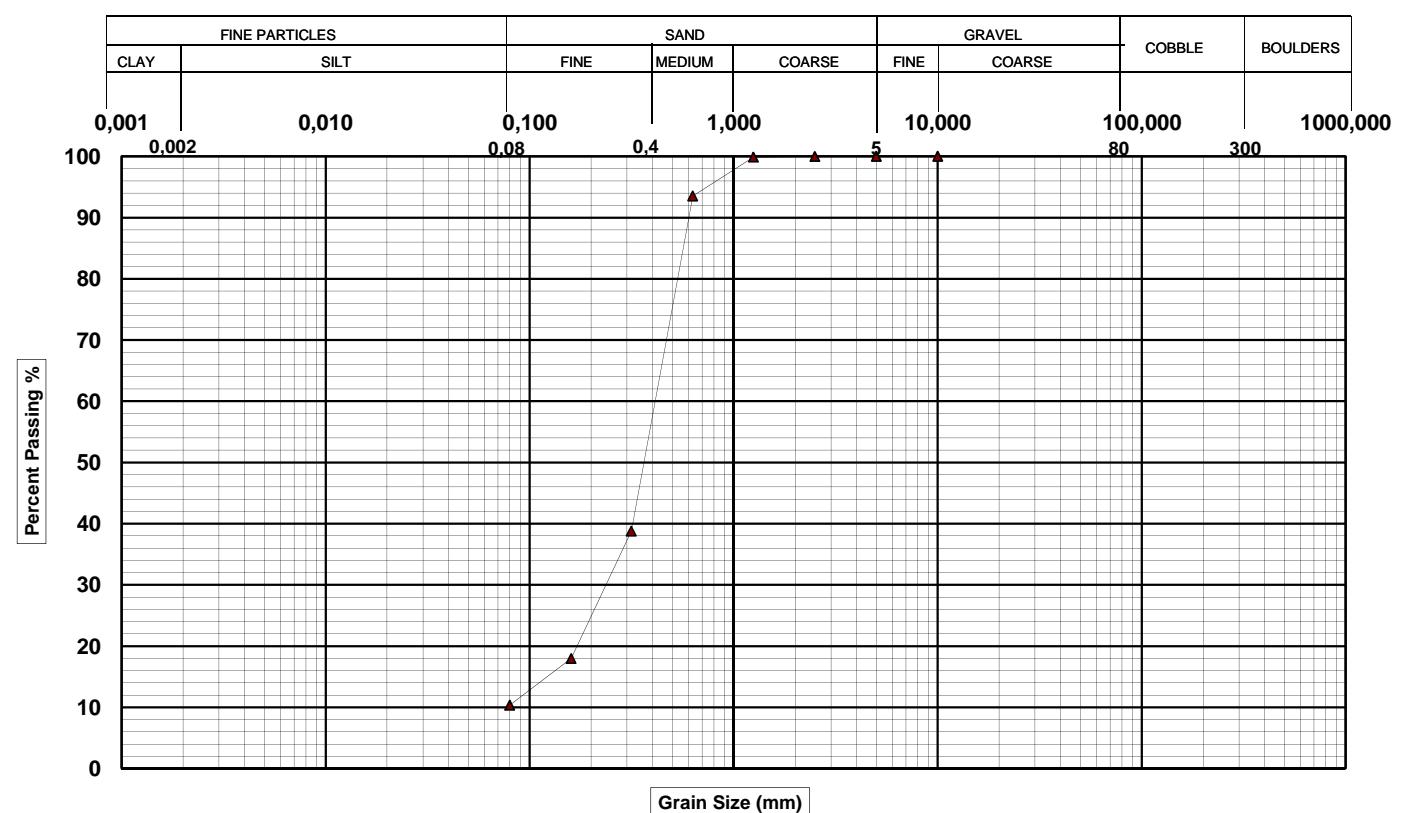
SAMPLE IDENTIFICATION										
Sample	10BH-12 (SS-10)									
Depth	8,53 - 9,14 m									
Soil Description										
Gravelly sandy Silt										

Prepared by Benoit St-Pierre, tech.

Approved by Ibrahim Ja'far, ing.

Date 2010-04-01

CLIENT	TransAlta	N/D G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)	
LOCATION	St-Valentin, Québec	NO. LAB. 36375



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	10,4	89,6	0,0	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	0,24	0,41	N/A	N/A	17

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	100		
56,00	100	1,250	100		
40,00	100	0,630	94		
31,50	100	0,315	39		
20,00	100	0,160	18		
14,00	100	0,080	10,4		
10,00	100				
5,00	100				

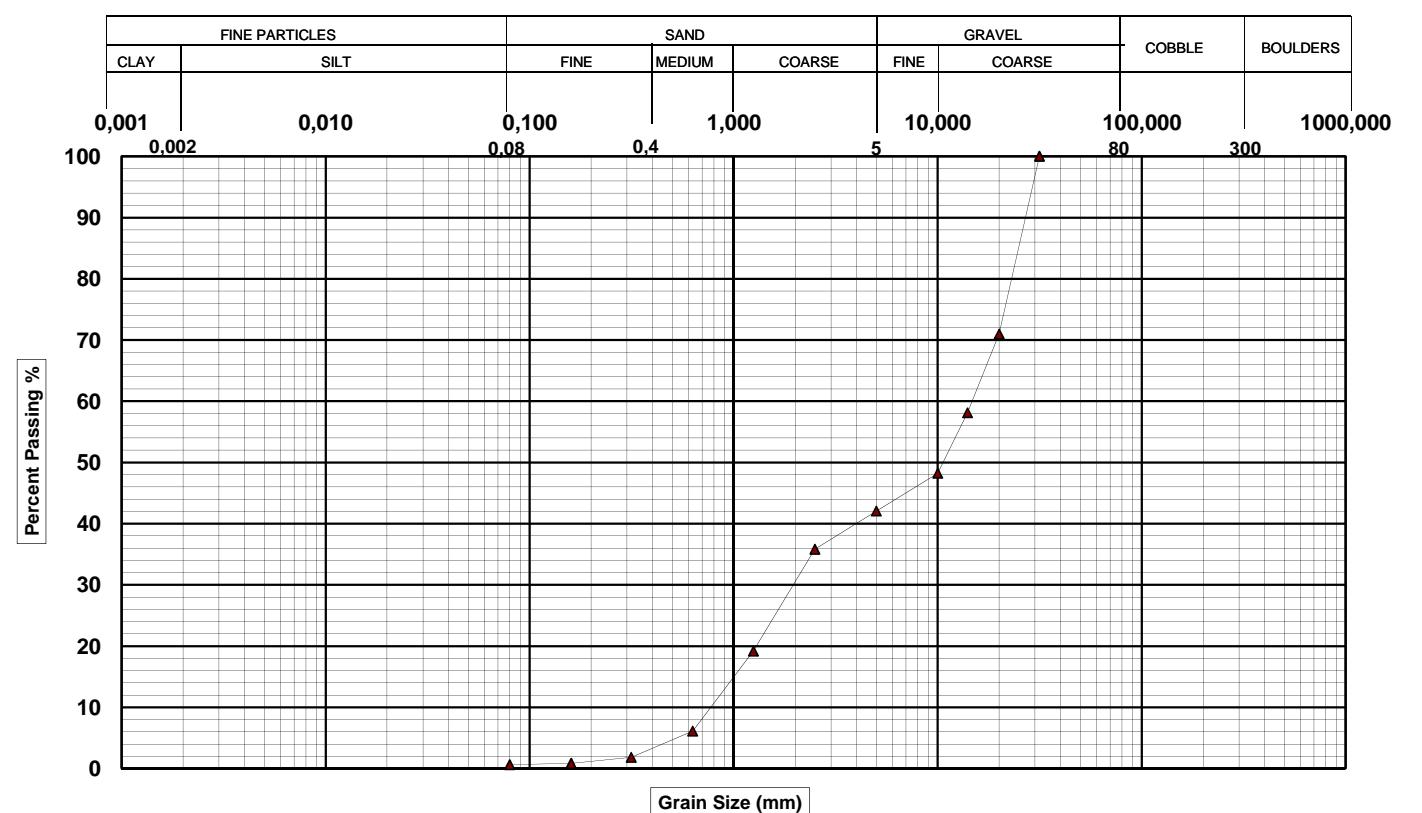
SAMPLE IDENTIFICATION										
Sample	10BH-14 (SS-05)									
Depth	3,35 - 3,96 m									
Soil Description										
Sand, some of silt										

Prepared by Benoit St-Pierre, tech.

Approved by Ibrahim Ja'far, ing.

Date 2010-04-01

CLIENT	TransAlta	N/D G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)	
LOCATION	St-Valentin, Québec	NO. LAB. 36376



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	0,6	41,4	57,9	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
0,800	2,00	16,00	20,00	0,31	10

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	36		
56,00	100	1,250	19		
40,00	100	0,630	6		
31,50	100	0,315	2		
20,00	71	0,160	1		
14,00	58	0,080	0,6		
10,00	48				
5,00	42				

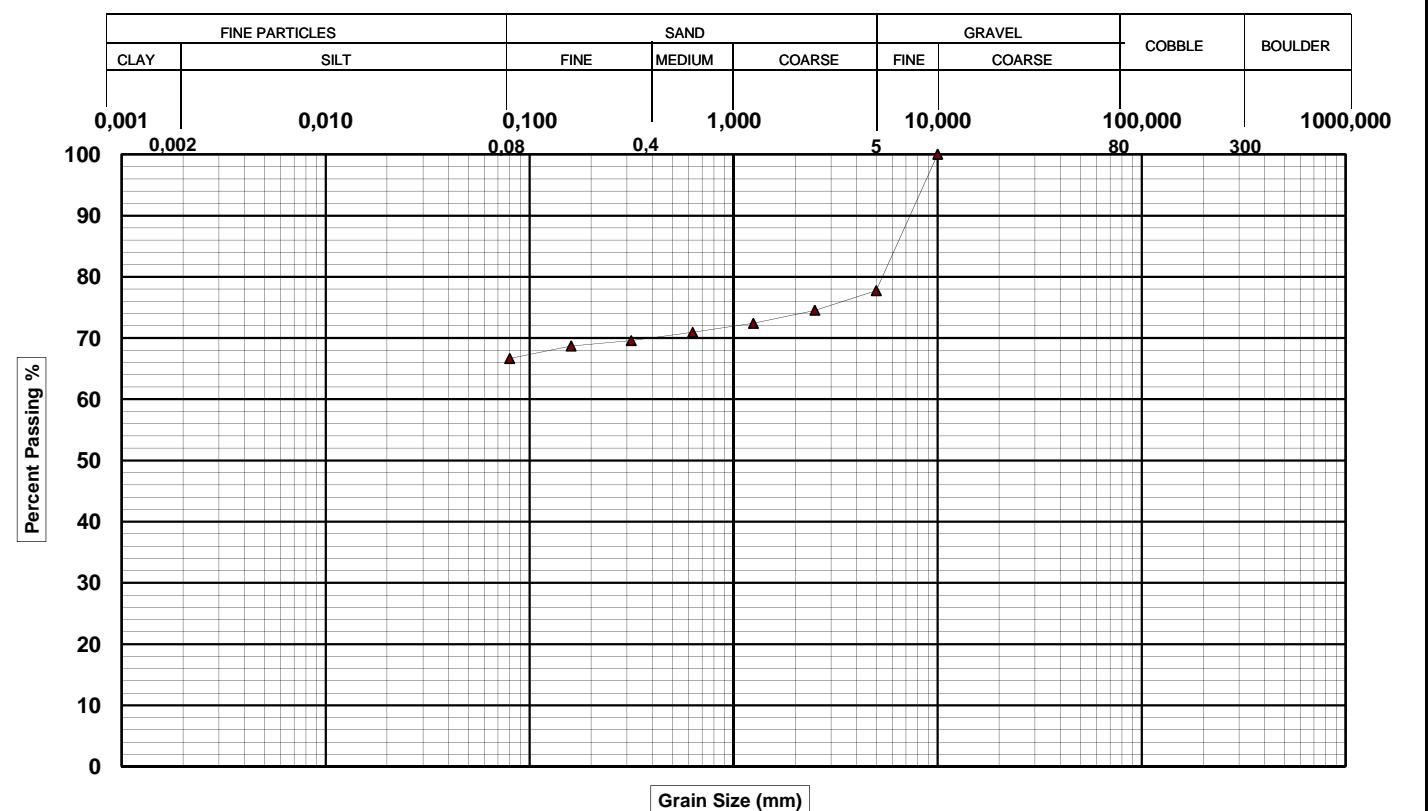
SAMPLE IDENTIFICATION										
Sample	10BH-14 (SS-11)									
Depth	8,53 - 9,14 m									
Soil Description										
Gravel and sand										

Prepared by Benoit St-Pierre, tech.

Approved by Ibrahim Ja'far, ing.

Date 2010-04-01

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36422

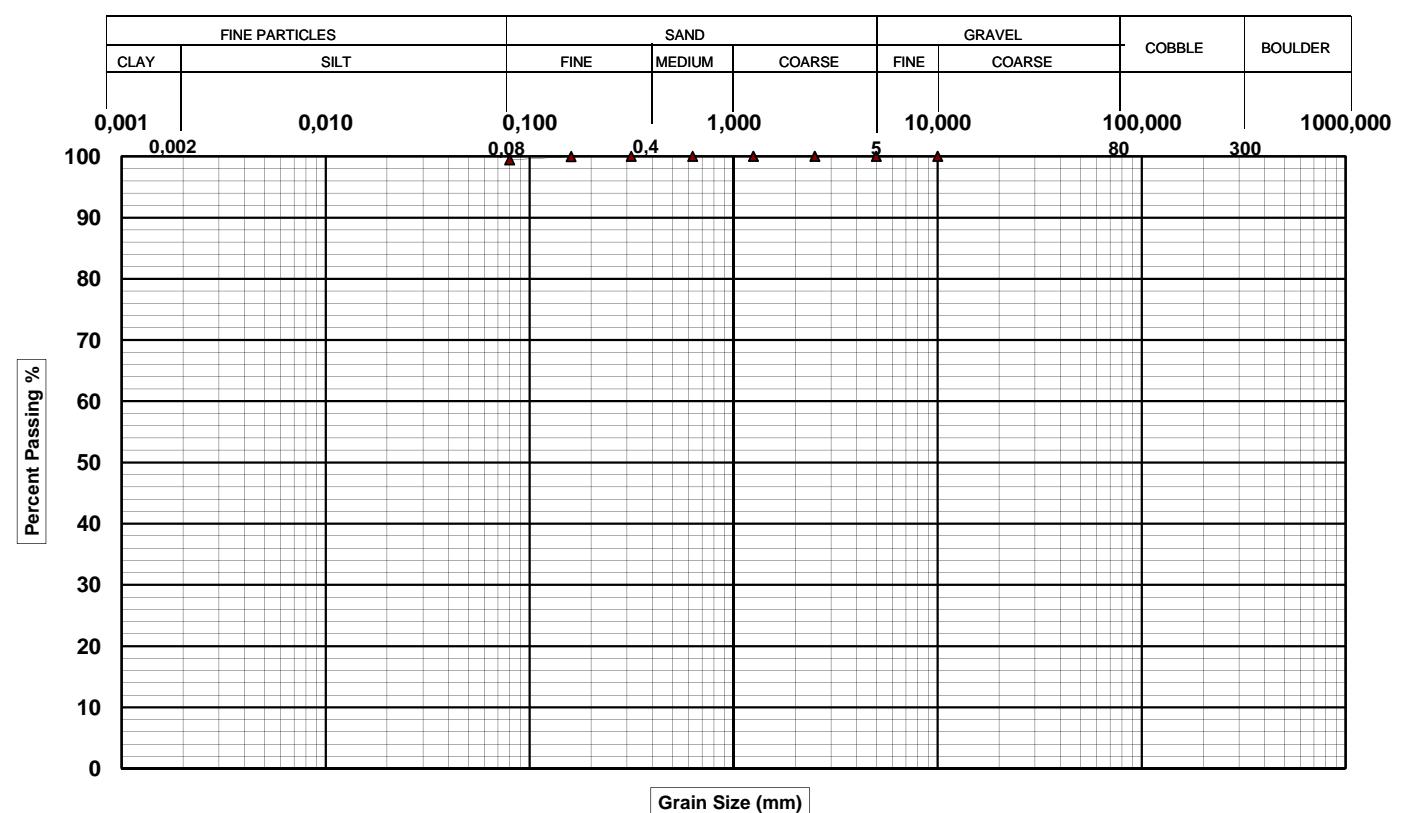


GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	66,7	11,1	22,3	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	N/A	N/A	N/A	15

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	75		
56,00	100	1,250	72		
40,00	100	0,630	71		
31,50	100	0,315	70		
20,00	100	0,160	69		
14,00	100	0,080	66,7		
10,00	100				
5,00	78				

SAMPLE IDENTIFICATION										
Sample	10BH-06 (SS-11)									
Depth	8,84 - 9,45 m									
Soil Description										
Silt, some gravel and sand										

CLIENT	TransAlta	N/D G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)	
LOCATION	St-Valentin (Québec)	NO. LAB. 36426



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	99,4	0,6	0,0	0,0	0,0
D₁₀ (mm)	D₃₀ (mm)	D₆₀ (mm)	C_u	C_c	W_n (%)
N/A	N/A	N/A	N/A	N/A	12

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	100		
56,00	100	1,250	100		
40,00	100	0,630	100		
31,50	100	0,315	100		
20,00	100	0,160	100		
14,00	100	0,080	99,4		
10,00	100				
5,00	100				

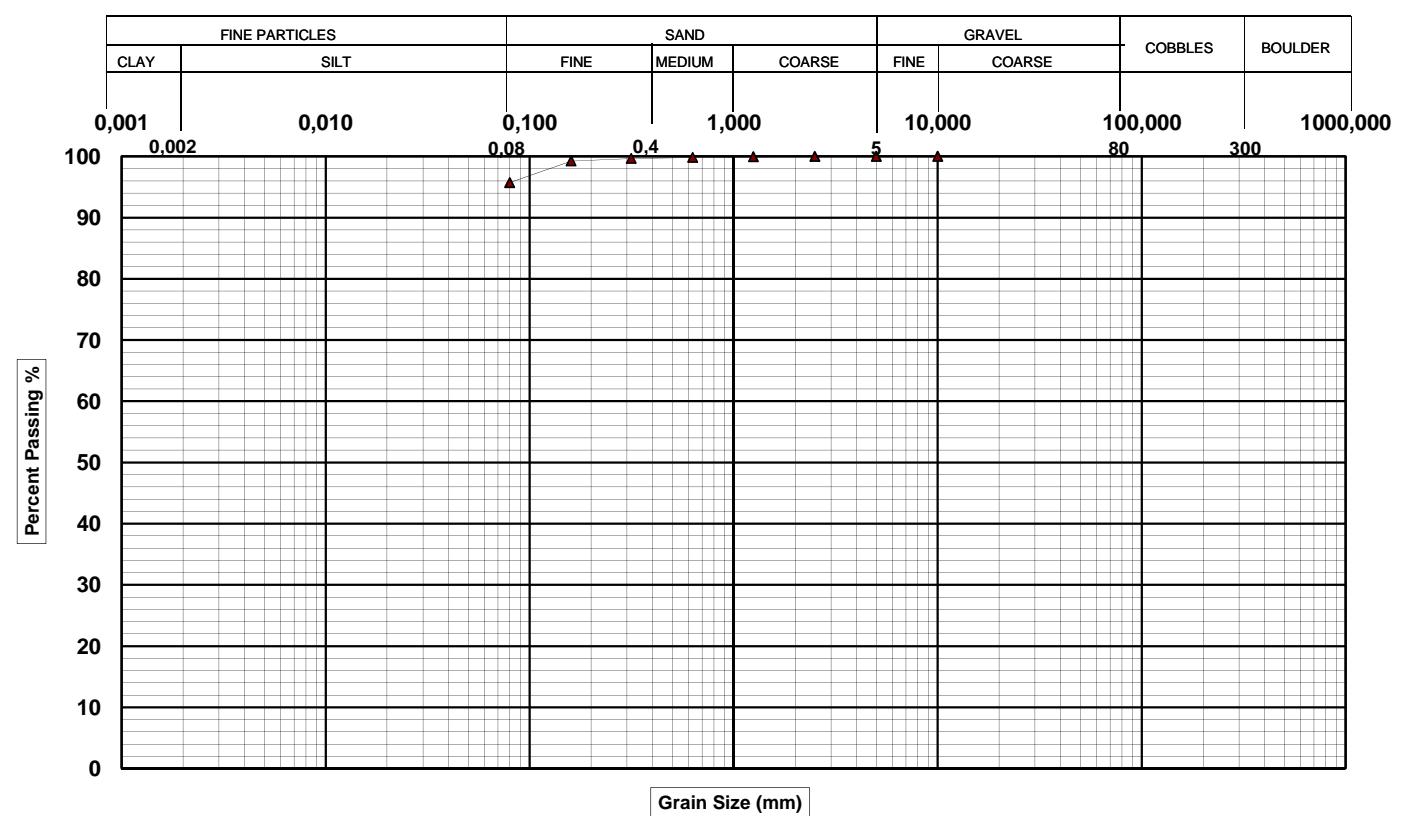
SAMPLE IDENTIFICATION										
Sample	10BH-11 (SS-05)									
Depth	3,05 - 3,66 m									
Soil Description										
Silt										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-08

CLIENT	TransAlta	N/D G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)	
LOCATION	St-Valentin (Québec)	NO. LAB. 36427



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	95,7	4,3	0,0	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	N/A	N/A	N/A	18

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	100		
56,00	100	1,250	100		
40,00	100	0,630	100		
31,50	100	0,315	100		
20,00	100	0,160	99		
14,00	100	0,080	95,7		
10,00	100				
5,00	100				

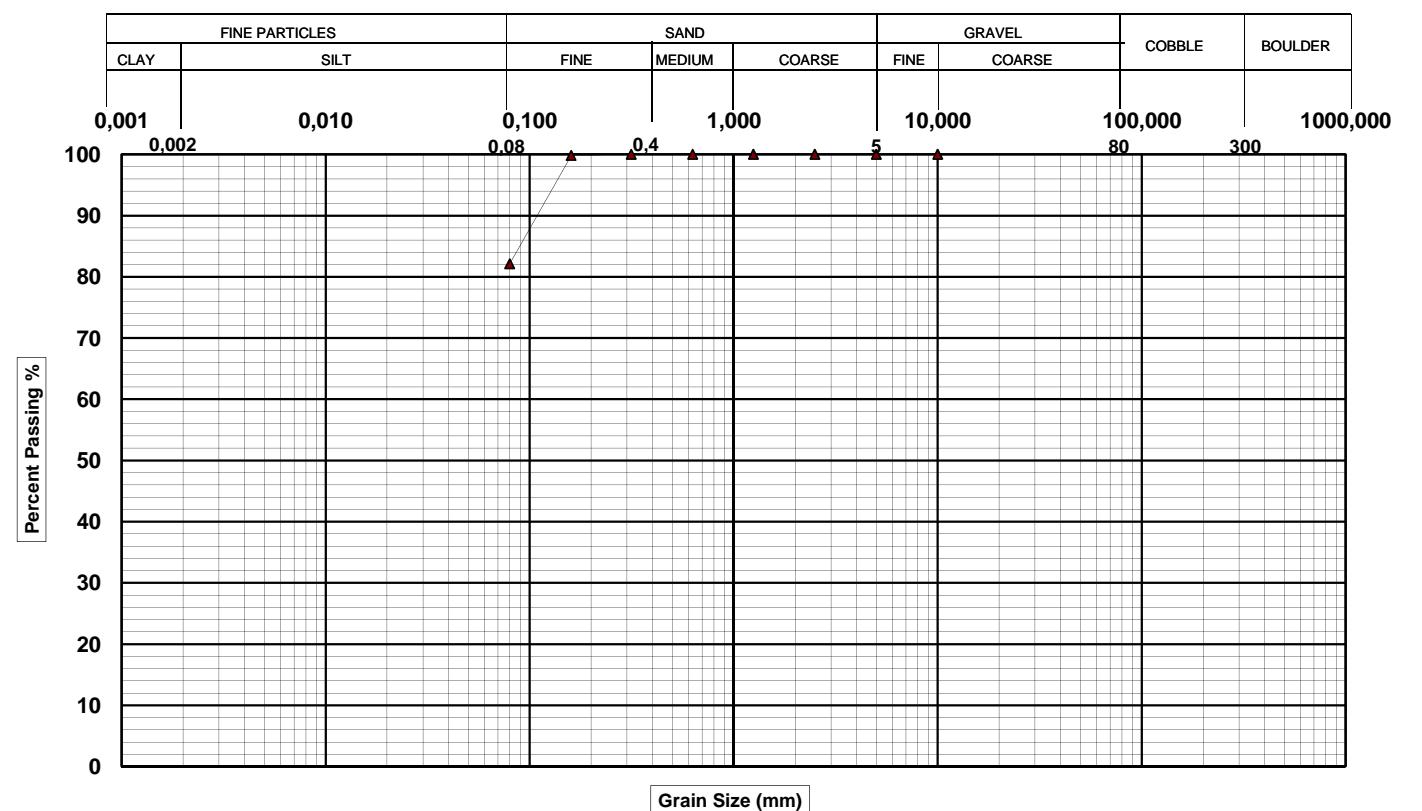
SAMPLE IDENTIFICATION										
Sample	10BH-11 (SS-11)									
Depth	8,53 - 9,14 m									
Soil Description										
Silt, traces of sand										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-08

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36421

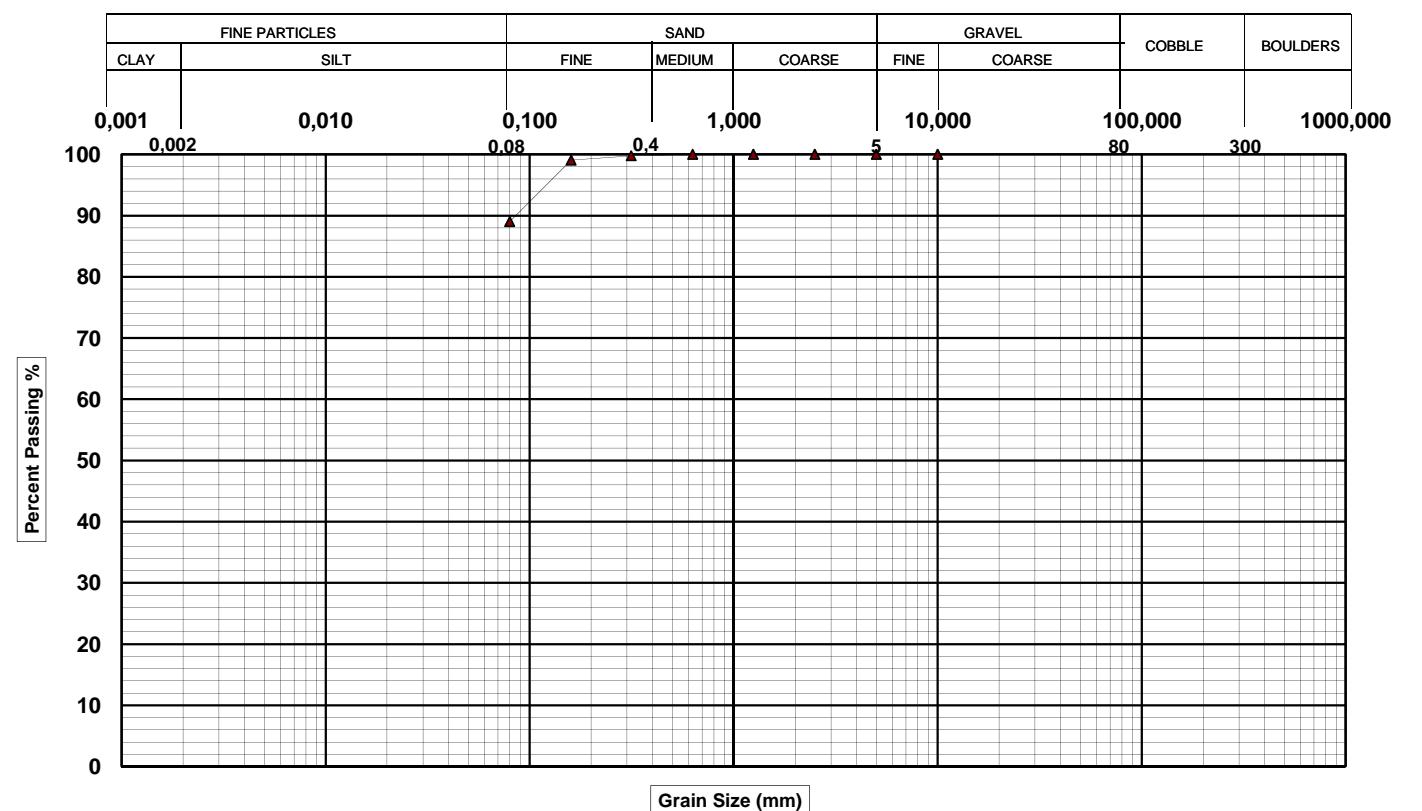


GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	82,1	17,9	0,0	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	N/A	N/A	N/A	19

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	100		
56,00	100	1,250	100		
40,00	100	0,630	100		
31,50	100	0,315	100		
20,00	100	0,160	100		
14,00	100	0,080	82,1		
10,00	100				
5,00	100				

SAMPLE IDENTIFICATION	
Sample	10BH-06 (SS-06)
Depth	4,27 - 4,88 m
Soil Description	
Silt, some sand	

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36431



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	89,0	11,0	0,0	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	N/A	N/A	N/A	16

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	100		
56,00	100	1,250	100		
40,00	100	0,630	100		
31,50	100	0,315	100		
20,00	100	0,160	99		
14,00	100	0,080	89,0		
10,00	100				
5,00	100				

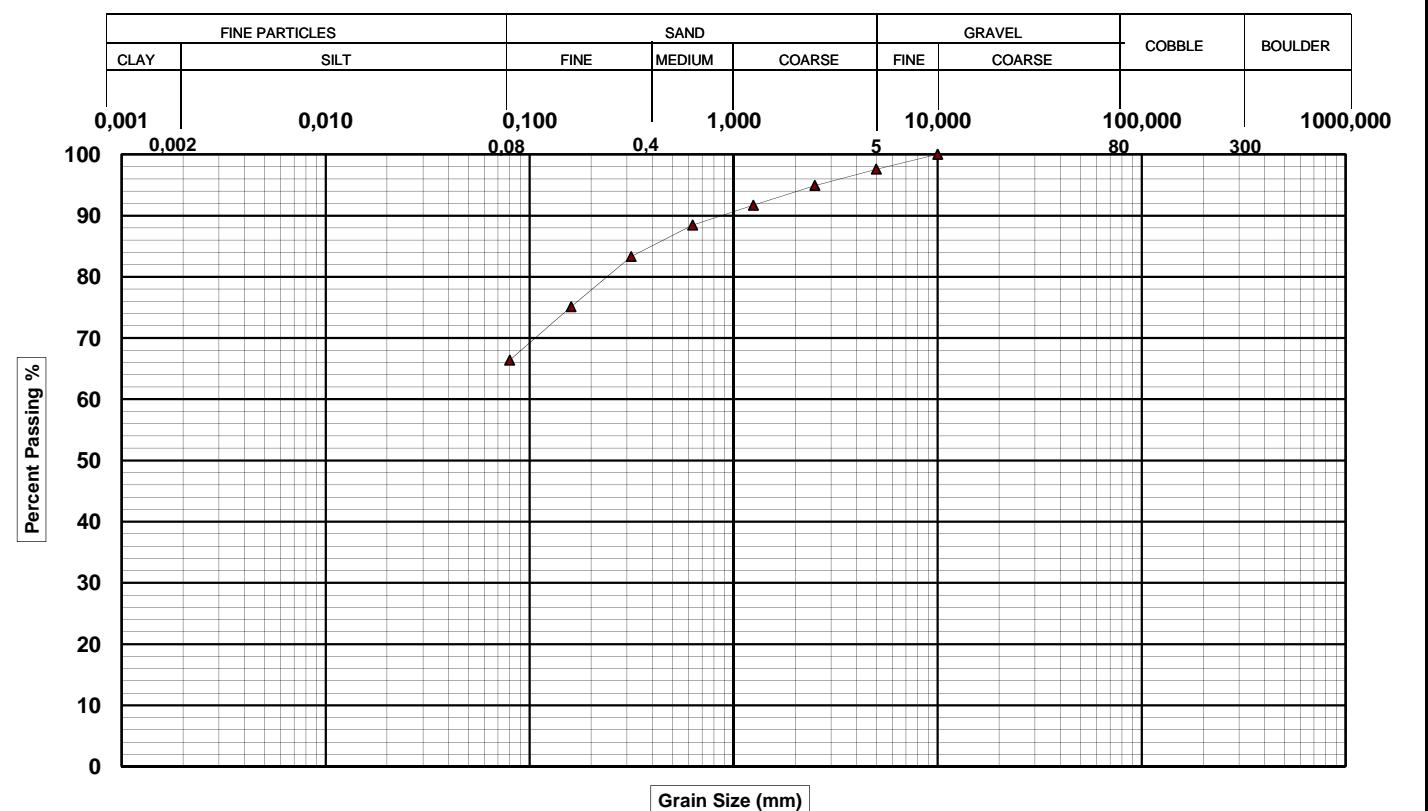
SAMPLE IDENTIFICATION										
Sample	10BH-08 (SS-12)									
Depth	9,75 - 10,36 m									
Soil Description										
Silt, some sand										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-08

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36434



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	66,4	31,2	2,4	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	N/A	N/A	N/A	13

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	95		
56,00	100	1,250	92		
40,00	100	0,630	88		
31,50	100	0,315	83		
20,00	100	0,160	75		
14,00	100	0,080	66,4		
10,00	100				
5,00	98				

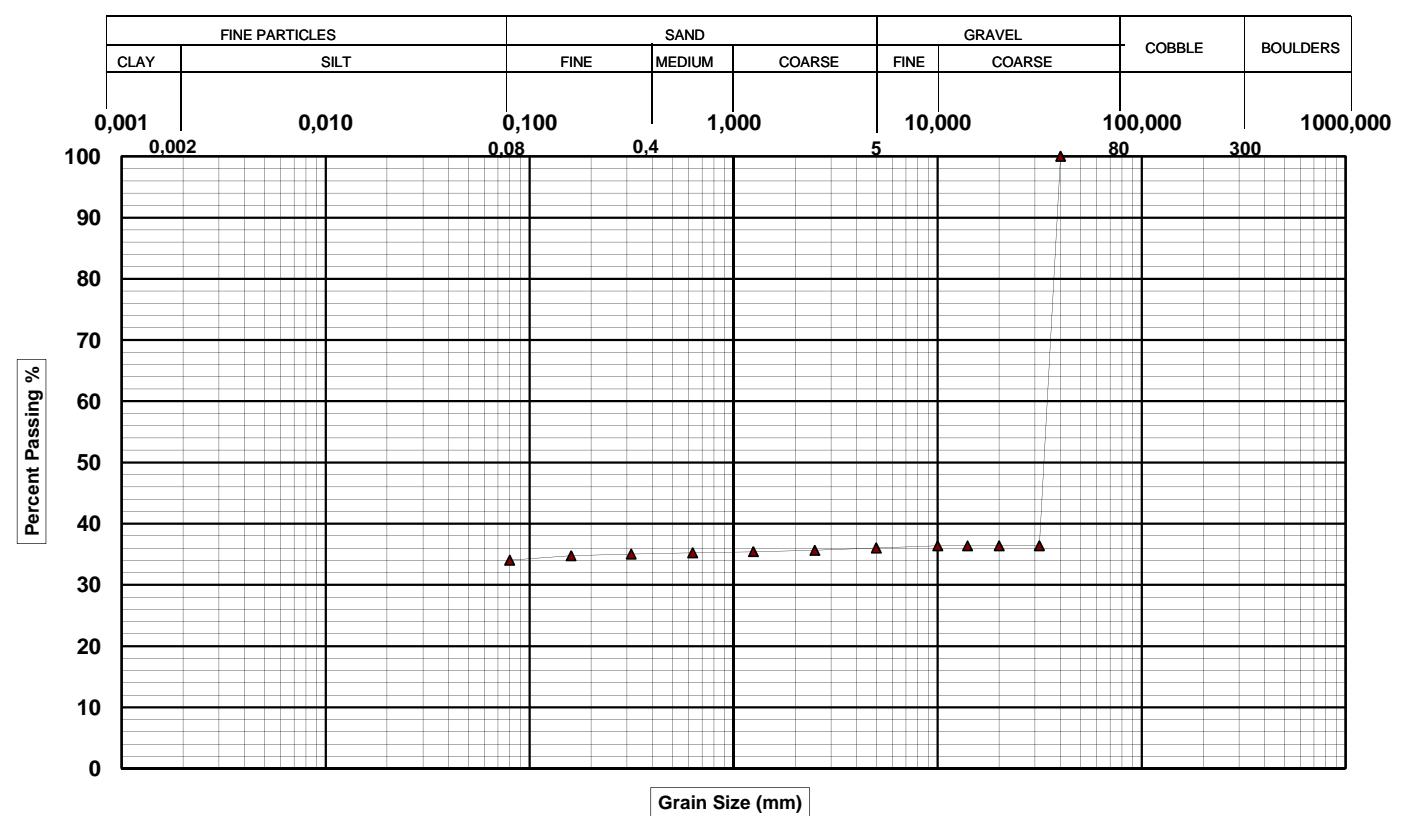
SAMPLE IDENTIFICATION										
Sample	10BH-13 (SS-09)									
Depth	7,01 - 7,62 m									
Soil Description										
Sandy silt, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-08

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36435



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	34,0	2,0	64,0	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	N/A	N/A	N/A	7

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	36		
56,00	100	1,250	35		
40,00	100	0,630	35		
31,50	36	0,315	35		
20,00	36	0,160	35		
14,00	36	0,080	34,0		
10,00	36				
5,00	36				

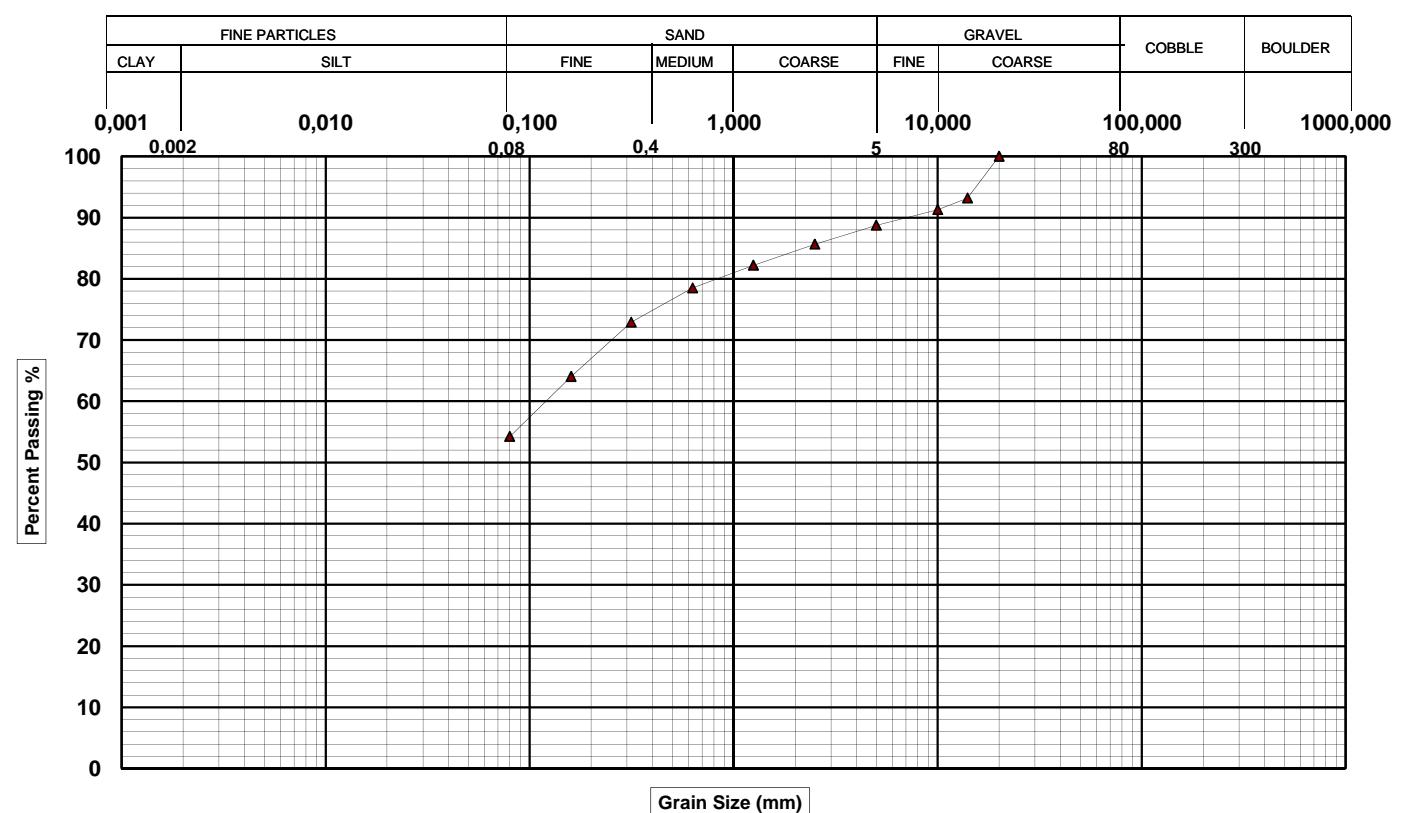
SAMPLE IDENTIFICATION										
Sample	10F-13 (CF-13)									
Depth	10,67 - 11,28 m									
Soil Description										
Gravel silteux, traces of sand										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-08

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	34633



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	54,2	34,5	11,3	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,12	N/A	N/A	10

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	86		
56,00	100	1,250	82		
40,00	100	0,630	79		
31,50	100	0,315	73		
20,00	100	0,160	64		
14,00	93	0,080	54,2		
10,00	91				
5,00	89				

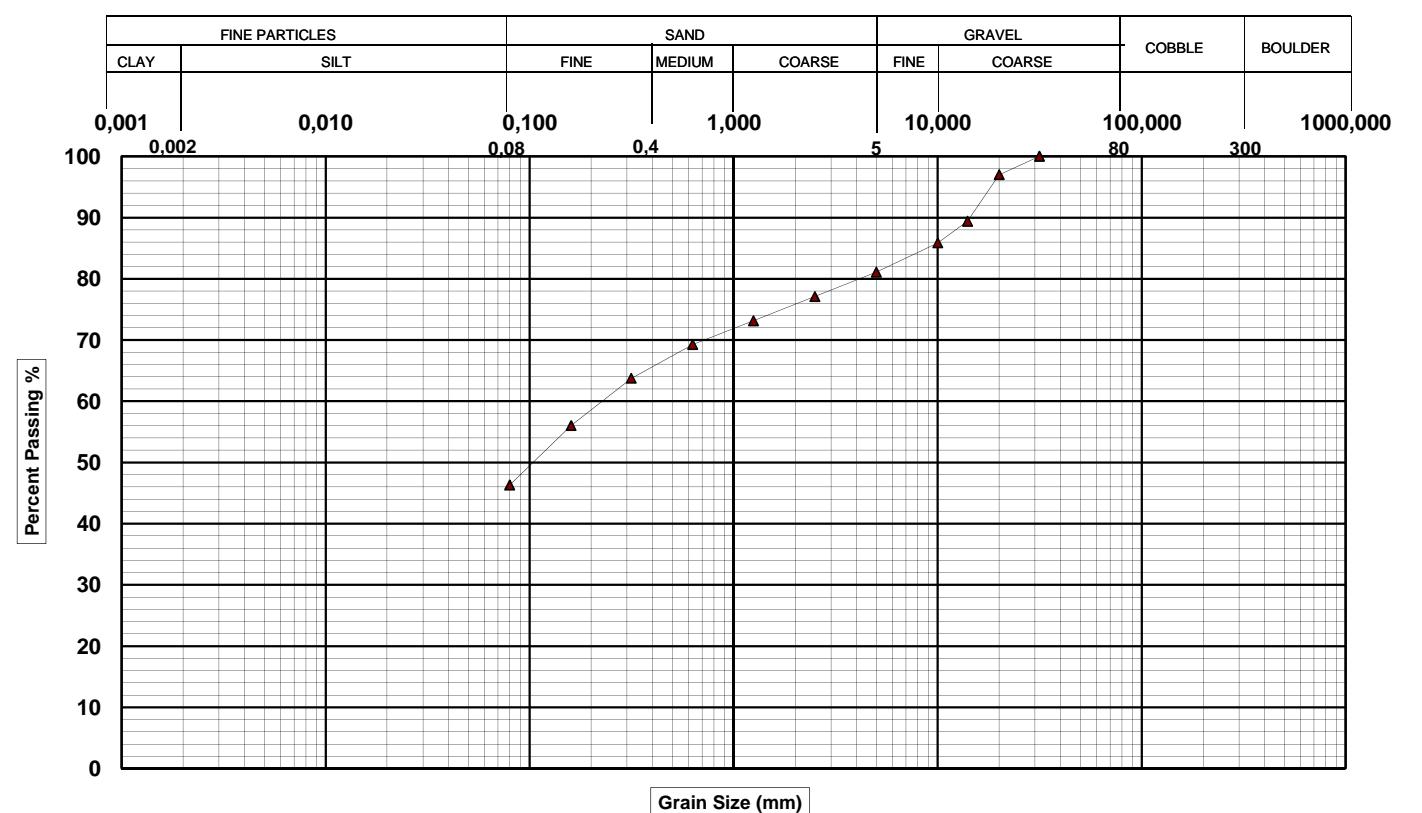
SAMPLE IDENTIFICATION										
Sample	10BH-13 (SS-05)									
Depth	3,35 - 3, 96 m									
Soil Description										
Sandy silt, some gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-08

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36432



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	46,3	34,8	18,9	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,23	N/A	N/A	8

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	77		
56,00	100	1,250	73		
40,00	100	0,630	69		
31,50	100	0,315	64		
20,00	97	0,160	56		
14,00	89	0,080	46,3		
10,00	86				
5,00	81				

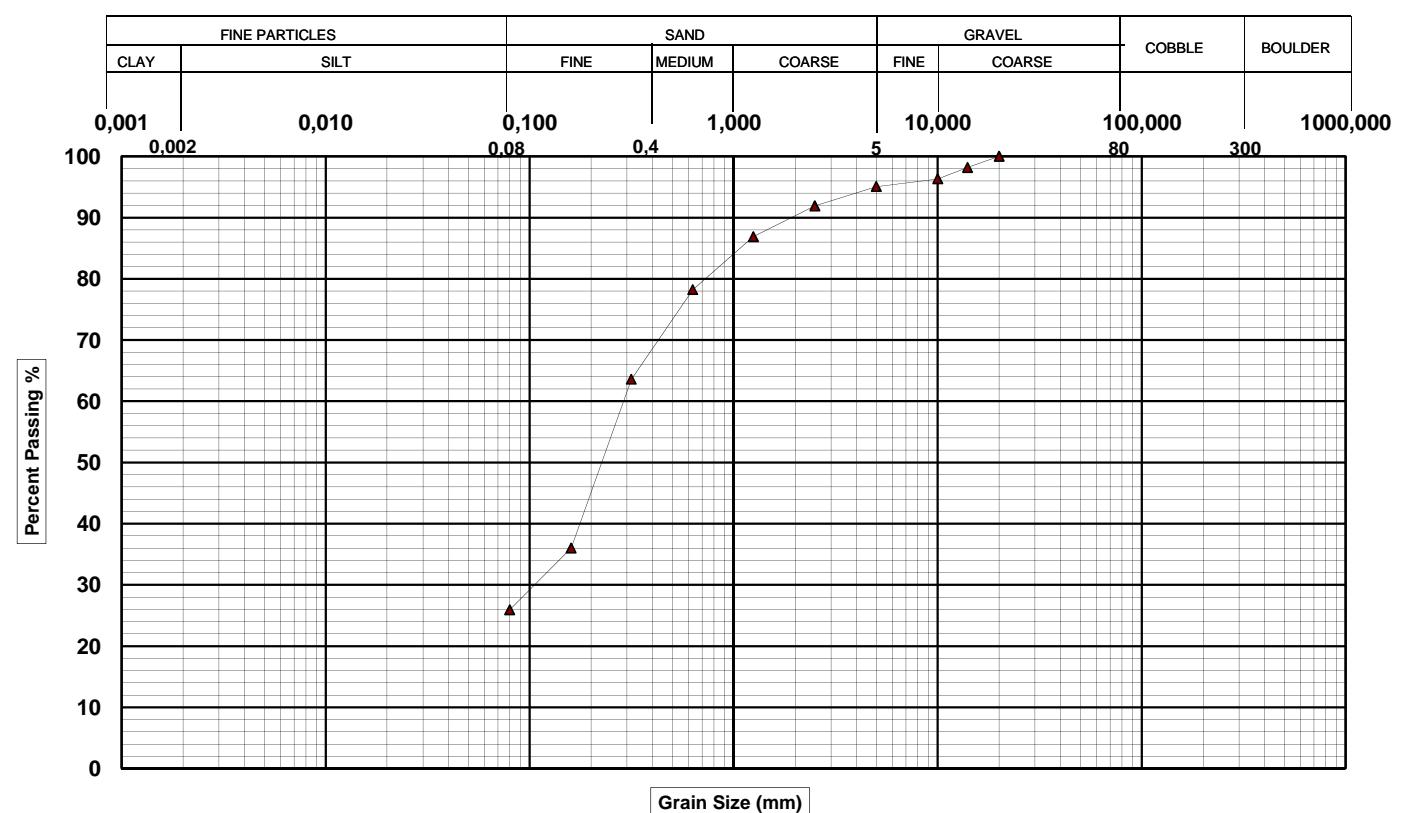
SAMPLE IDENTIFICATION										
Sample	10BH-08 (SS-16)									
Depth	15,00 - 15,61 m									
Soil Description										
Sandy silt, some gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-08

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36436



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	25,9	69,1	4,9	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	0,10	0,30	N/A	N/A	16

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	92		
56,00	100	1,250	87		
40,00	100	0,630	78		
31,50	100	0,315	64		
20,00	100	0,160	36		
14,00	98	0,080	25,9		
10,00	96				
5,00	95				

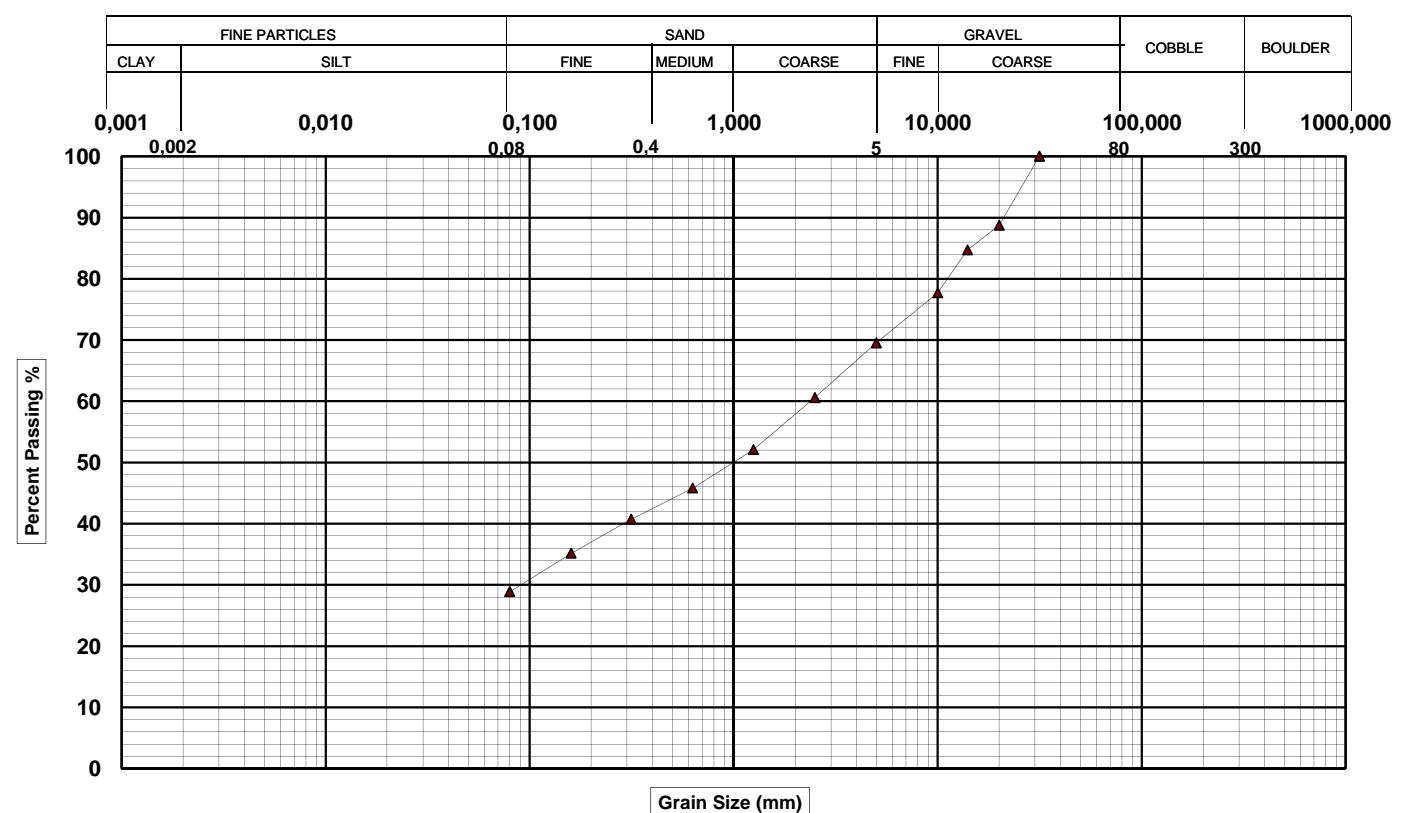
SAMPLE IDENTIFICATION										
Sample	10BH-13 (SS-16)									
Depth	15,24 - 15,85 m									
Soil Description										
Silty sand, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-08

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36424



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	28,9	40,6	30,5	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	0,09	0,25	N/A	N/A	8

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	61		
56,00	100	1,250	52		
40,00	100	0,630	46		
31,50	100	0,315	41		
20,00	89	0,160	35		
14,00	85	0,080	28,9		
10,00	78				
5,00	70				

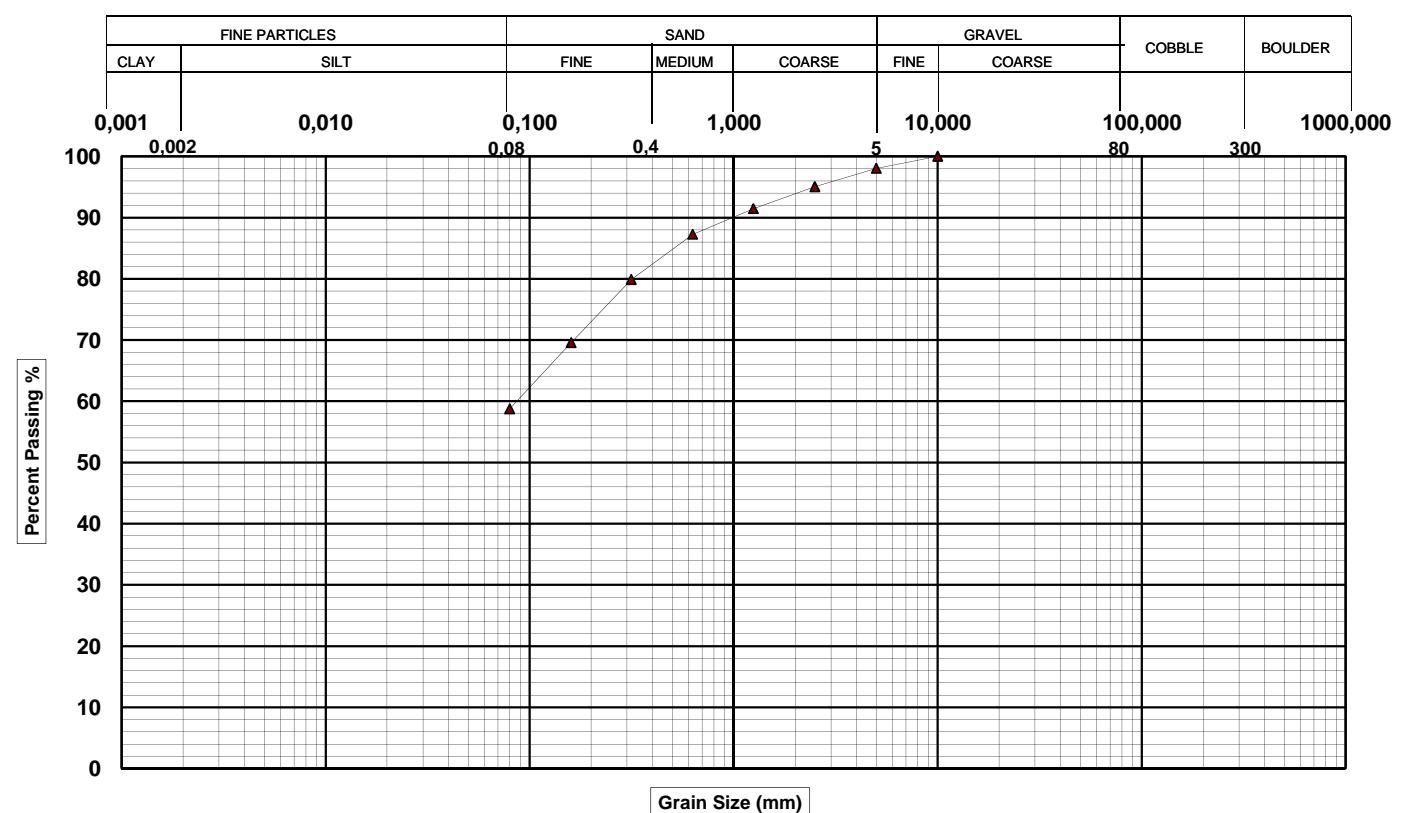
SAMPLE IDENTIFICATION										
Sample	10BH-07 (SS-07)									
Depth	5,18 - 5,79 m									
Soil Description										
Silty gravelly sand										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-08

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36429



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	58,7	39,3	2,0	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,09	N/A	N/A	4

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	95		
56,00	100	1,250	91		
40,00	100	0,630	87		
31,50	100	0,315	80		
20,00	100	0,160	70		
14,00	100	0,080	58,7		
10,00	100				
5,00	98				

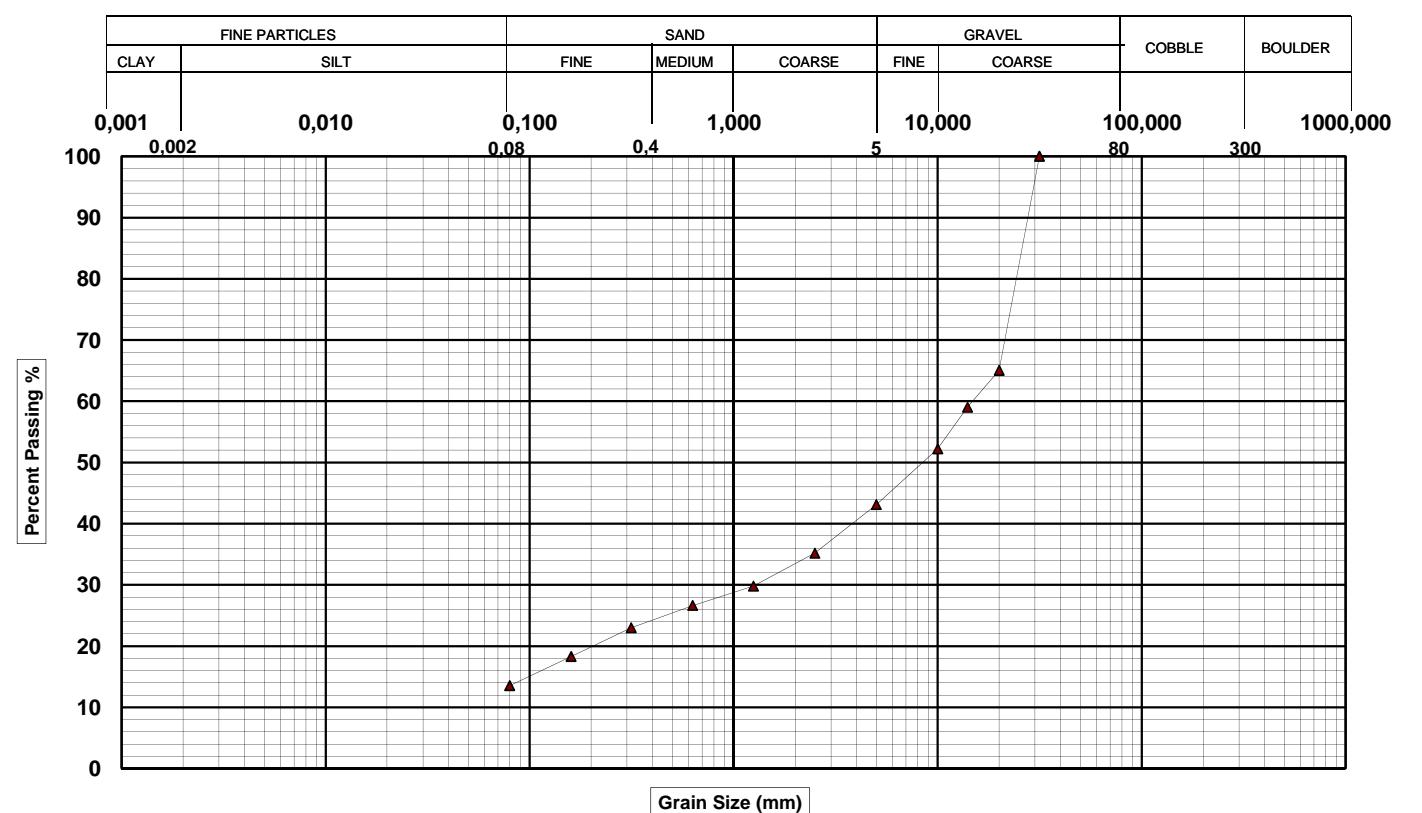
SAMPLE IDENTIFICATION										
Sample	10BH-08 (SS-04)									
Depth	2,44 - 3,05 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-08

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36428



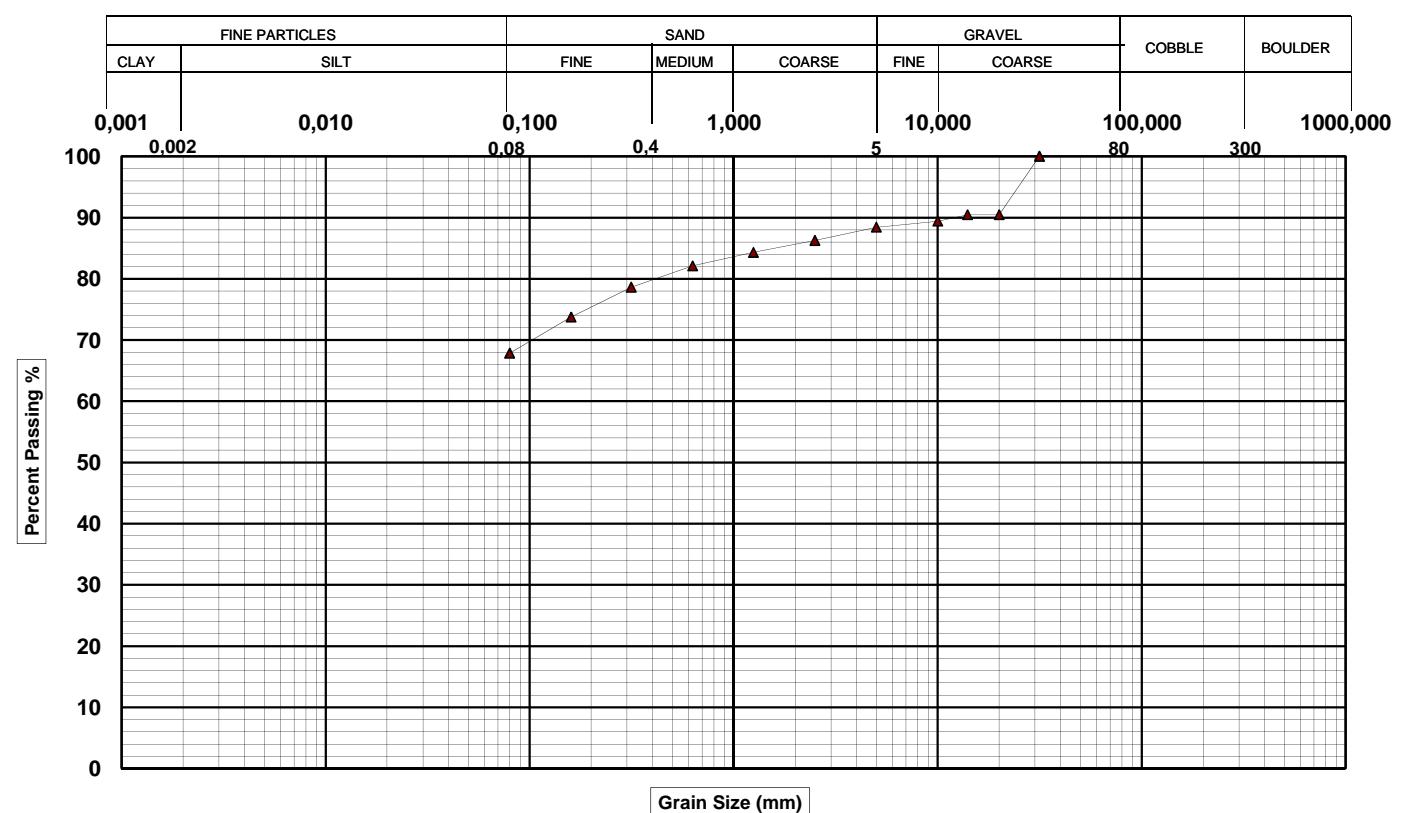
GRAIN-SIZE DISTRIBUTION										
Fine Particles		Coarse Particles								
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)					
-	13,5	29,6	56,9	0,0	0,0					
PERCENT PASSING										
(mm)	(%)	(mm)	(%)	(mm)	(%)					
80,00	100	2,500	35							
56,00	100	1,250	30							
40,00	100	0,630	27							
31,50	100	0,315	23							
20,00	65	0,160	18							
14,00	59	0,080	13,5							
10,00	52									
5,00	43									
SAMPLE IDENTIFICATION										
Sample	10BH-11 (SS-13)									
Depth	10,67 - 11,28 m									
Soil Description										
Sandy gravel, some silt										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-08

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36430



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	67,9	20,6	11,6	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	N/A	N/A	N/A	13

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	86		
56,00	100	1,250	84		
40,00	100	0,630	82		
31,50	100	0,315	79		
20,00	90	0,160	74		
14,00	90	0,080	67,9		
10,00	89				
5,00	88				

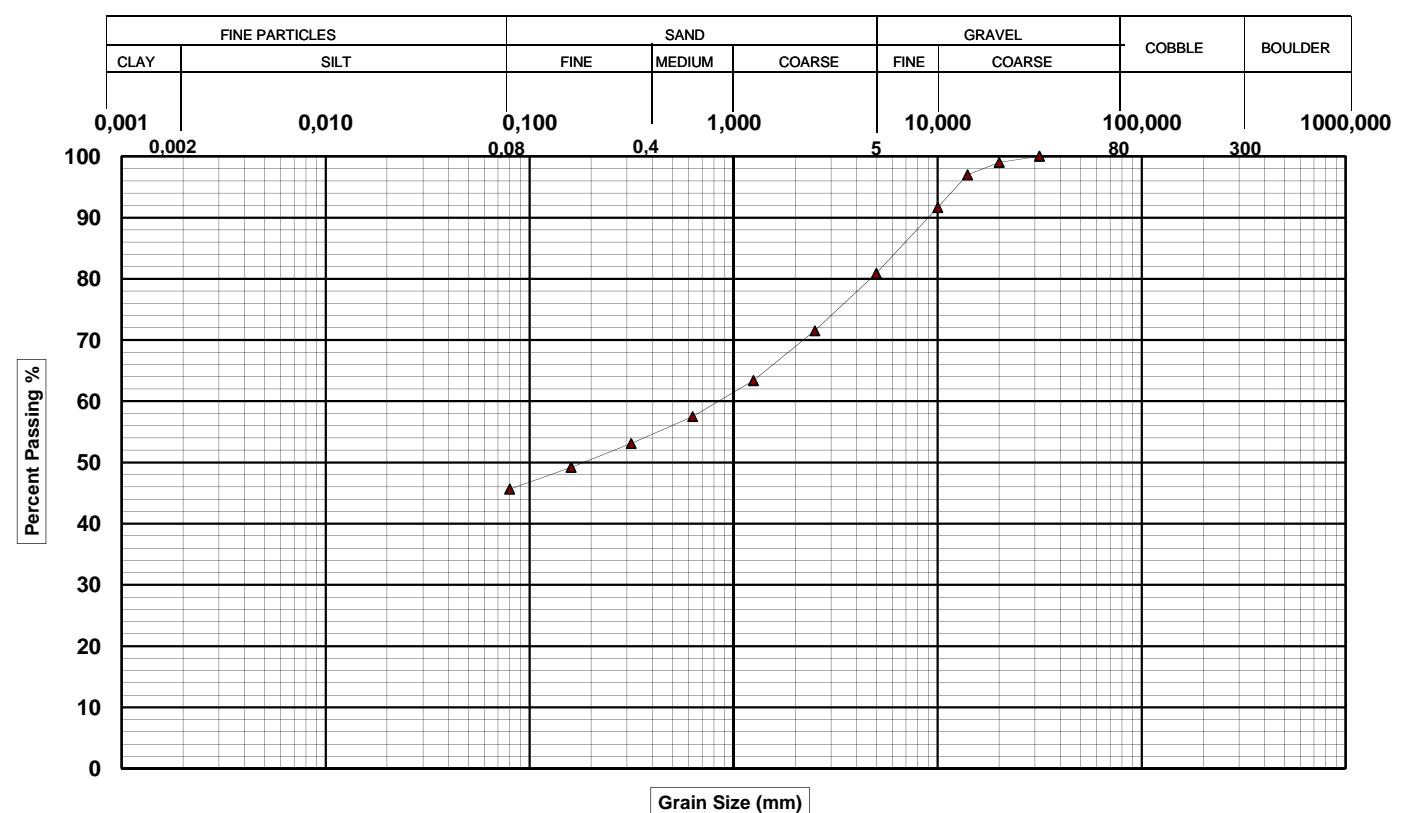
SAMPLE IDENTIFICATION										
Sample	10BH-08 (SS-09)									
Depth	7,01 - 7,62 m									
Soil Description										
Sandy silt, some gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-08

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36525



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	45,7	35,2	19,1	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,86	N/A	N/A	10

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	72		
56,00	100	1,250	63		
40,00	100	0,630	58		
31,50	100	0,315	53		
20,00	99	0,160	49		
14,00	97	0,080	45,7		
10,00	92				
5,00	81				

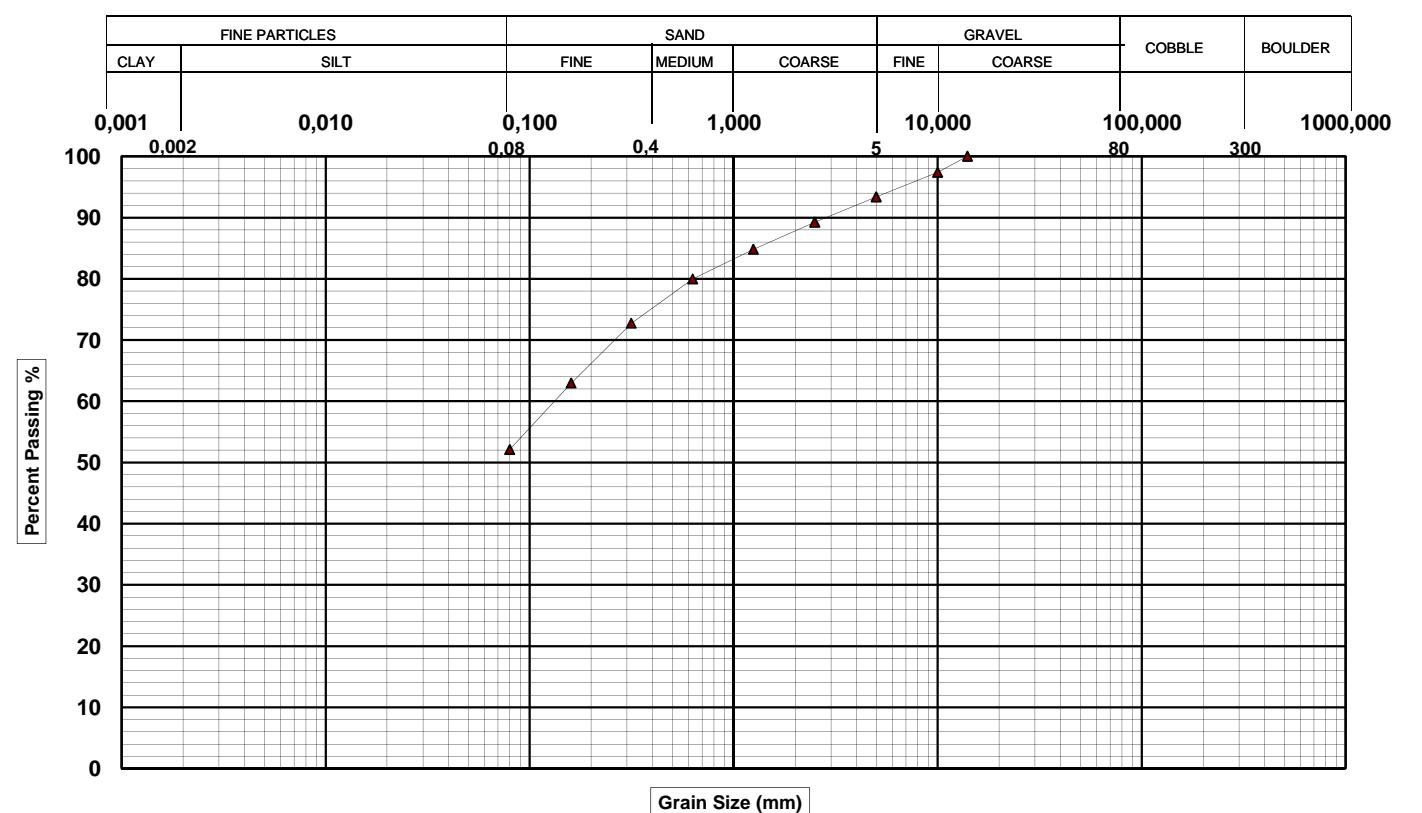
SAMPLE IDENTIFICATION										
Sample	10BH-29 (SS-05)									
Depth	3,35 - 3,86 m									
Soil Description										
Silt and sand, a little gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-12

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36524



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	52,1	41,2	6,6	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,15	N/A	N/A	11

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	89		
56,00	100	1,250	85		
40,00	100	0,630	80		
31,50	100	0,315	73		
20,00	100	0,160	63		
14,00	100	0,080	52,1		
10,00	97				
5,00	93				

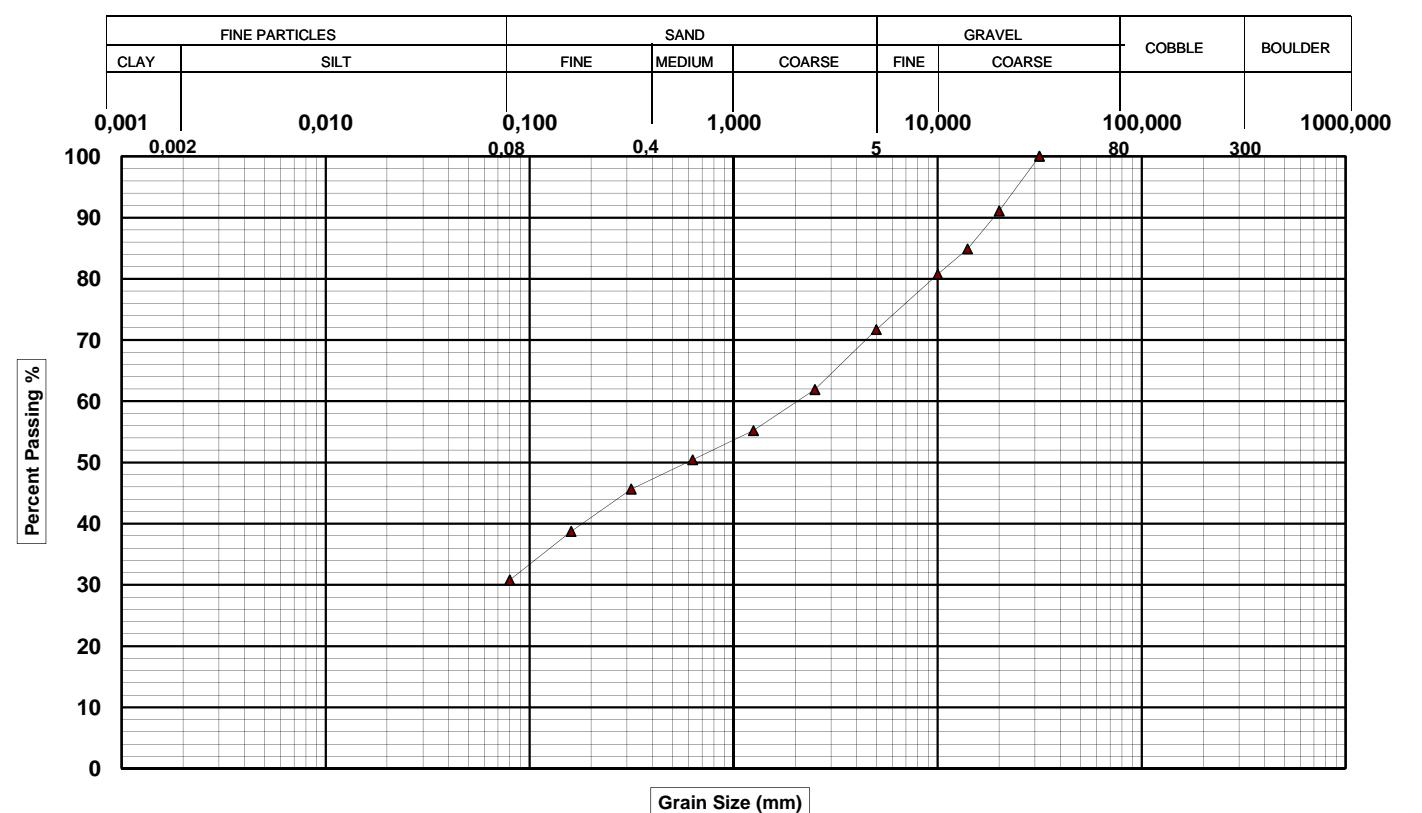
SAMPLE IDENTIFICATION										
Sample	10BH-29 (SS-03)									
Depth	1,52 - 2,13 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-12

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36527



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	30,8	40,9	28,3	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	2,00	N/A	N/A	11

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	62		
56,00	100	1,250	55		
40,00	100	0,630	50		
31,50	100	0,315	46		
20,00	91	0,160	39		
14,00	85	0,080	30,8		
10,00	81				
5,00	72				

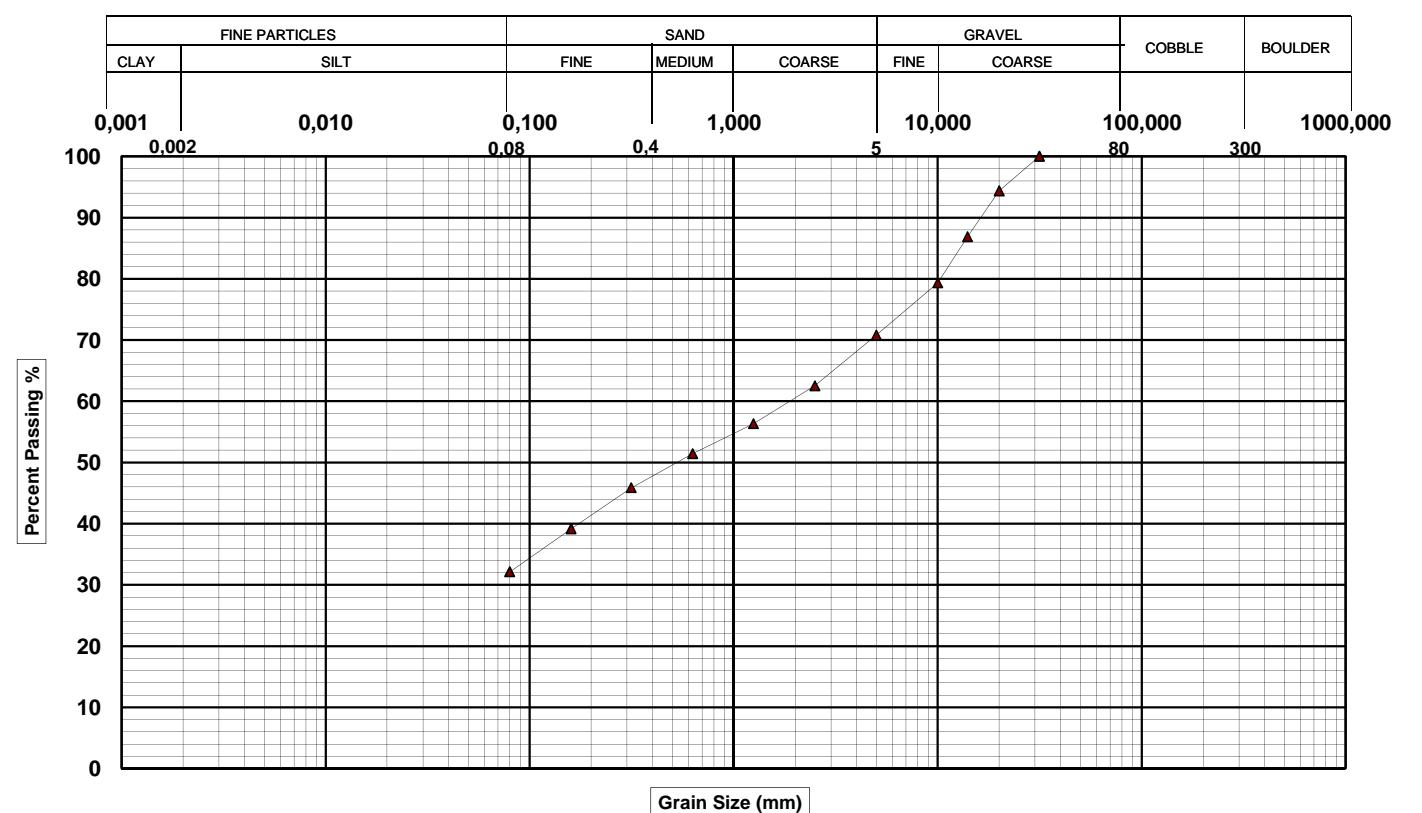
SAMPLE IDENTIFICATION										
Sample	10BH-30 (SS-03)									
Depth	1,52 - 2,13 m									
Soil Description										
Silty gravelly sand										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-12

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36522



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	32,1	38,7	29,2	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	2,00	N/A	N/A	8

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	63		
56,00	100	1,250	56		
40,00	100	0,630	51		
31,50	100	0,315	46		
20,00	94	0,160	39		
14,00	87	0,080	32,1		
10,00	79				
5,00	71				

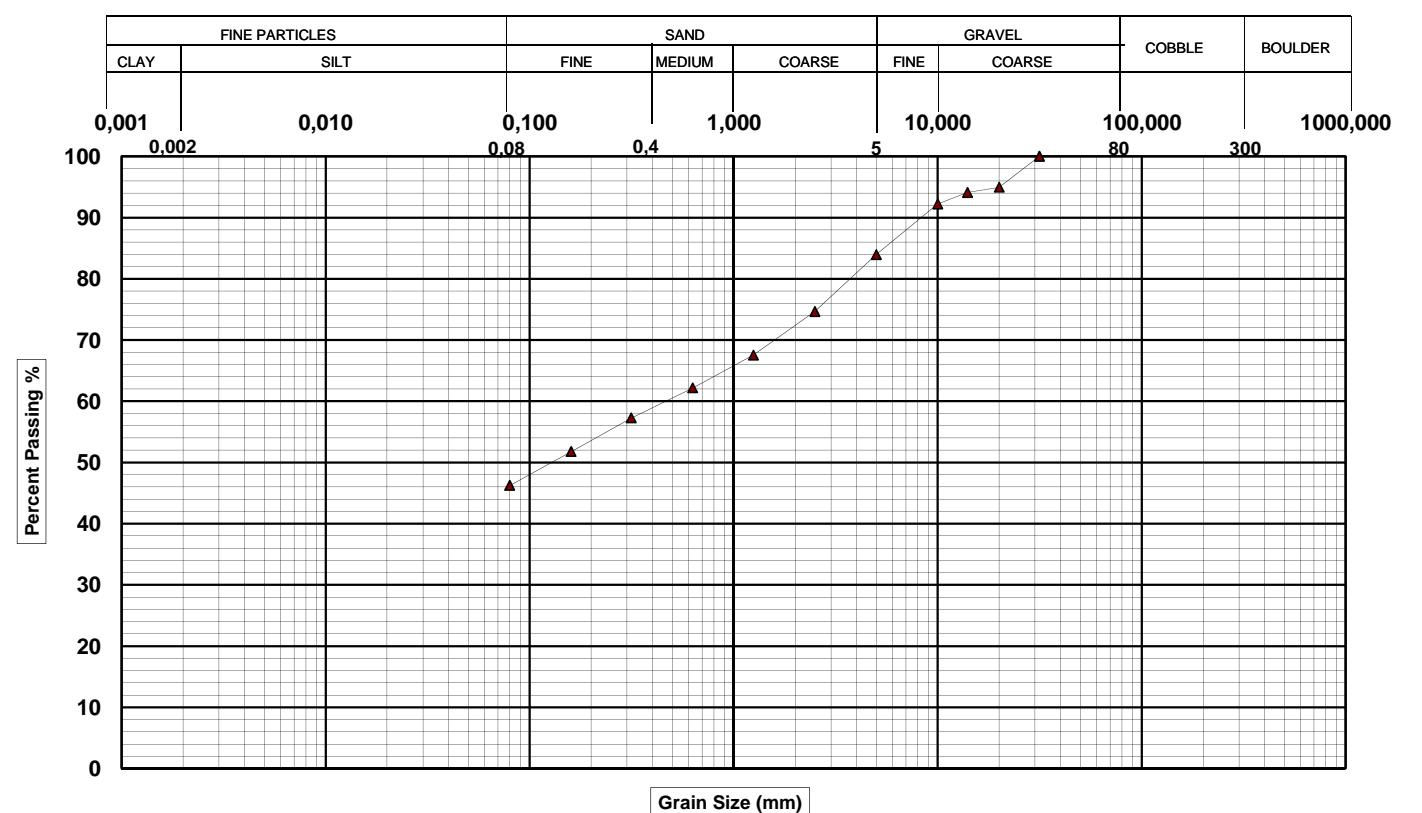
SAMPLE IDENTIFICATION										
Sample	10BH-25 (SS-06)									
Depth	4,27 - 4,88 m									
Soil Description										
Gravelly silty sand										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-12

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36528



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	46,2	37,7	16,1	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,49	N/A	N/A	10

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	75		
56,00	100	1,250	68		
40,00	100	0,630	62		
31,50	100	0,315	57		
20,00	95	0,160	52		
14,00	94	0,080	46,2		
10,00	92				
5,00	84				

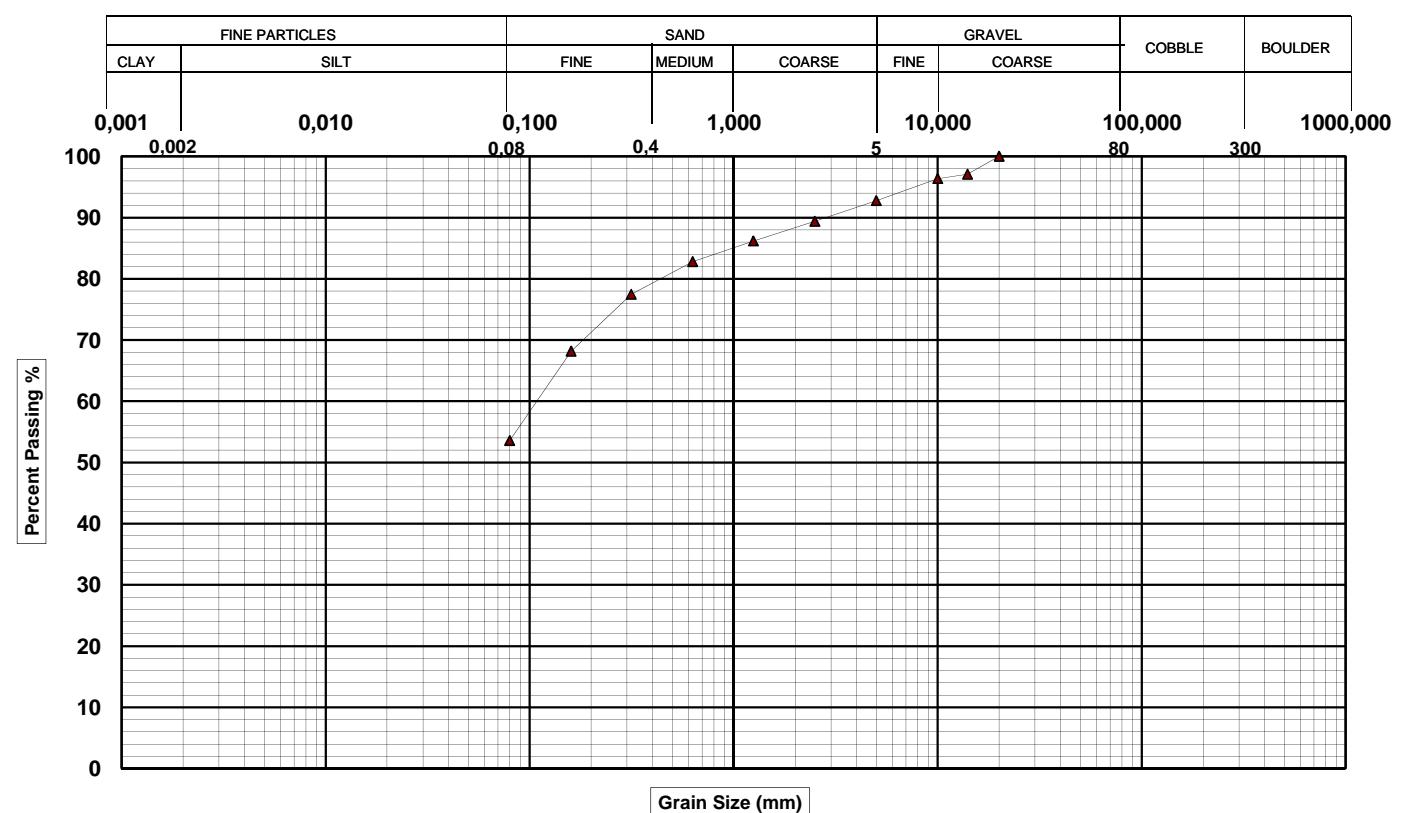
SAMPLE IDENTIFICATION										
Sample	10BH-30 (SS-06)									
Depth	4,57 - 5,18 m									
Soil Description										
Silt and sand, some gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-12

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36521



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	53,6	39,2	7,2	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,11	N/A	N/A	11

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	89		
56,00	100	1,250	86		
40,00	100	0,630	83		
31,50	100	0,315	77		
20,00	100	0,160	68		
14,00	97	0,080	53,6		
10,00	96				
5,00	93				

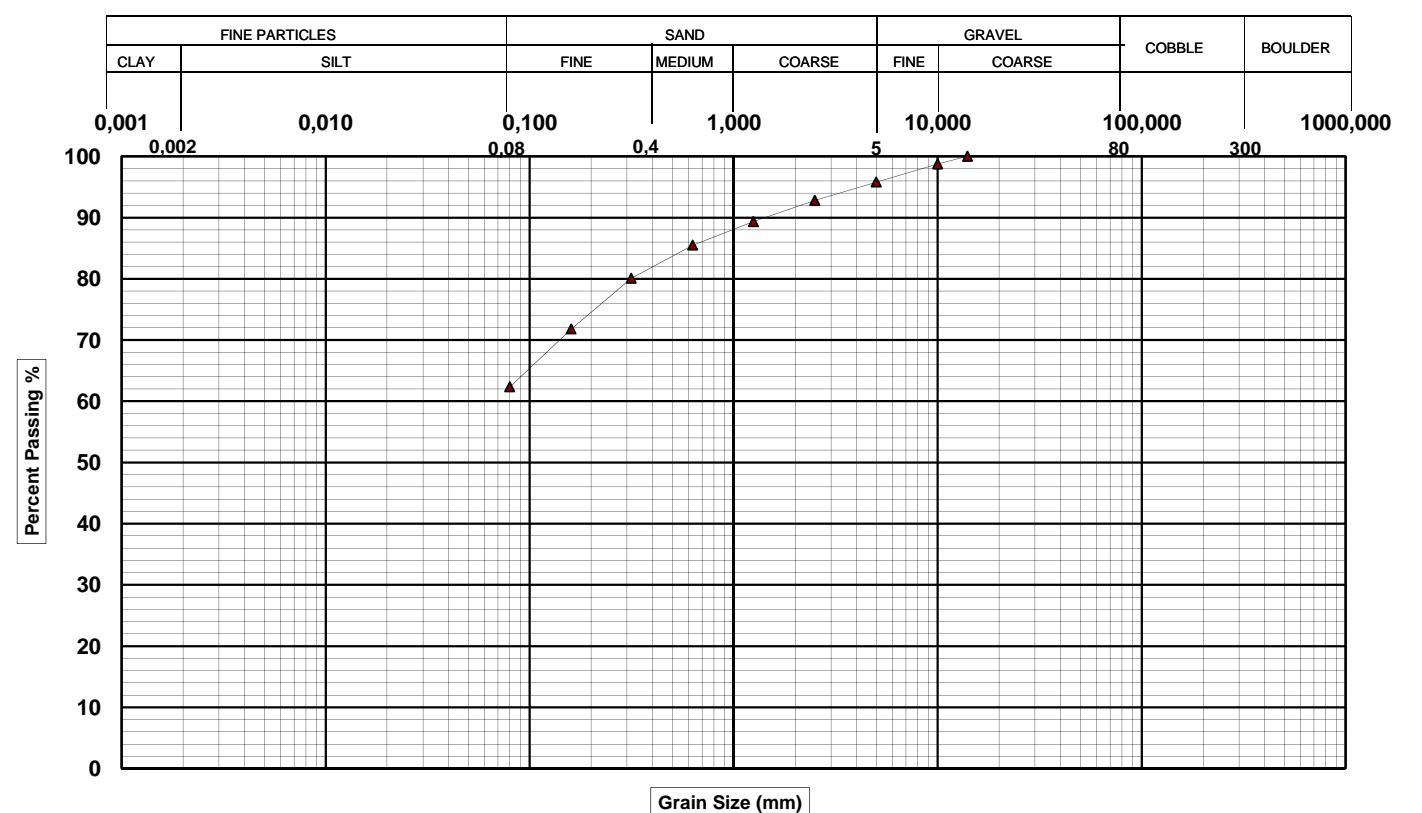
SAMPLE IDENTIFICATION										
Sample	10BH-26 (SS-03)									
Depth	1,52 - 2,13 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-12

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36529



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	62,3	33,4	4,2	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	N/A	N/A	N/A	6

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	93		
56,00	100	1,250	89		
40,00	100	0,630	86		
31,50	100	0,315	80		
20,00	100	0,160	72		
14,00	100	0,080	62,3		
10,00	99				
5,00	96				

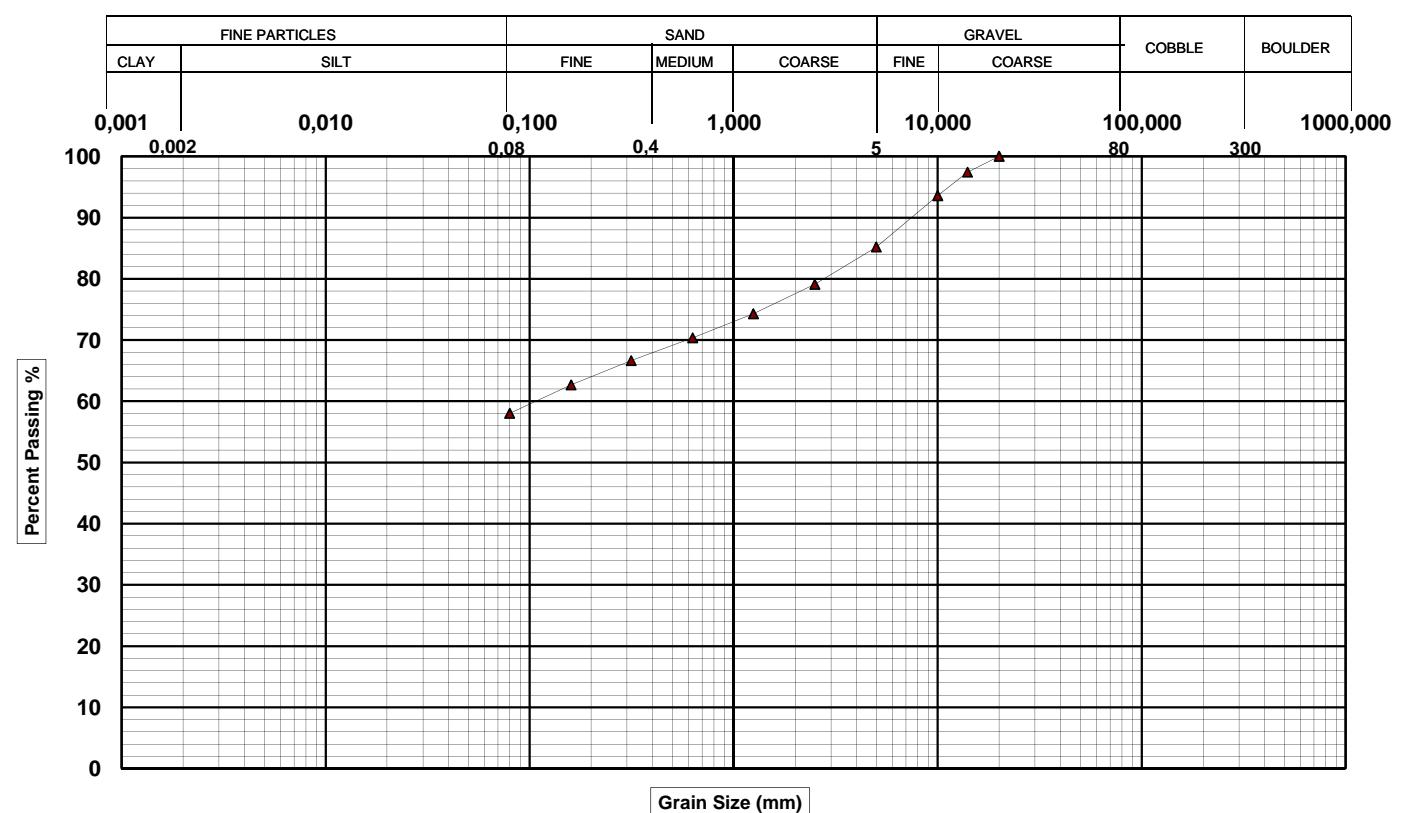
SAMPLE IDENTIFICATION										
Sample	10BH-32 (SS-02)									
Depth	0,61 - 1,22									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-12

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36530



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	58,1	27,1	14,8	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,11	N/A	N/A	12

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	79		
56,00	100	1,250	74		
40,00	100	0,630	70		
31,50	100	0,315	67		
20,00	100	0,160	63		
14,00	97	0,080	58,1		
10,00	94				
5,00	85				

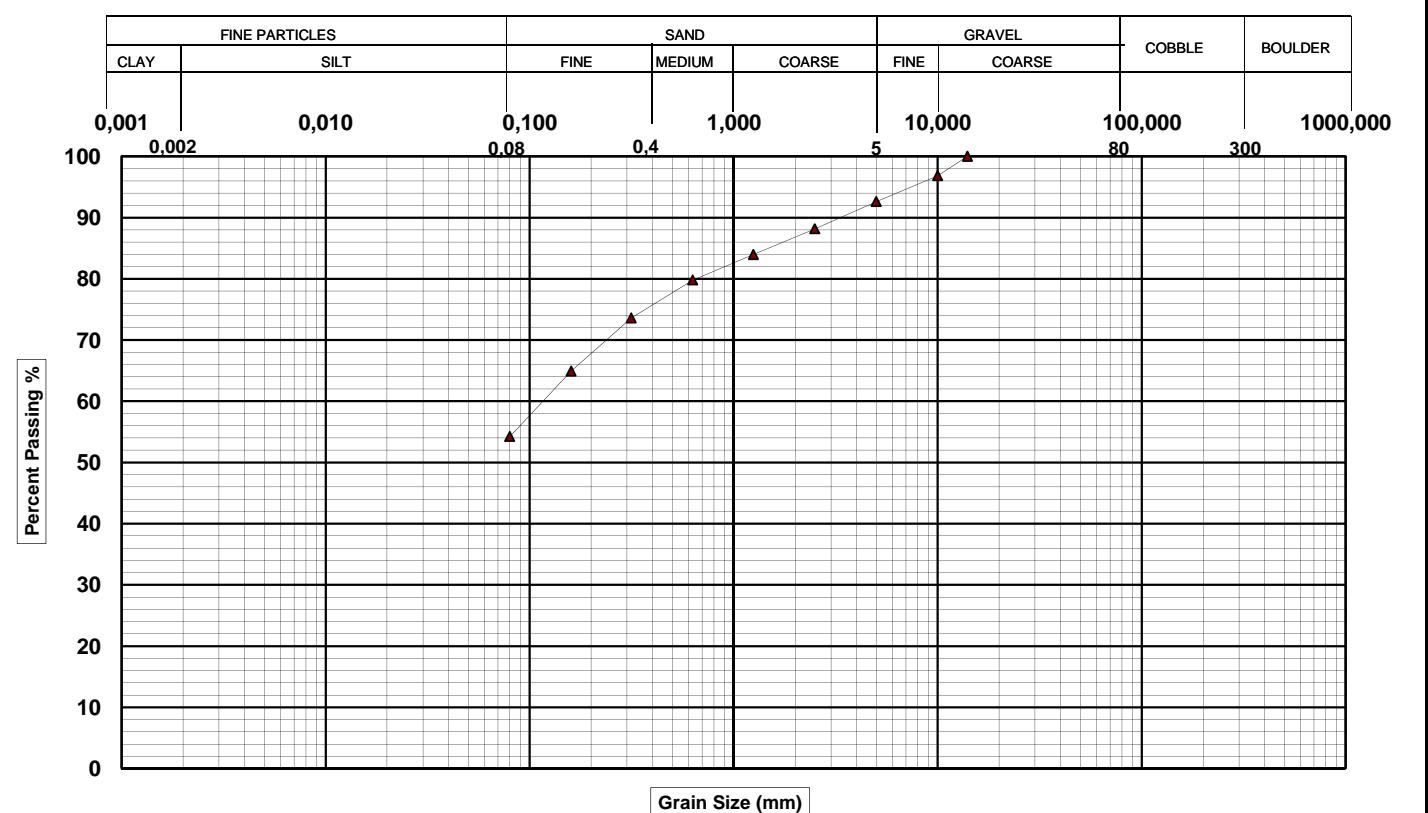
SAMPLE IDENTIFICATION										
Sample	10BH-32 (SS-07)									
Depth	4,57 - 5,18 m									
Soil Description										
Sandy silt, some gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-12

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36545



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	54,2	38,4	7,4	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,12	N/A	N/A	10

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	88		
56,00	100	1,250	84		
40,00	100	0,630	80		
31,50	100	0,315	74		
20,00	100	0,160	65		
14,00	100	0,080	54,2		
10,00	97				
5,00	93				

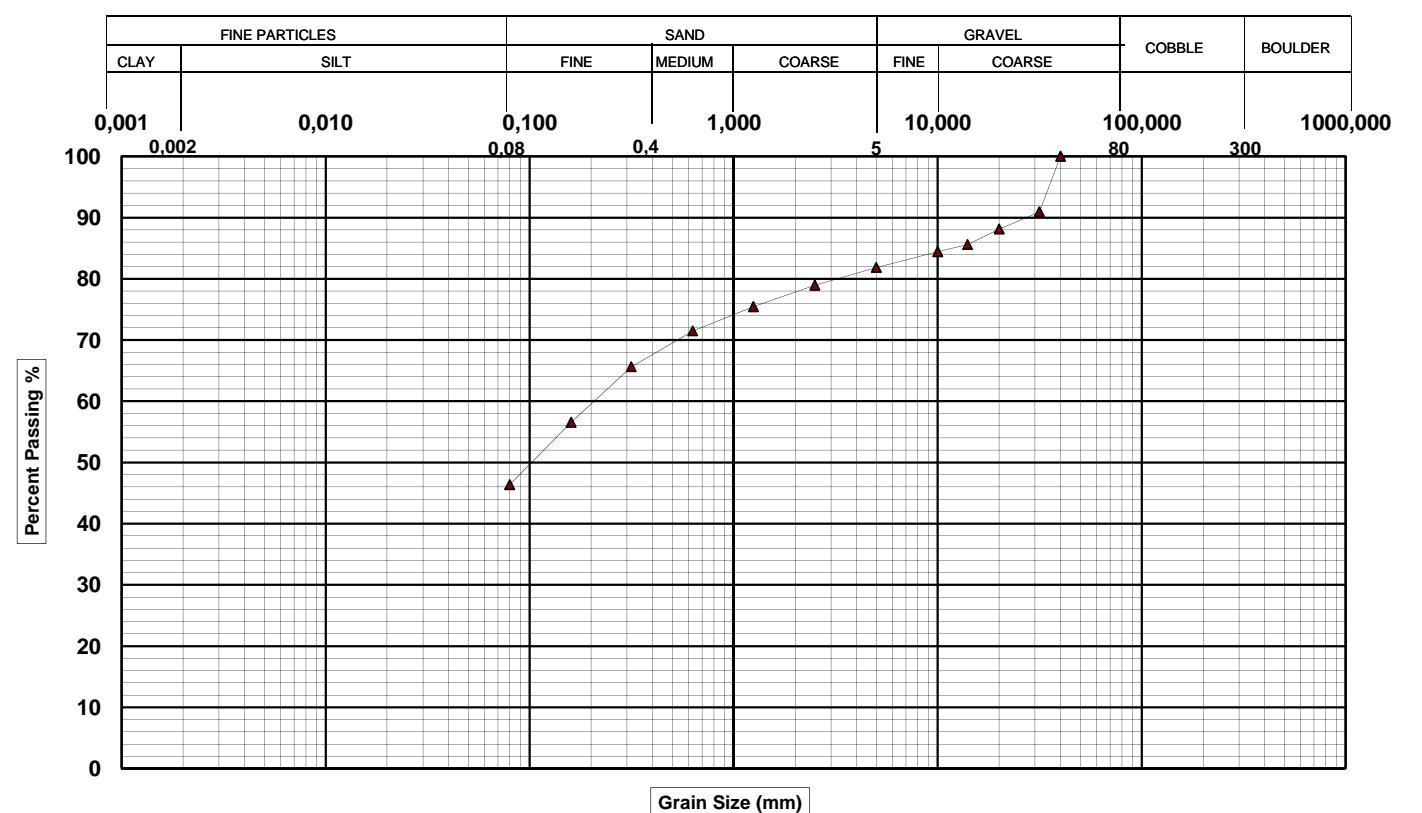
SAMPLE IDENTIFICATION										
Sample	10BH-17A (SS-07)									
Depth	5,18 - 5,79 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36535



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	46,4	35,5	18,2	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,20	N/A	N/A	9

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	79		
56,00	100	1,250	75		
40,00	100	0,630	71		
31,50	91	0,315	66		
20,00	88	0,160	57		
14,00	86	0,080	46,4		
10,00	84				
5,00	82				

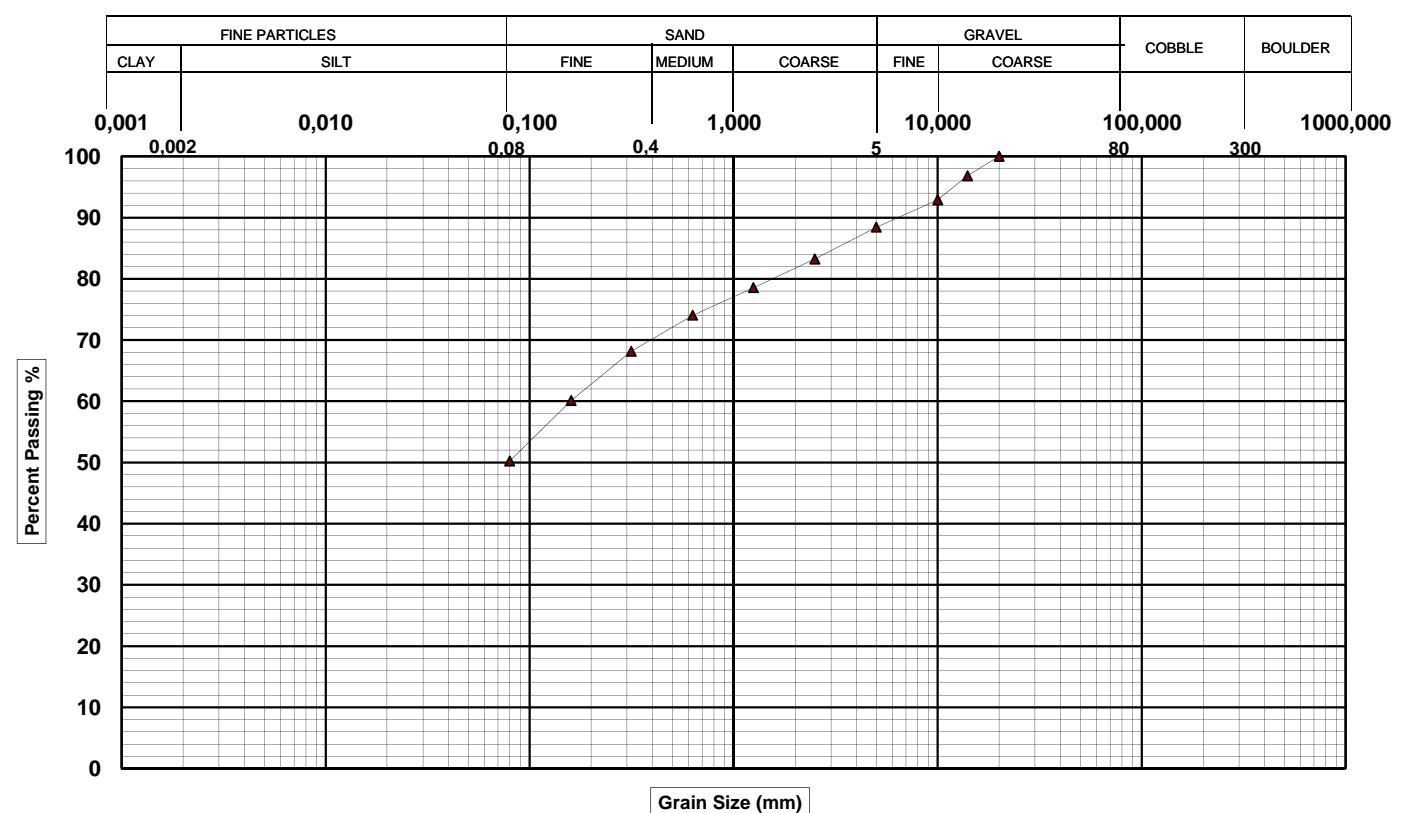
SAMPLE IDENTIFICATION										
Sample	10BH-10 (SS-04)									
Depth	2,44 - 3,05 m									
Soil Description										
Silt and sand, some gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36536



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	50,2	38,2	11,6	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,17	N/A	N/A	8

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	83		
56,00	100	1,250	79		
40,00	100	0,630	74		
31,50	100	0,315	68		
20,00	100	0,160	60		
14,00	97	0,080	50,2		
10,00	93				
5,00	88				

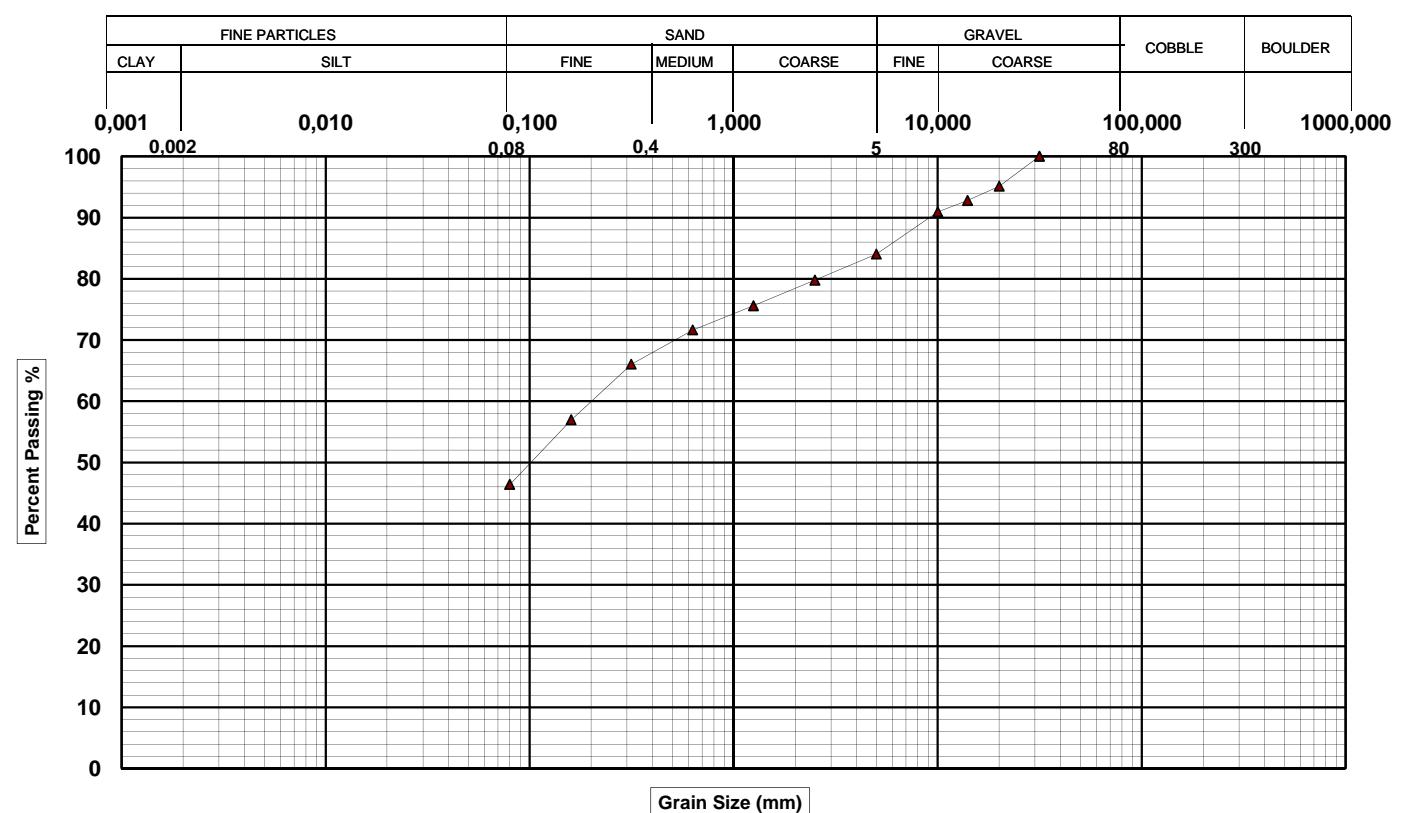
SAMPLE IDENTIFICATION										
Sample	10BH-10 (SS-08)									
Depth	6,10 - 6,71 m									
Soil Description										
Silt and sand, some gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36539

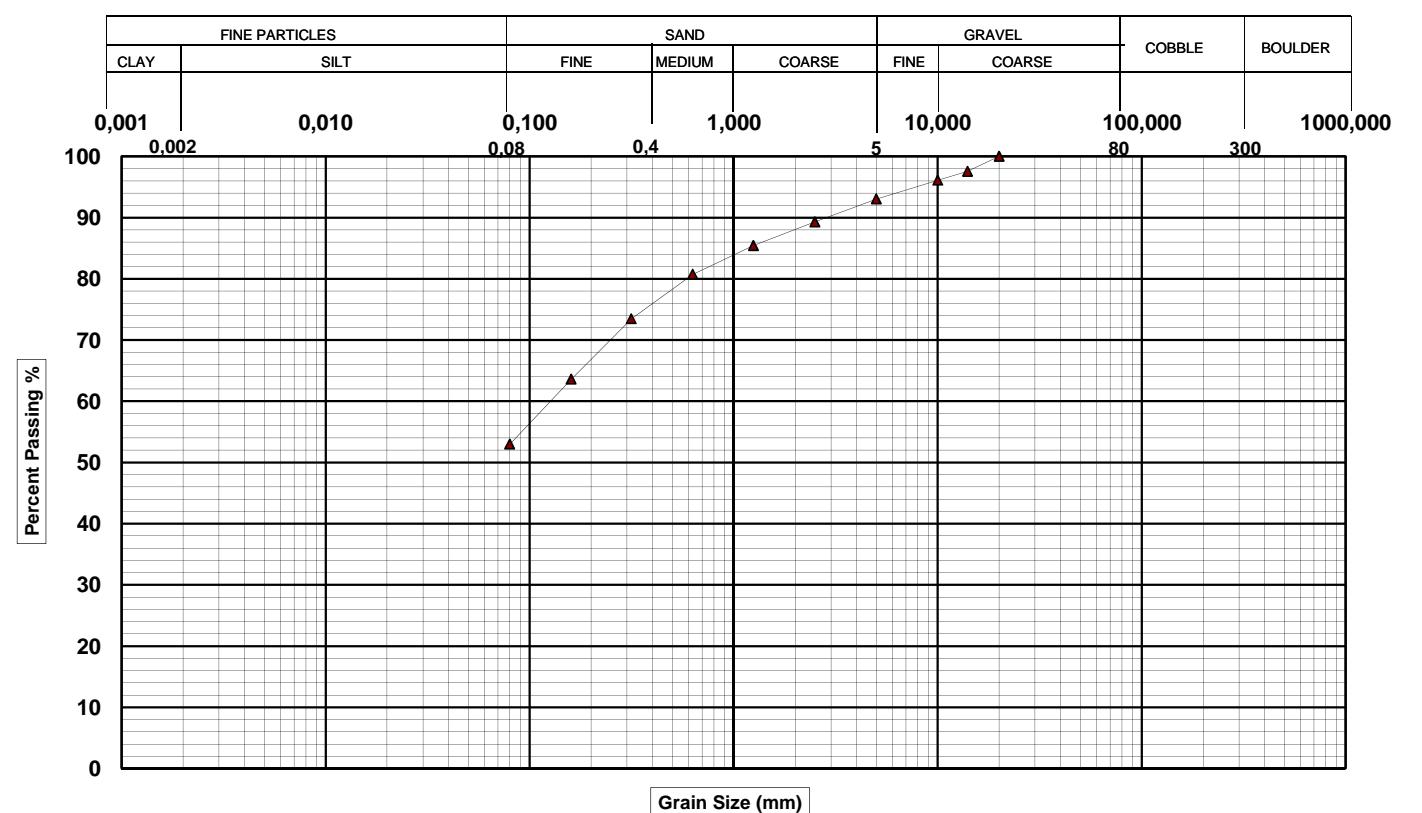


GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	46,4	37,6	16,0	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,20	N/A	N/A	9

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	80		
56,00	100	1,250	76		
40,00	100	0,630	72		
31,50	100	0,315	66		
20,00	95	0,160	57		
14,00	93	0,080	46,4		
10,00	91				
5,00	84				

SAMPLE IDENTIFICATION										
Sample	10BH-16 (SS-08)									
Depth	6,10 - 6,71 m									
Soil Description										
Silt and sand, a little gravel										

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36534



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	53,0	40,0	7,0	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,13	N/A	N/A	10

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	89		
56,00	100	1,250	85		
40,00	100	0,630	81		
31,50	100	0,315	73		
20,00	100	0,160	64		
14,00	98	0,080	53,0		
10,00	96				
5,00	93				

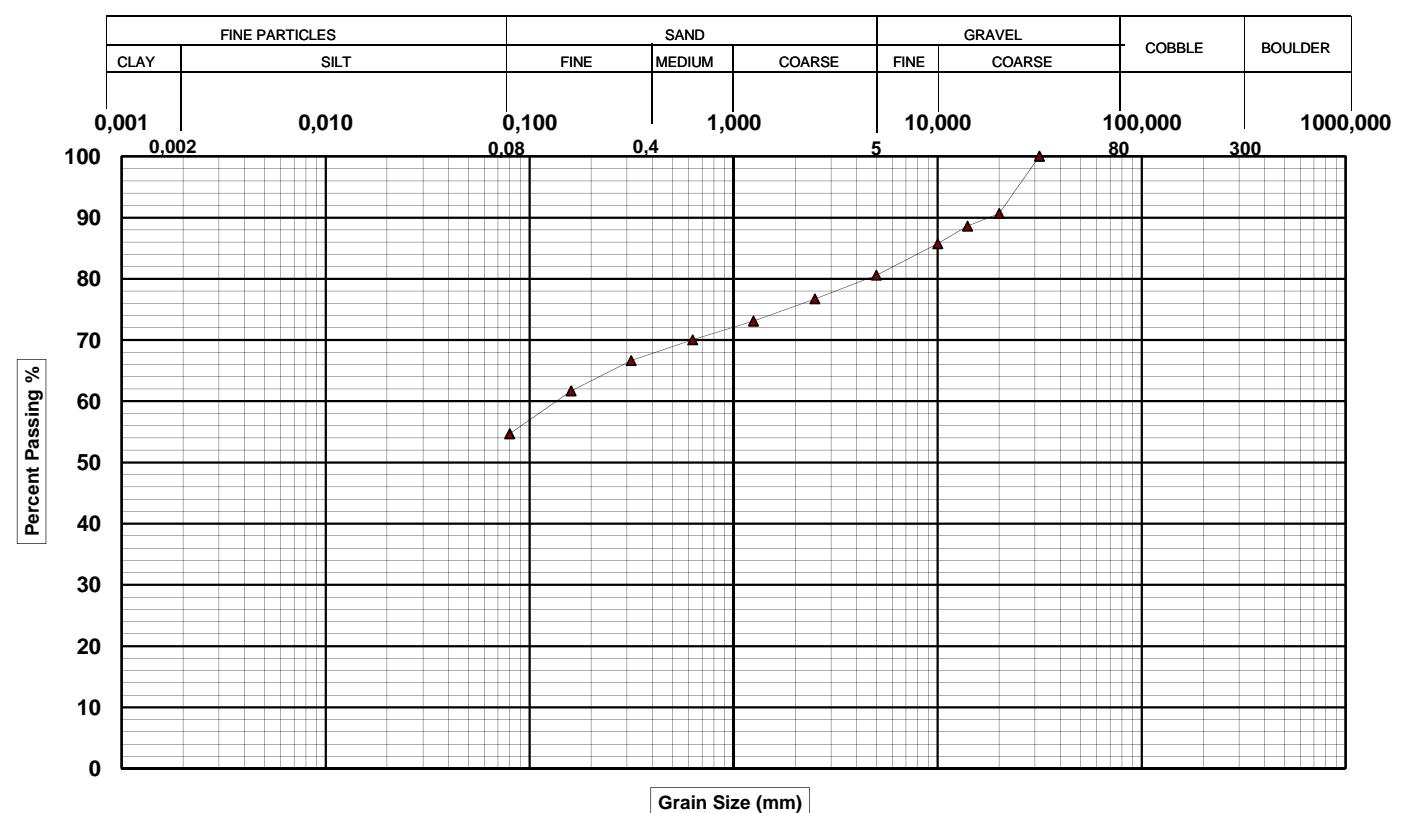
SAMPLE IDENTIFICATION										
Sample	10BH-10 (SS-02)									
Depth	0,61 - 1,22 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36537



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	54,7	25,9	19,4	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,15	N/A	N/A	11

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	77		
56,00	100	1,250	73		
40,00	100	0,630	70		
31,50	100	0,315	67		
20,00	91	0,160	62		
14,00	89	0,080	54,7		
10,00	86				
5,00	81				

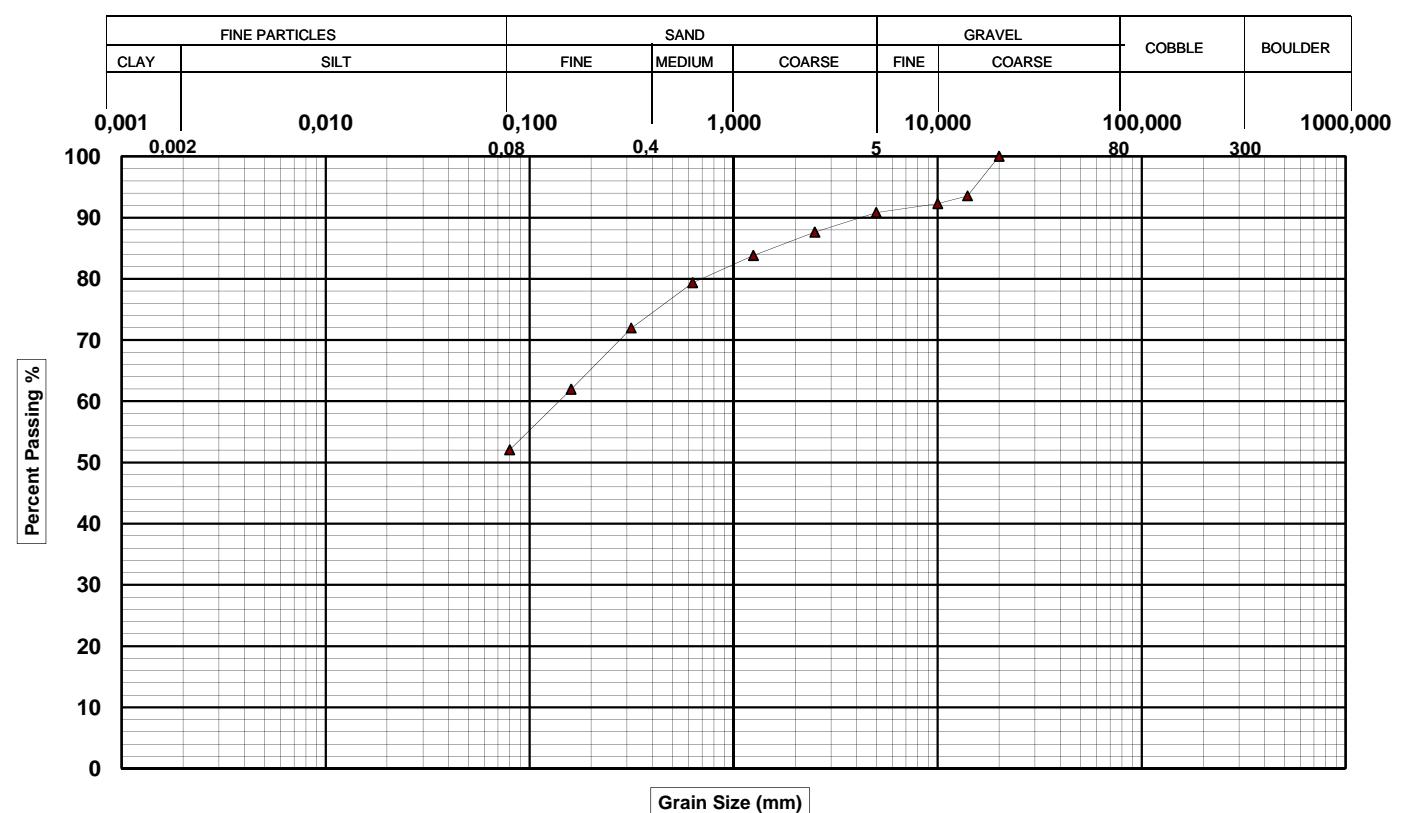
SAMPLE IDENTIFICATION										
Sample	10BH-10 (SS-16)									
Depth	16,5 - 16,927 m									
Soil Description										
Sandy silt, some gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36542



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	52,1	38,8	9,2	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,15	N/A	N/A	11

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	88		
56,00	100	1,250	84		
40,00	100	0,630	79		
31,50	100	0,315	72		
20,00	100	0,160	62		
14,00	94	0,080	52,1		
10,00	92				
5,00	91				

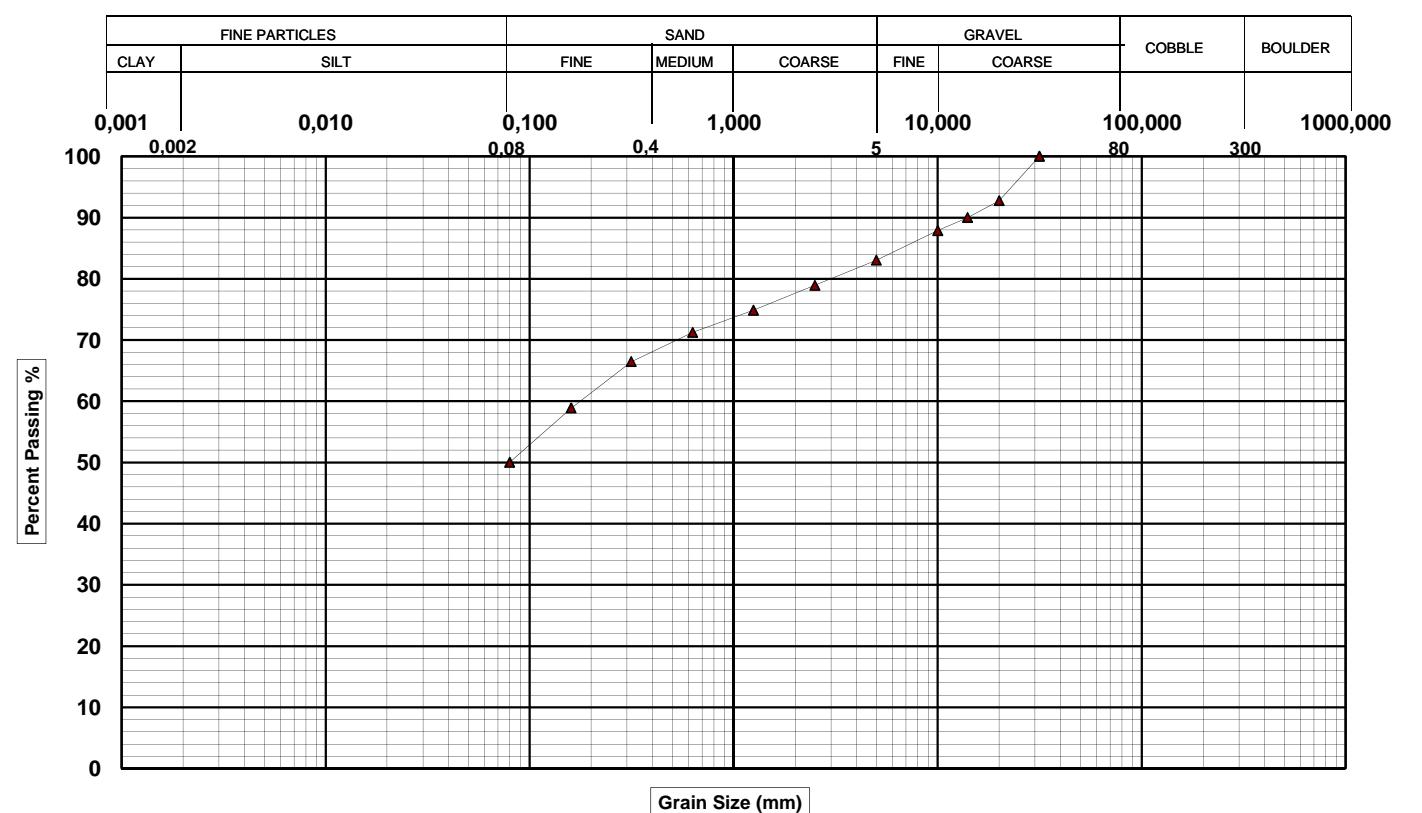
SAMPLE IDENTIFICATION										
Sample	10BH-09 (SS-03)									
Depth	1,22 - 1,83 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36543



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	50,0	33,0	17,0	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,19	N/A	N/A	10

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	79		
56,00	100	1,250	75		
40,00	100	0,630	71		
31,50	100	0,315	66		
20,00	93	0,160	59		
14,00	90	0,080	50,0		
10,00	88				
5,00	83				

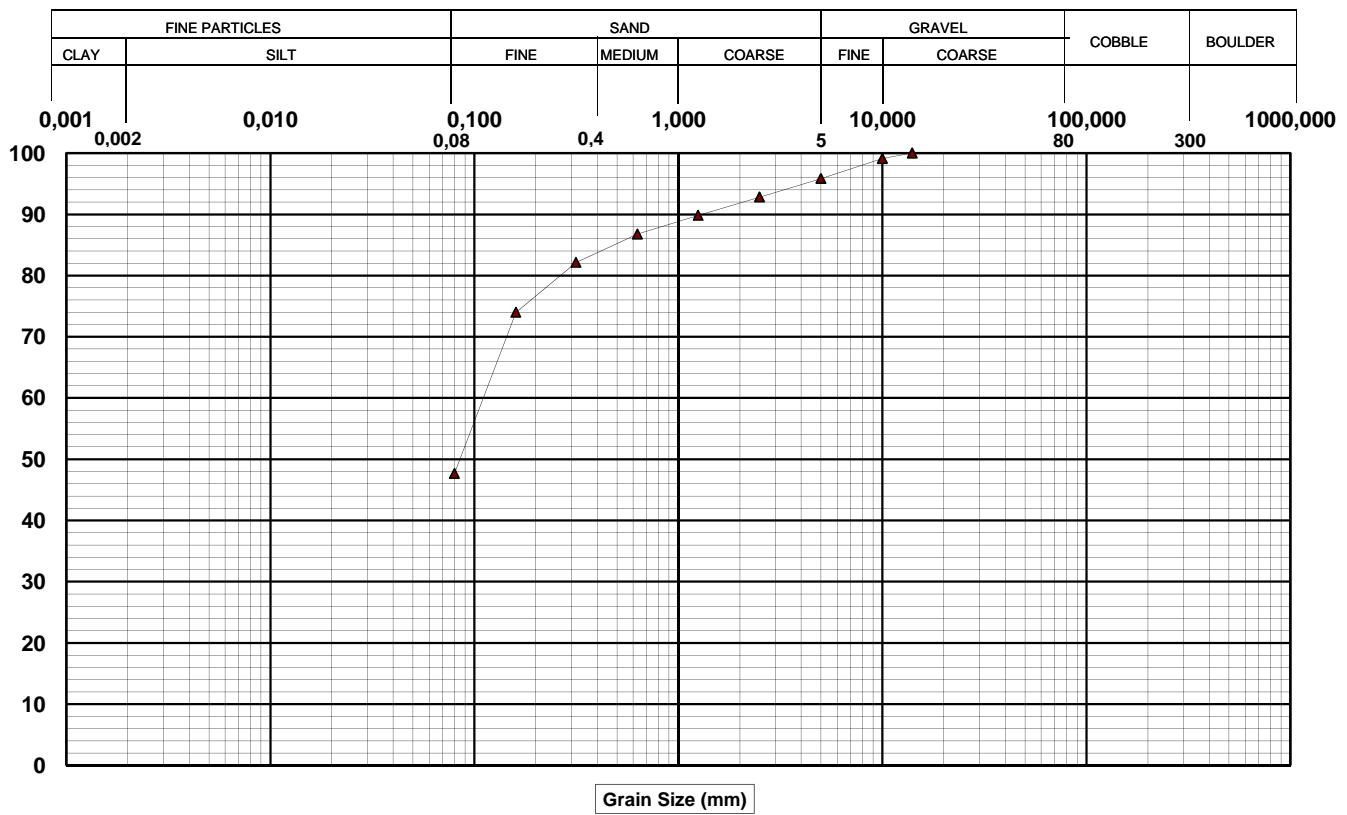
SAMPLE IDENTIFICATION										
Sample	10BH-09 (SS-07)									
Depth	4,57 - 5,18 m									
Soil Description										
Sandy silt, some gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36547



D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,11	N/A	N/A	9

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	93		
56,00	100	1,250	90		
40,00	100	0,630	87		
31,50	100	0,315	82		
20,00	100	0,160	74		
14,00	100	0,080	47,7		
10,00	99				
5,00	96				

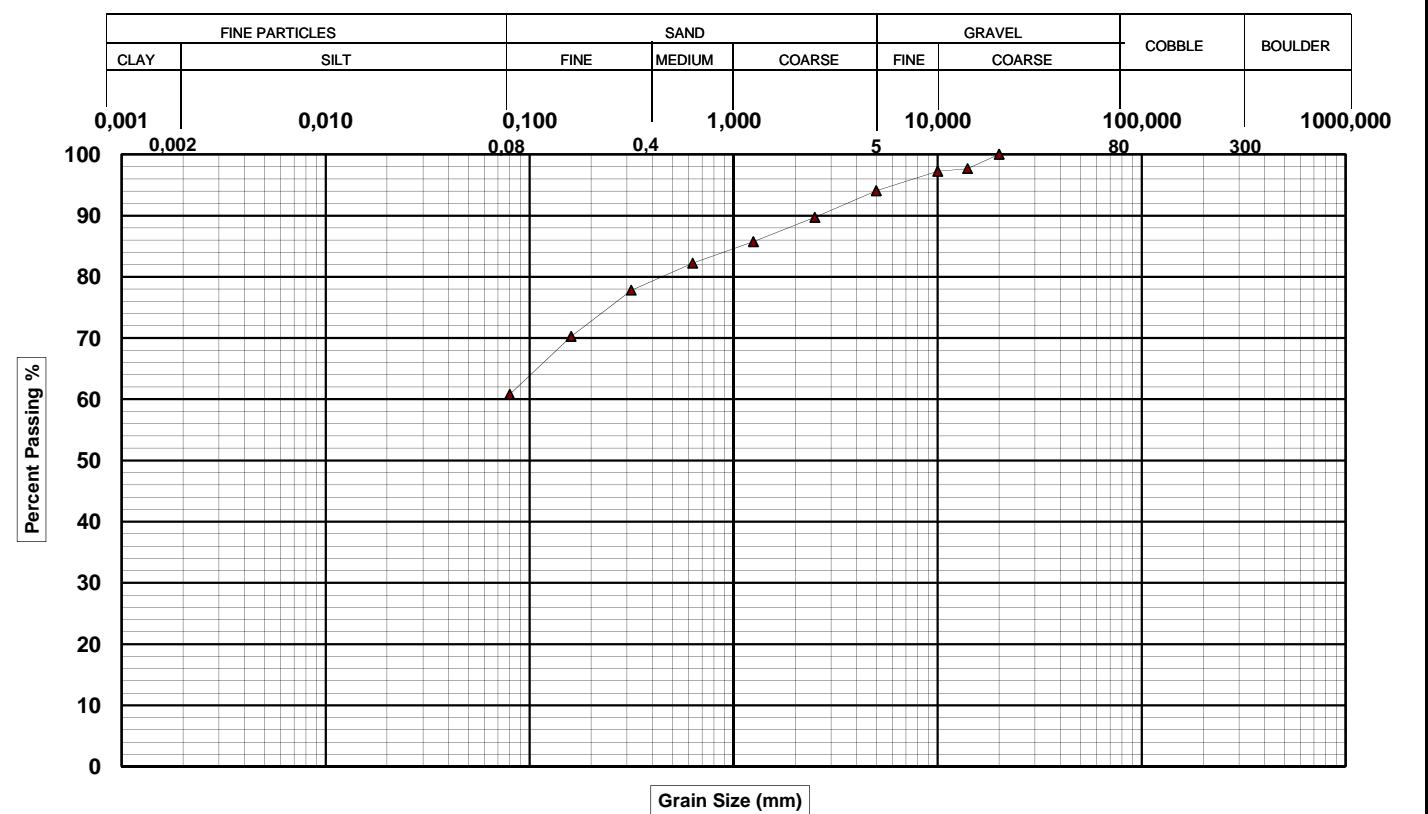
SAMPLE IDENTIFICATION	
Sample	10BH-17A (SS-10)
Depth	7,92 - 8,53 m
Soil Description	
Sand and silt, traces of gravel	

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36546



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	60,8	33,2	6,0	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	N/A	N/A	N/A	9

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	90		
56,00	100	1,250	86		
40,00	100	0,630	82		
31,50	100	0,315	78		
20,00	100	0,160	70		
14,00	98	0,080	60,8		
10,00	97				
5,00	94				

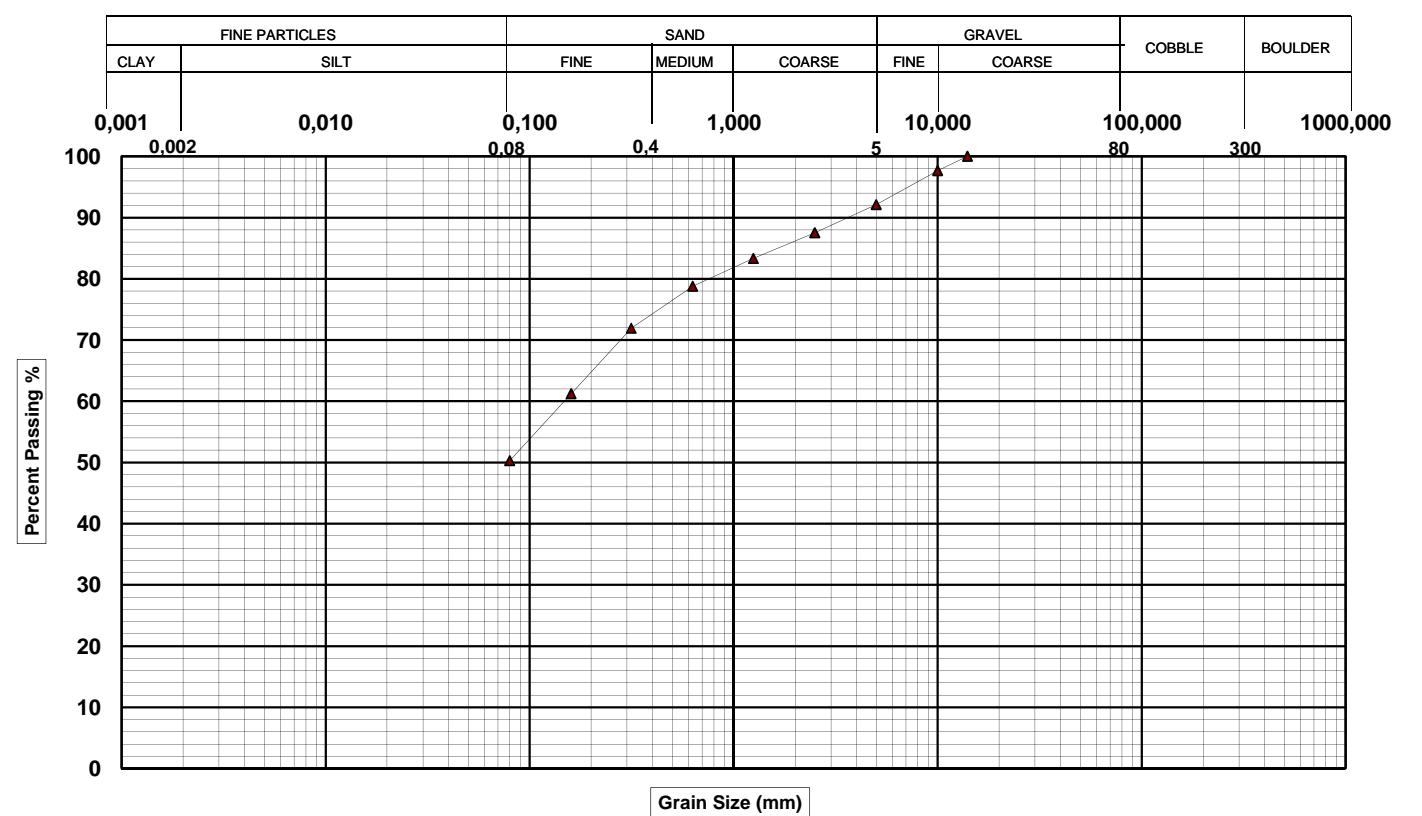
SAMPLE IDENTIFICATION										
Sample	10BH-17A (SS-12)									
Depth	9,75 - 10,36 m									
Soil Description										
Sandy silt, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36538



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	50,3	41,8	7,9	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,16	N/A	N/A	11

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	88		
56,00	100	1,250	83		
40,00	100	0,630	79		
31,50	100	0,315	72		
20,00	100	0,160	61		
14,00	100	0,080	50,3		
10,00	98				
5,00	92				

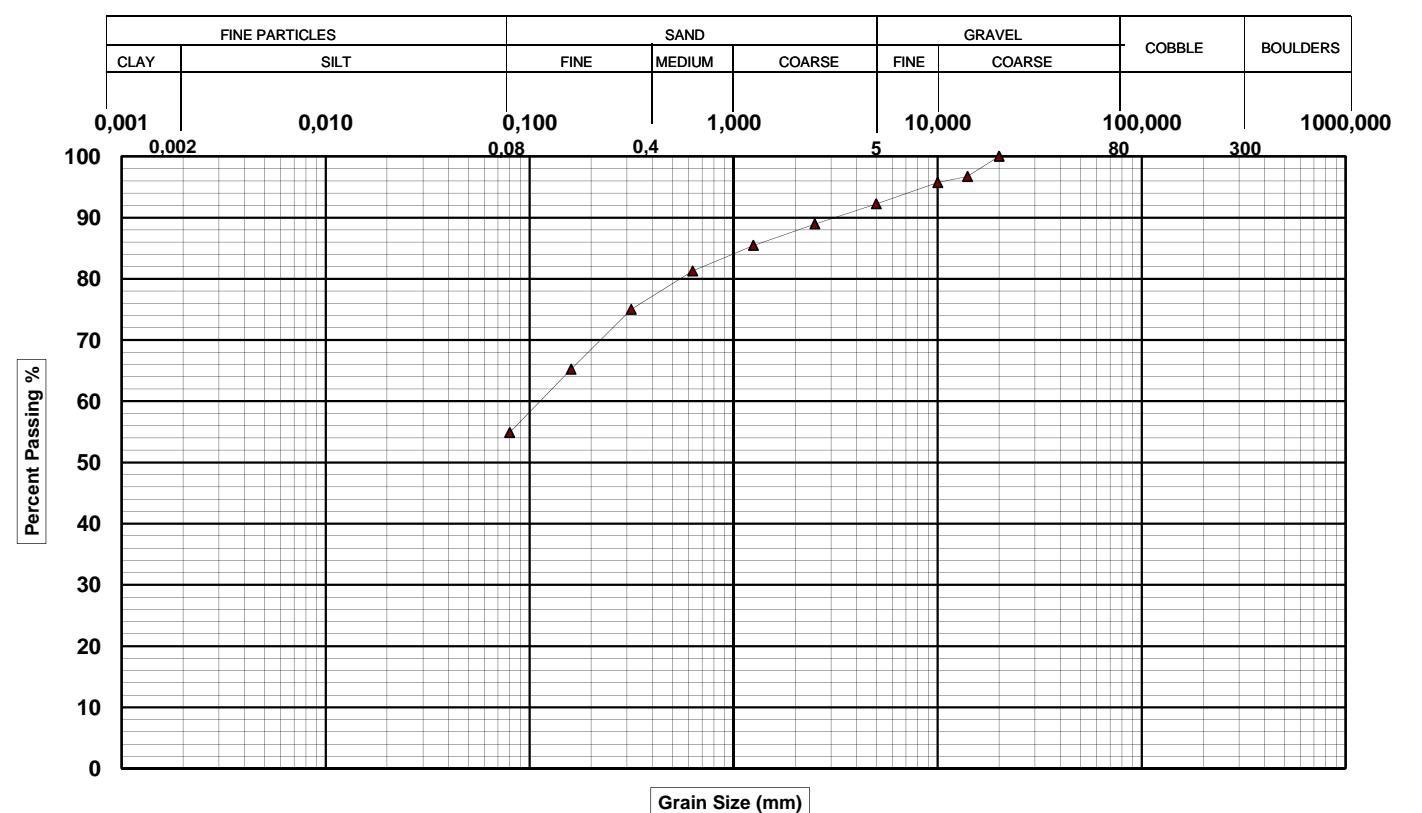
SAMPLE IDENTIFICATION										
Sample	10BH-16 (SS-03)									
Depth	1,52 - 2,13 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

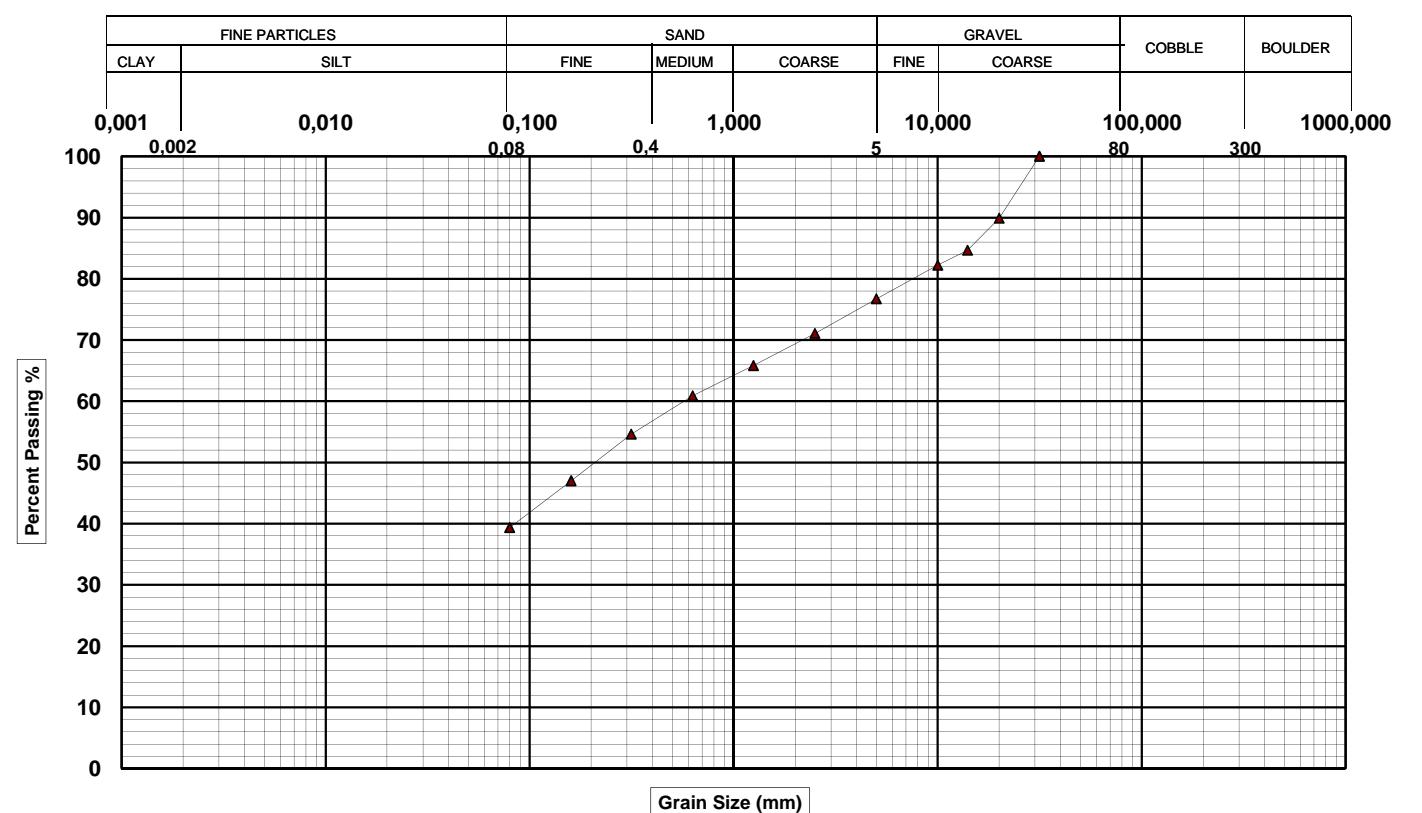
Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36553



GRAIN-SIZE DISTRIBUTION										
Fine Particles		Coarse Particles								
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)					
-	54,9	37,3	7,8	0,0	0,0					
PERCENT PASSING										
(mm)	(%)	(mm)	(%)	(mm)	(%)					
80,00	100	2,500	89							
56,00	100	1,250	85							
40,00	100	0,630	81							
31,50	100	0,315	75							
20,00	100	0,160	65							
14,00	97	0,080	54,9							
10,00	96									
5,00	92									
SAMPLE IDENTIFICATION										
Sample	10BH-08 (SS-04)									
Depth	2,44 - 3,05 m									
Soil Description										
Silt and sand, traces of gravel										

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36554



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	39,4	37,4	23,3	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,60	N/A	N/A	8

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	71		
56,00	100	1,250	66		
40,00	100	0,630	61		
31,50	100	0,315	55		
20,00	90	0,160	47		
14,00	85	0,080	39,4		
10,00	82				
5,00	77				

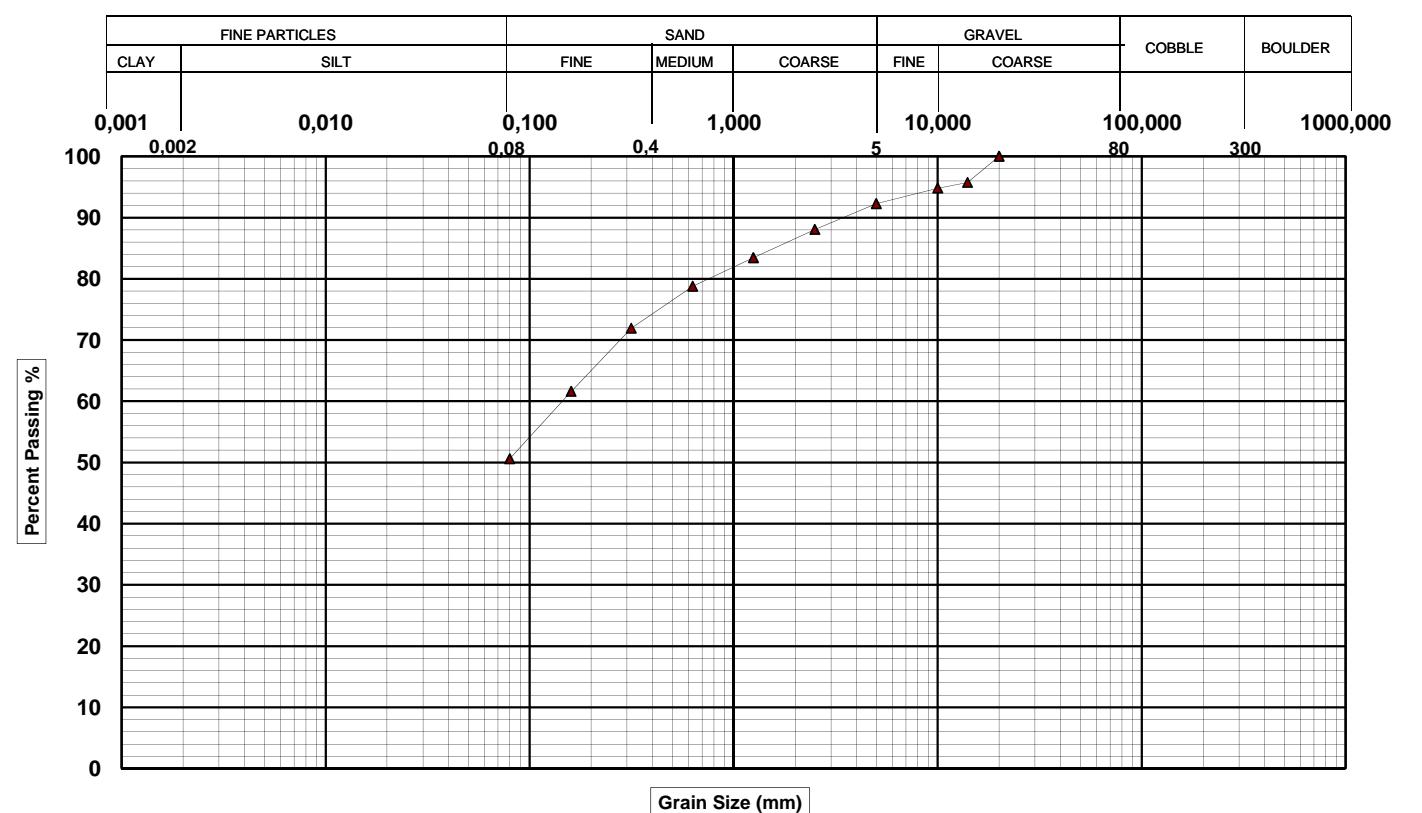
SAMPLE IDENTIFICATION										
Sample	10BH-07 (SS-09)									
Depth	7,01 - 7,62 m									
Soil Description										
Gravelly silt and sand										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36552



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	50,6	41,7	7,7	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,15	N/A	N/A	11

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	88		
56,00	100	1,250	83		
40,00	100	0,630	79		
31,50	100	0,315	72		
20,00	100	0,160	62		
14,00	96	0,080	50,6		
10,00	95				
5,00	92				

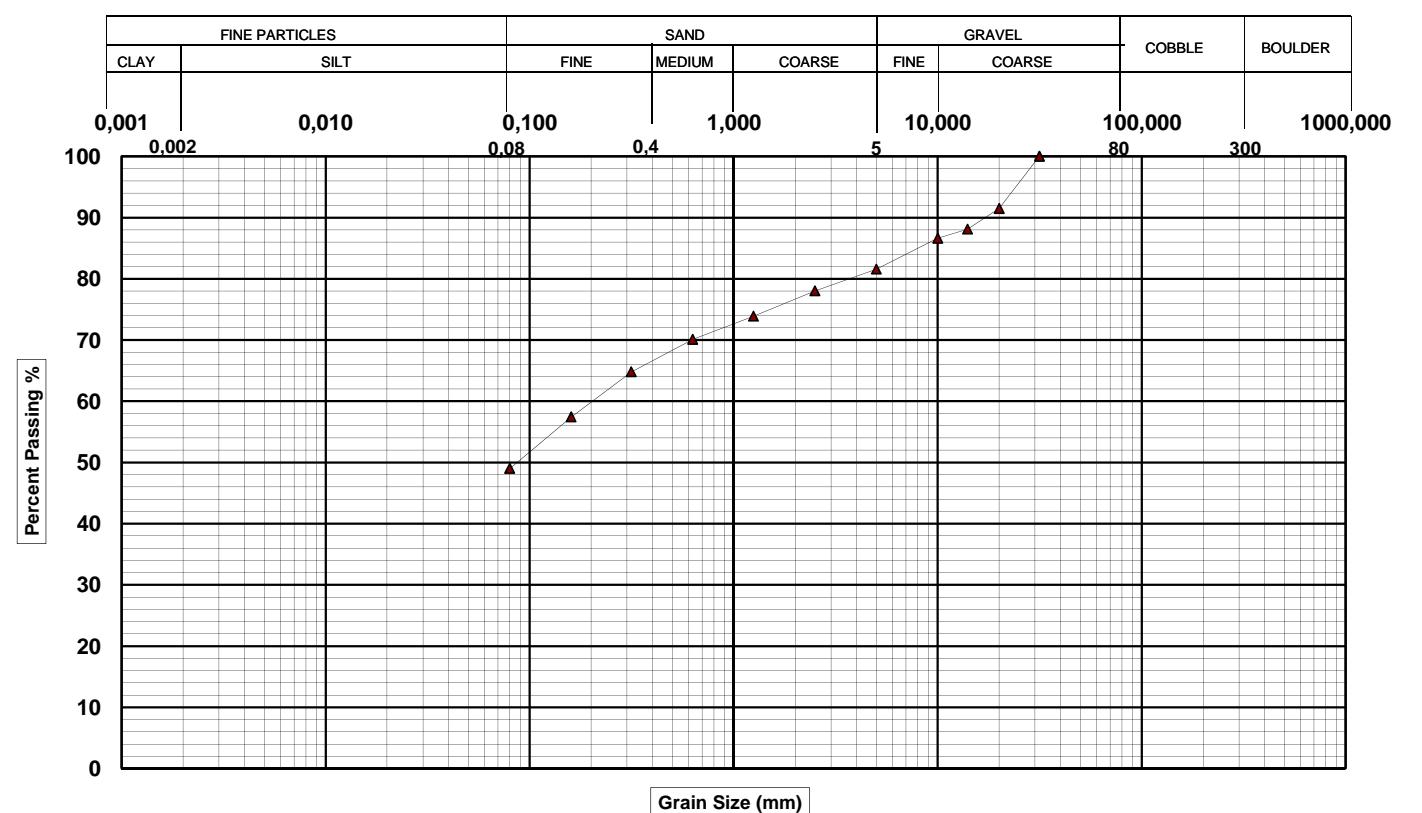
SAMPLE IDENTIFICATION										
Sample	10BH-07 (SS-02)									
Depth	0,61 - 1,22 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36550



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	49,0	32,6	18,4	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,20	N/A	N/A	7

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	78		
56,00	100	1,250	74		
40,00	100	0,630	70		
31,50	100	0,315	65		
20,00	91	0,160	57		
14,00	88	0,080	49,0		
10,00	87				
5,00	82				

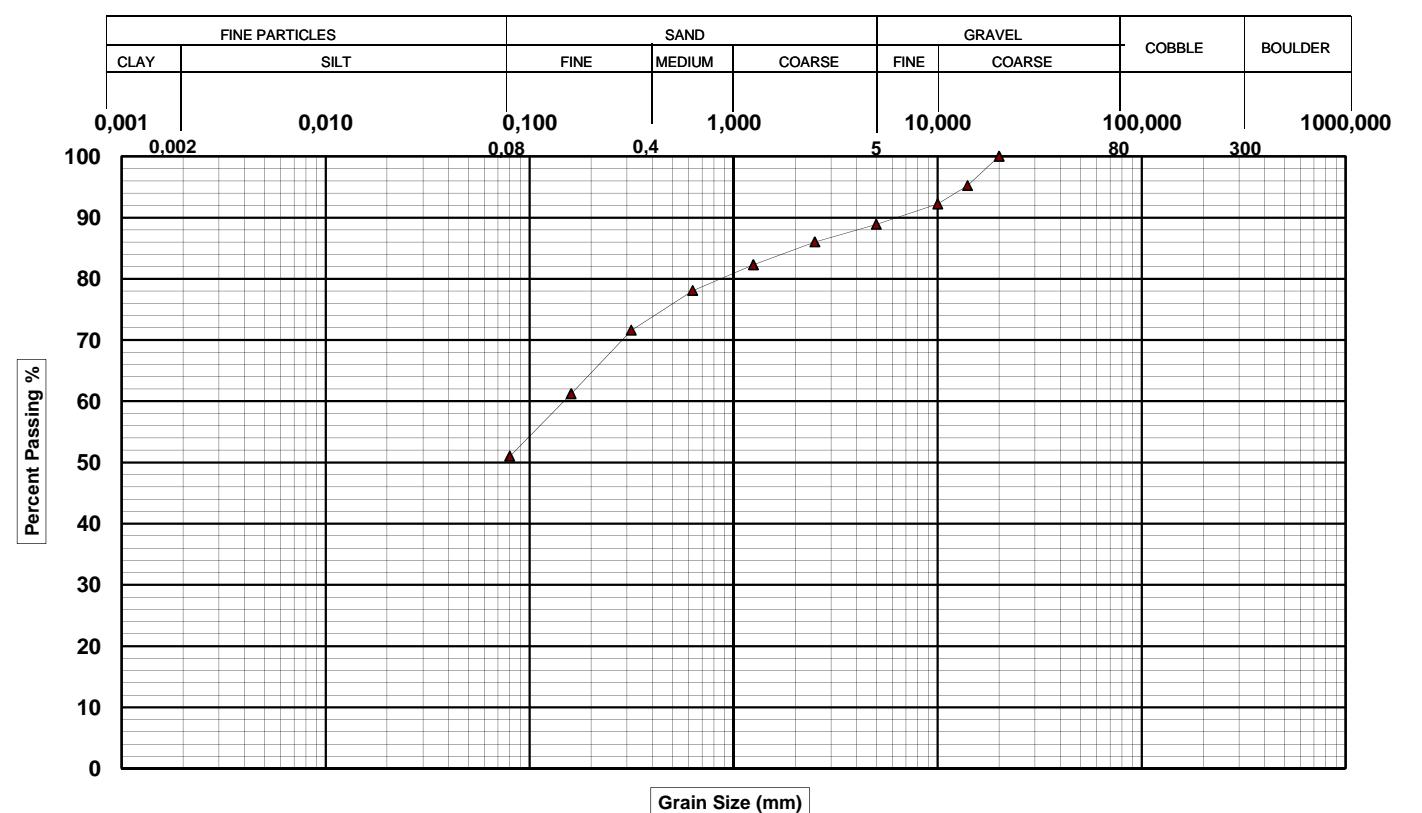
SAMPLE IDENTIFICATION										
Sample	10BH-18 (SS-07)									
Depth	5,18 - 5,74 m									
Soil Description										
Sandy silt some gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36548



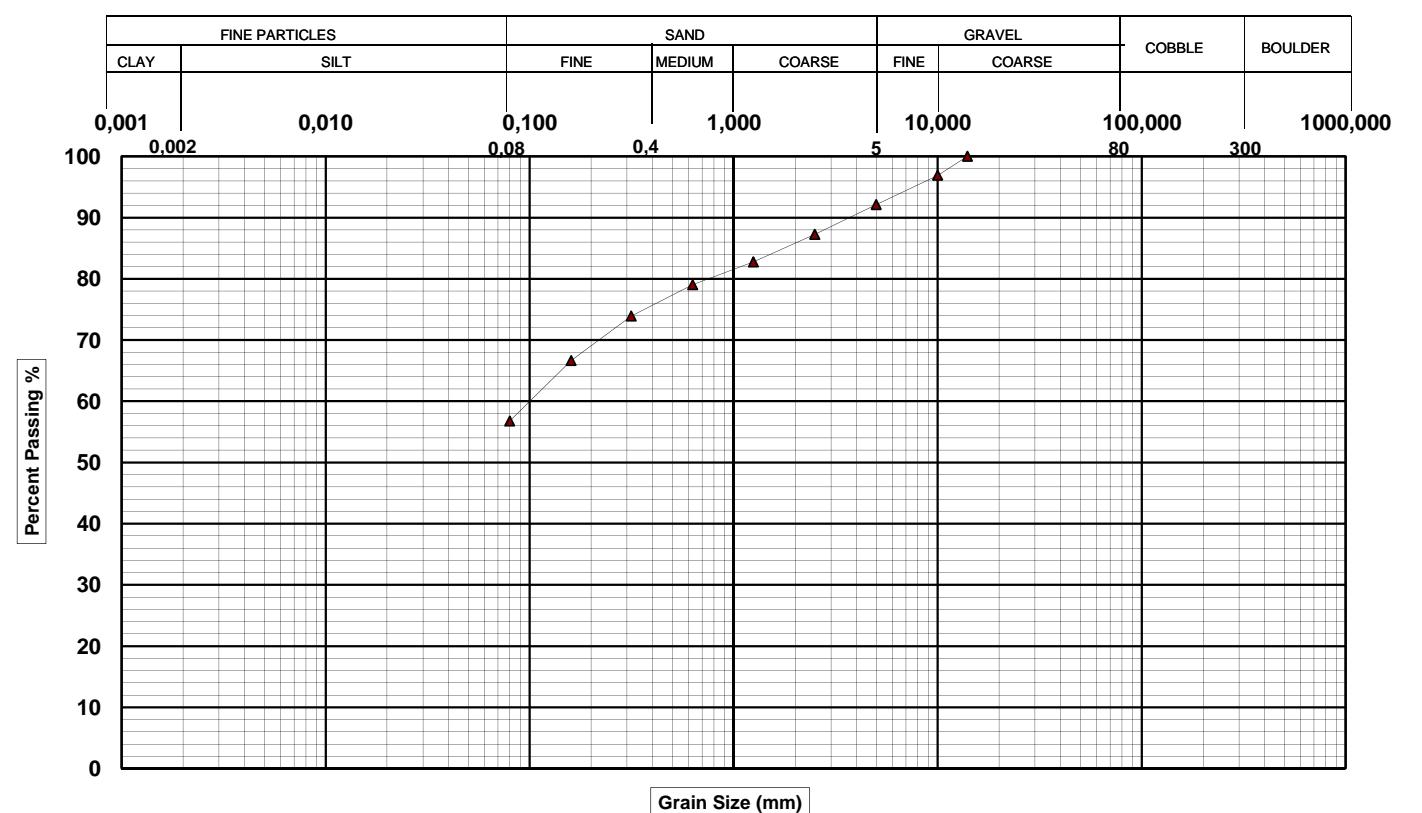
GRAIN-SIZE DISTRIBUTION										
Fine Particles		Coarse Particles								
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)					
-	51,0	37,9	11,1	0,0	0,0					
PERCENT PASSING										
(mm)	(%)	(mm)	(%)	(mm)	(%)					
80,00	100	2,500	86							
56,00	100	1,250	82							
40,00	100	0,630	78							
31,50	100	0,315	72							
20,00	100	0,160	61							
14,00	95	0,080	51,0							
10,00	92									
5,00	89									
SAMPLE IDENTIFICATION										
Sample	10BH-18 (SS-02)									
Depth	0,61 - 1,22 m									
Soil Description										
Silt and sand, some gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36549



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	56,8	35,3	7,9	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,10	N/A	N/A	10

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	87		
56,00	100	1,250	83		
40,00	100	0,630	79		
31,50	100	0,315	74		
20,00	100	0,160	67		
14,00	100	0,080	56,8		
10,00	97				
5,00	92				

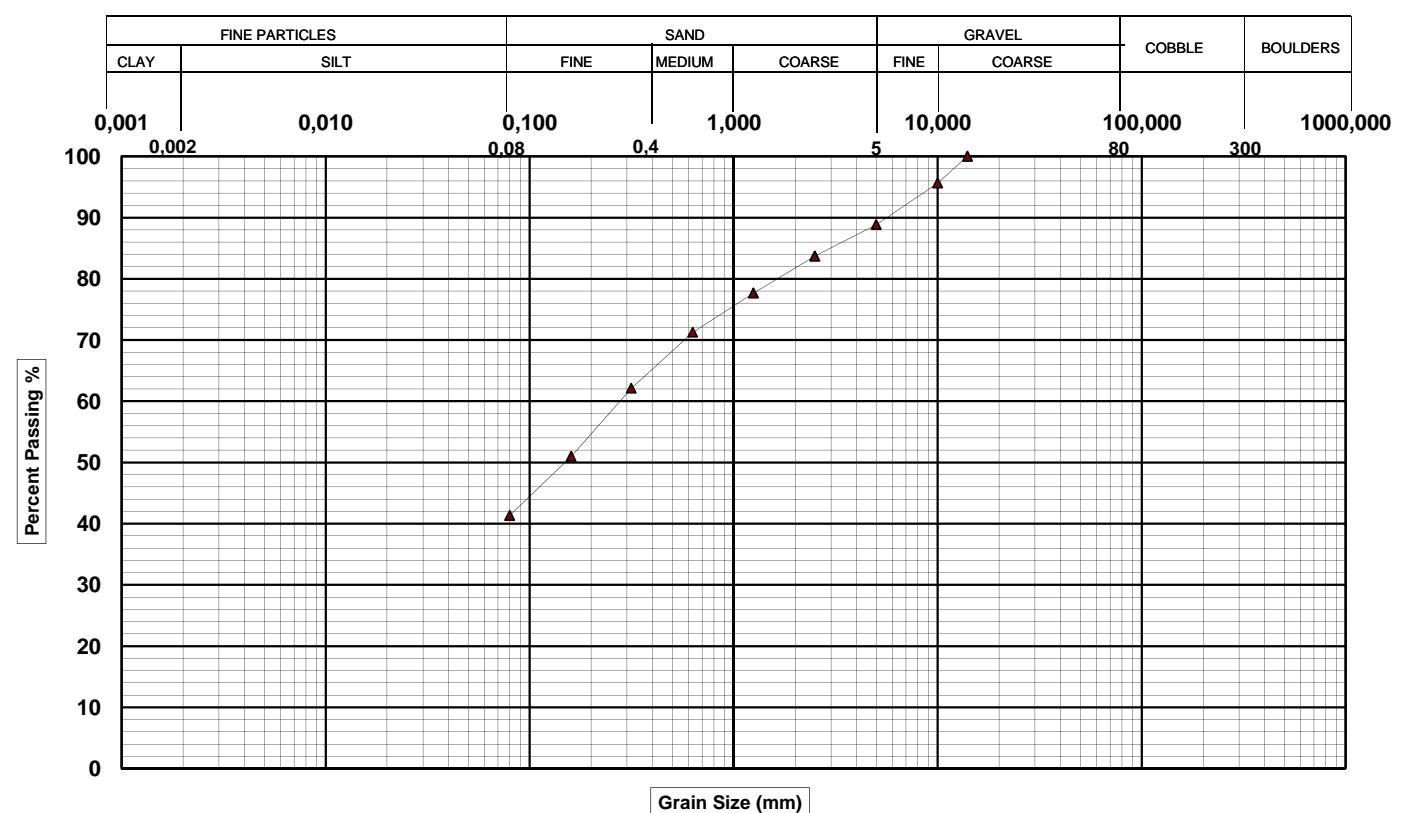
SAMPLE IDENTIFICATION										
Sample	10BH-18 (SS-05)									
Depth	3,35 - 3,96 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-14

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36887



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	41,3	47,5	11,2	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,29	N/A	N/A	11

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	84		
56,00	100	1,250	78		
40,00	100	0,630	71		
31,50	100	0,315	62		
20,00	100	0,160	51		
14,00	100	0,080	41,3		
10,00	96				
5,00	89				

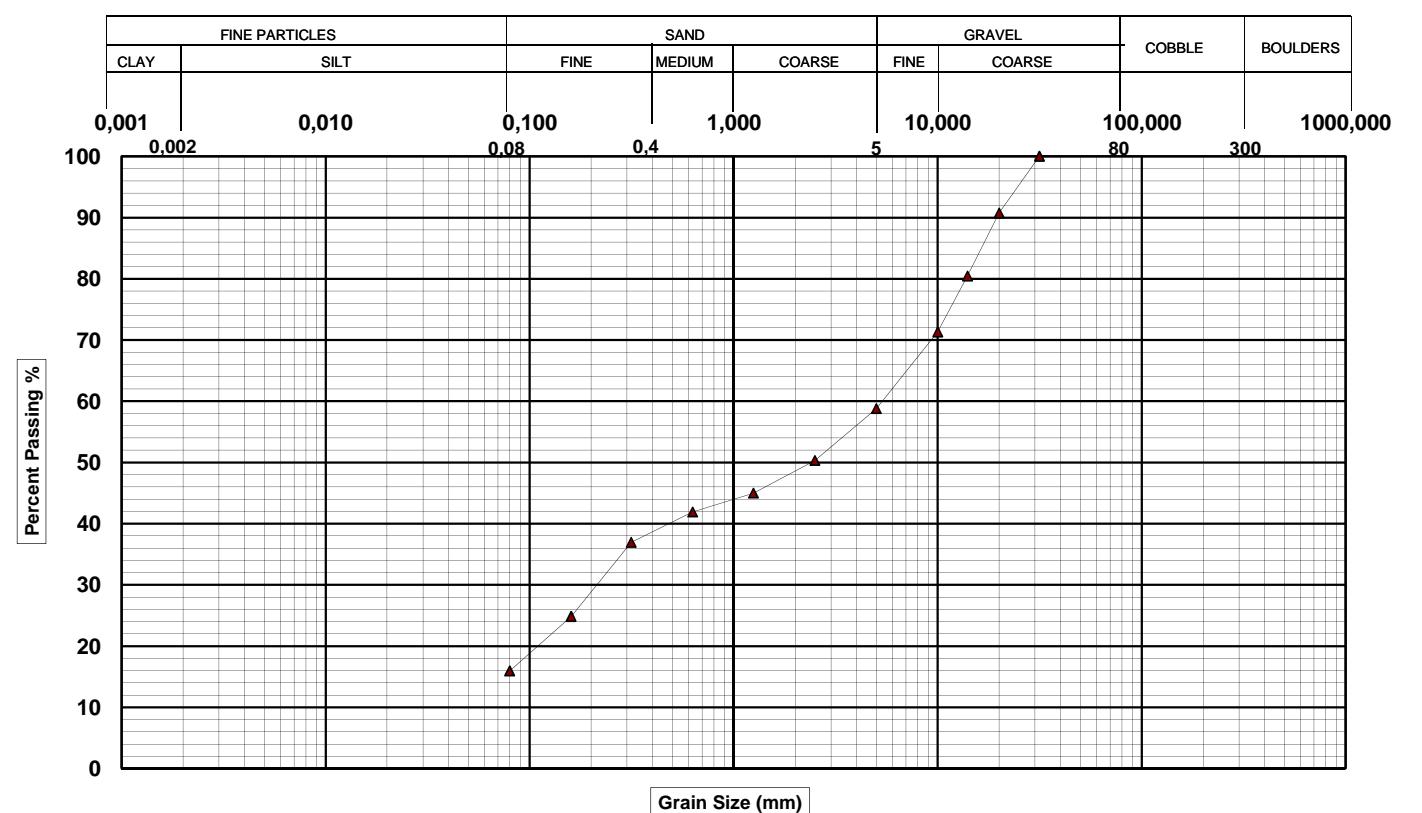
SAMPLE IDENTIFICATION										
Sample	10BH-27 (SS-06)									
Depth	5,18 - 5,79 m									
Soil Description										
Sand and silt, some gravel										

Prepared by Benoit St-Pierre, tech.

Approved by Ibrahim Ja'far, ing.

Date 2010-05-05

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36888



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	16,0	42,8	41,2	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	0,22	5,30	N/A	N/A	9

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	50		
56,00	100	1,250	45		
40,00	100	0,630	42		
31,50	100	0,315	37		
20,00	91	0,160	25		
14,00	80	0,080	16,0		
10,00	71				
5,00	59				

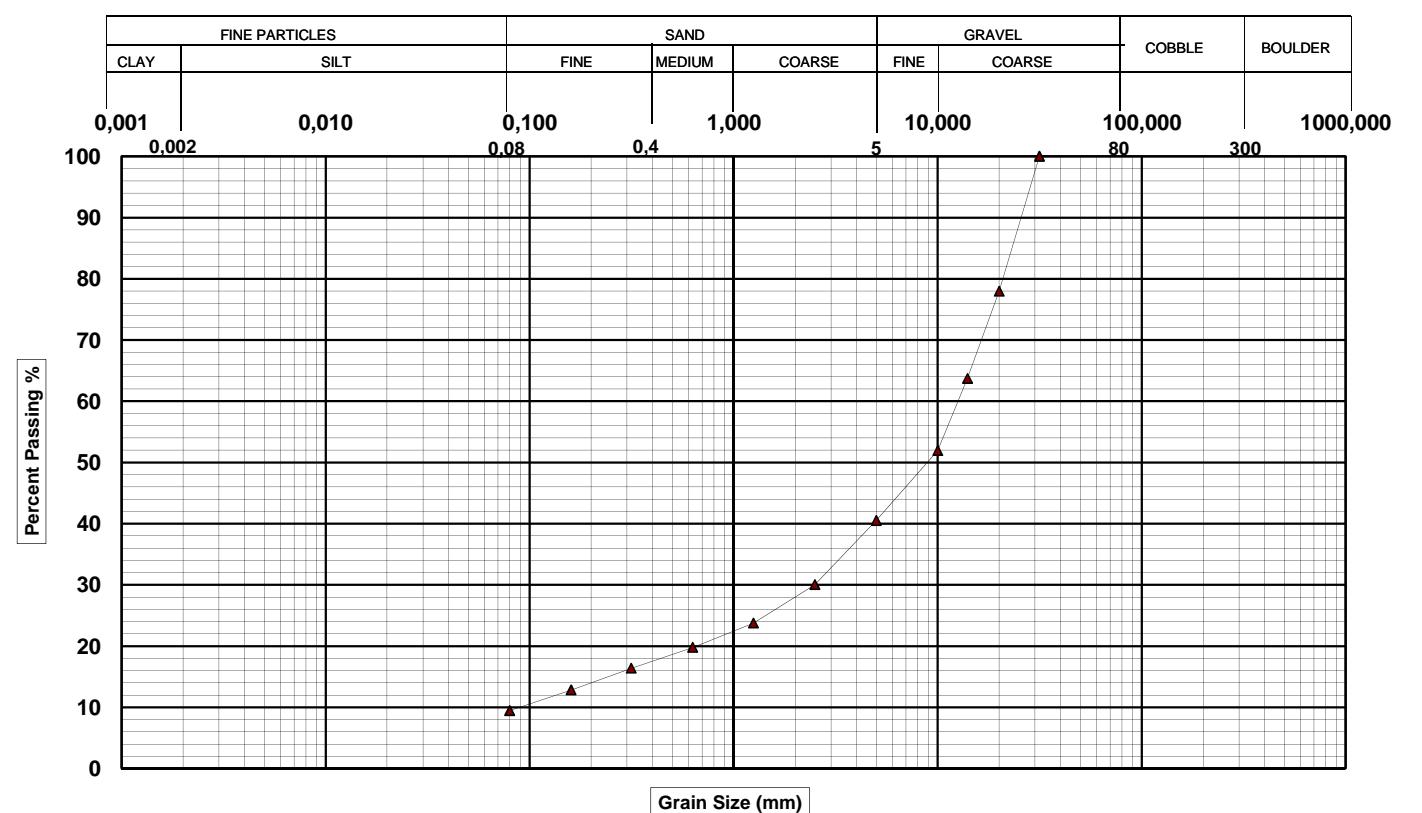
SAMPLE IDENTIFICATION										
Sample	10BH-27 (SS-10)									
Depth	9,14 - 9,75 m									
Soil Description										
sand and gravel, some silt										

Prepared by Benoit St-Pierre, tech.

Approved by Ibrahim Ja'far, ing.

Date 2010-05-05

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36891



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	9,4	31,1	59,5	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
0,090	2,50	13,00	144,44	5,34	7

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	30		
56,00	100	1,250	24		
40,00	100	0,630	20		
31,50	100	0,315	16		
20,00	78	0,160	13		
14,00	64	0,080	9,4		
10,00	52				
5,00	41				

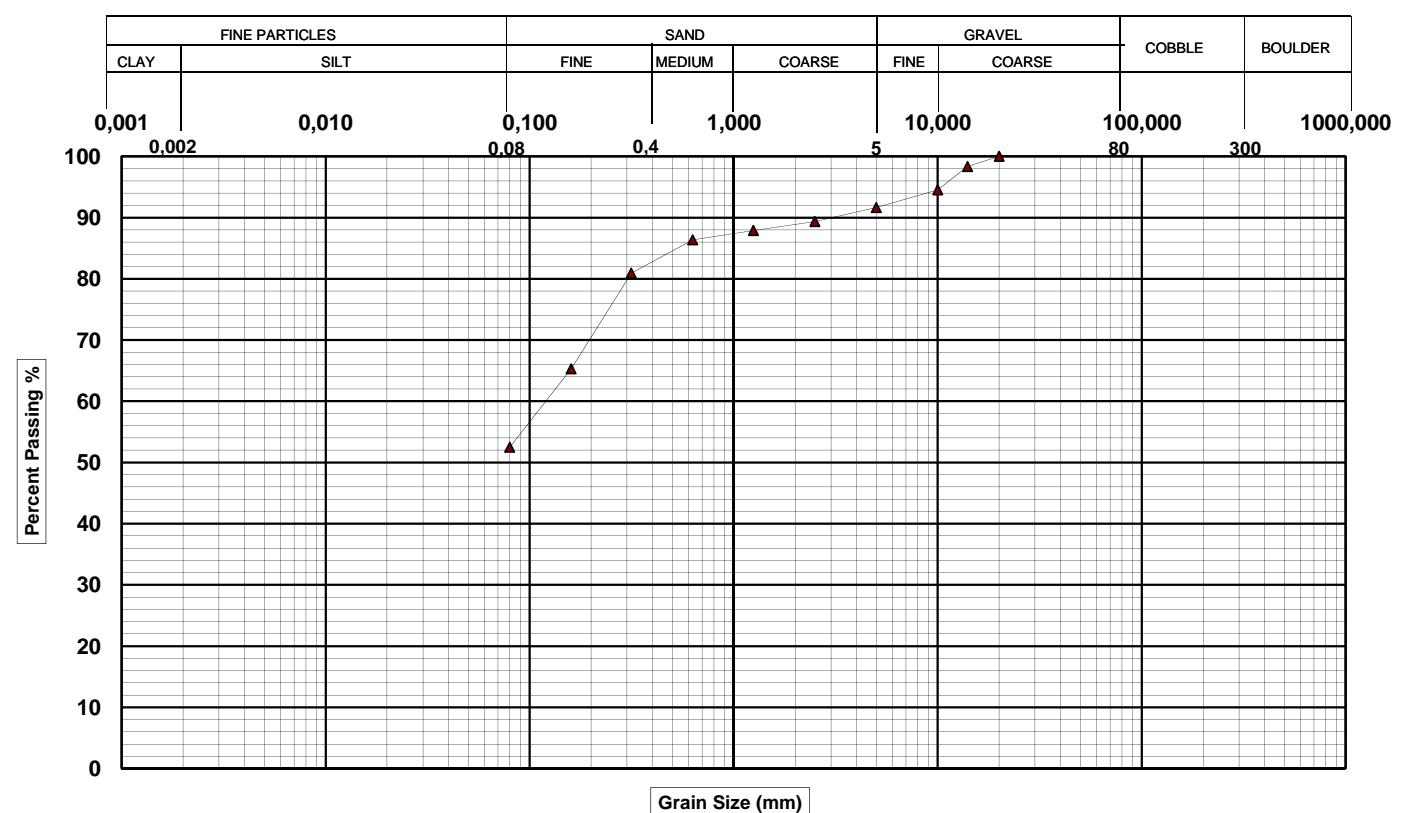
SAMPLE IDENTIFICATION										
Sample	10BH-28A (SS-08)									
Depth	6,48 - 7,09 m									
Soil Description										
Sandy gravel, traces of silt										

Prepared by Benoit St-Pierre, tech.

Approved by Ibrahim Ja'far, ing.

Date 2010-05-05

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36892



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	52,5	39,2	8,4	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,12	N/A	N/A	14

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	89		
56,00	100	1,250	88		
40,00	100	0,630	86		
31,50	100	0,315	81		
20,00	100	0,160	65		
14,00	98	0,080	52,5		
10,00	95				
5,00	92				

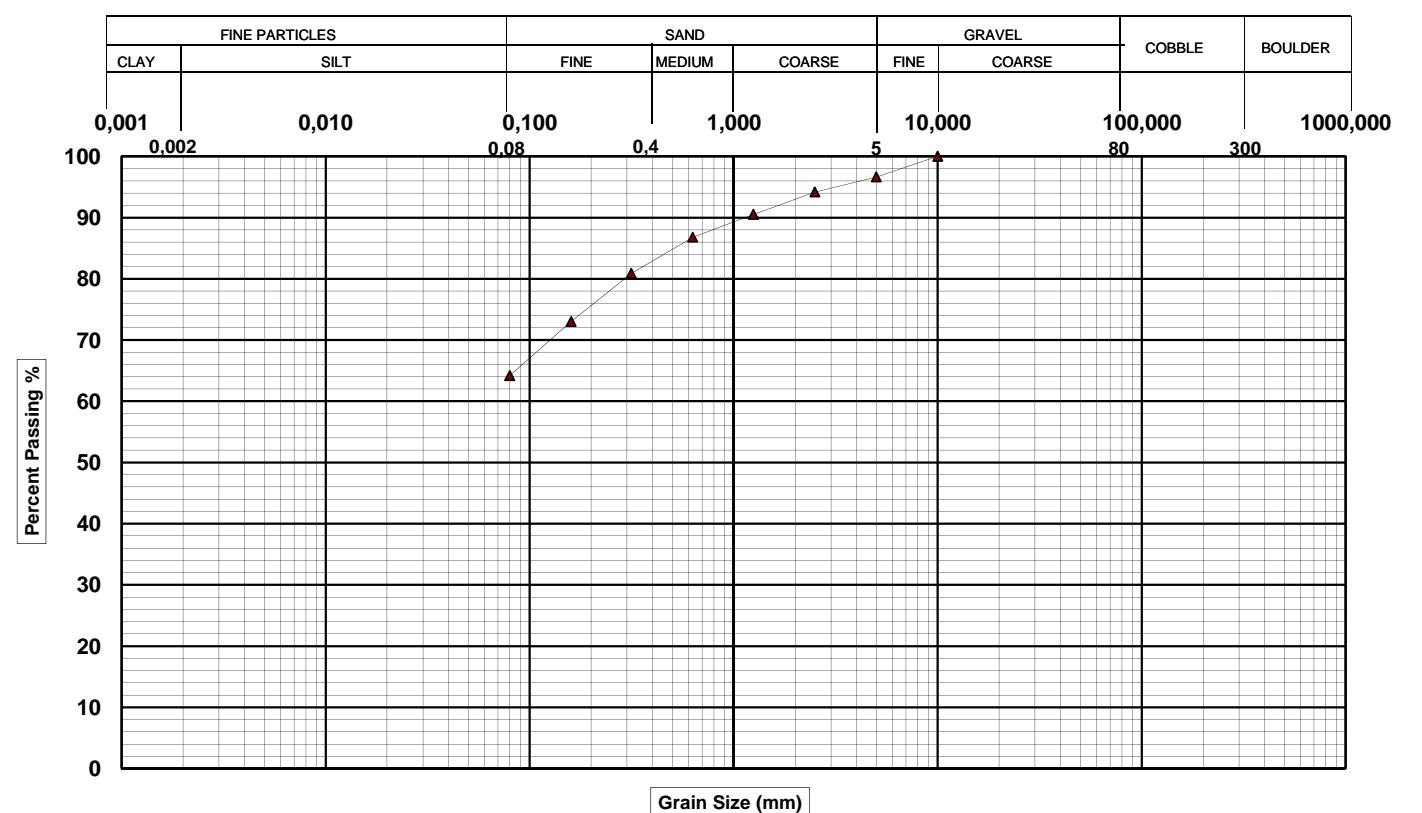
SAMPLE IDENTIFICATION										
Sample	10BH-28A (SS-11)									
Depth	9,14 - 9,75 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-Pierre, tech.

Approved by Ibrahim Ja'far, ing.

Date 2010-05-05

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36867



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	64,2	32,4	3,4	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	N/A	N/A	N/A	12

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	94		
56,00	100	1,250	91		
40,00	100	0,630	87		
31,50	100	0,315	81		
20,00	100	0,160	73		
14,00	100	0,080	64,2		
10,00	100				
5,00	97				

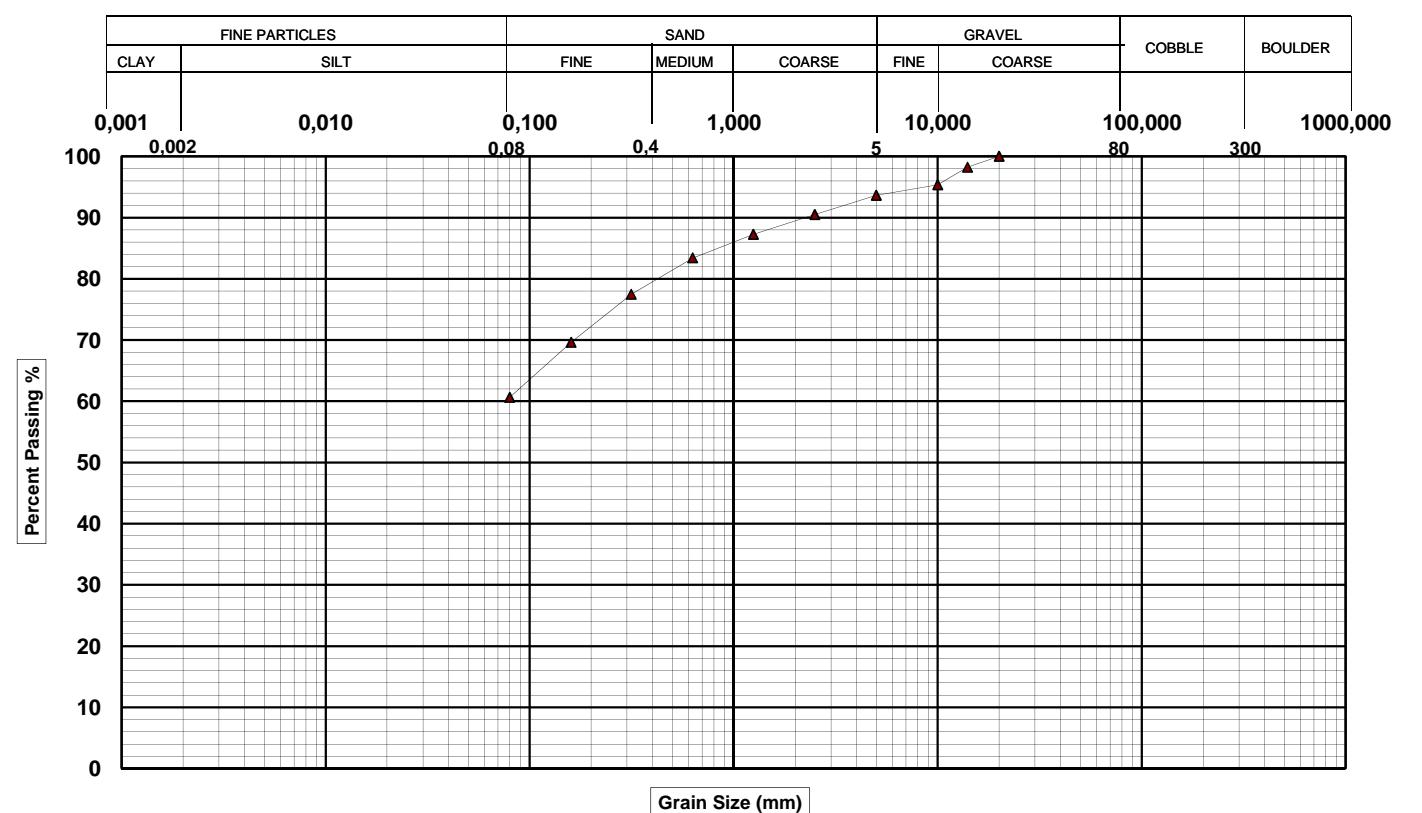
SAMPLE IDENTIFICATION										
Sample	10BH-22 (SS-02)									
Depth	0,61 - 1,22 m									
Soil Description										
Sandy silt, traces of gravel										

Prepared by Benoit St-Pierre, tech.

Approved by Ibrahim Ja'far, ing.

Date 2010-05-04

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36868



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	60,6	33,0	6,4	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	N/A	N/A	N/A	15

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	90		
56,00	100	1,250	87		
40,00	100	0,630	83		
31,50	100	0,315	77		
20,00	100	0,160	70		
14,00	98	0,080	60,6		
10,00	95				
5,00	94				

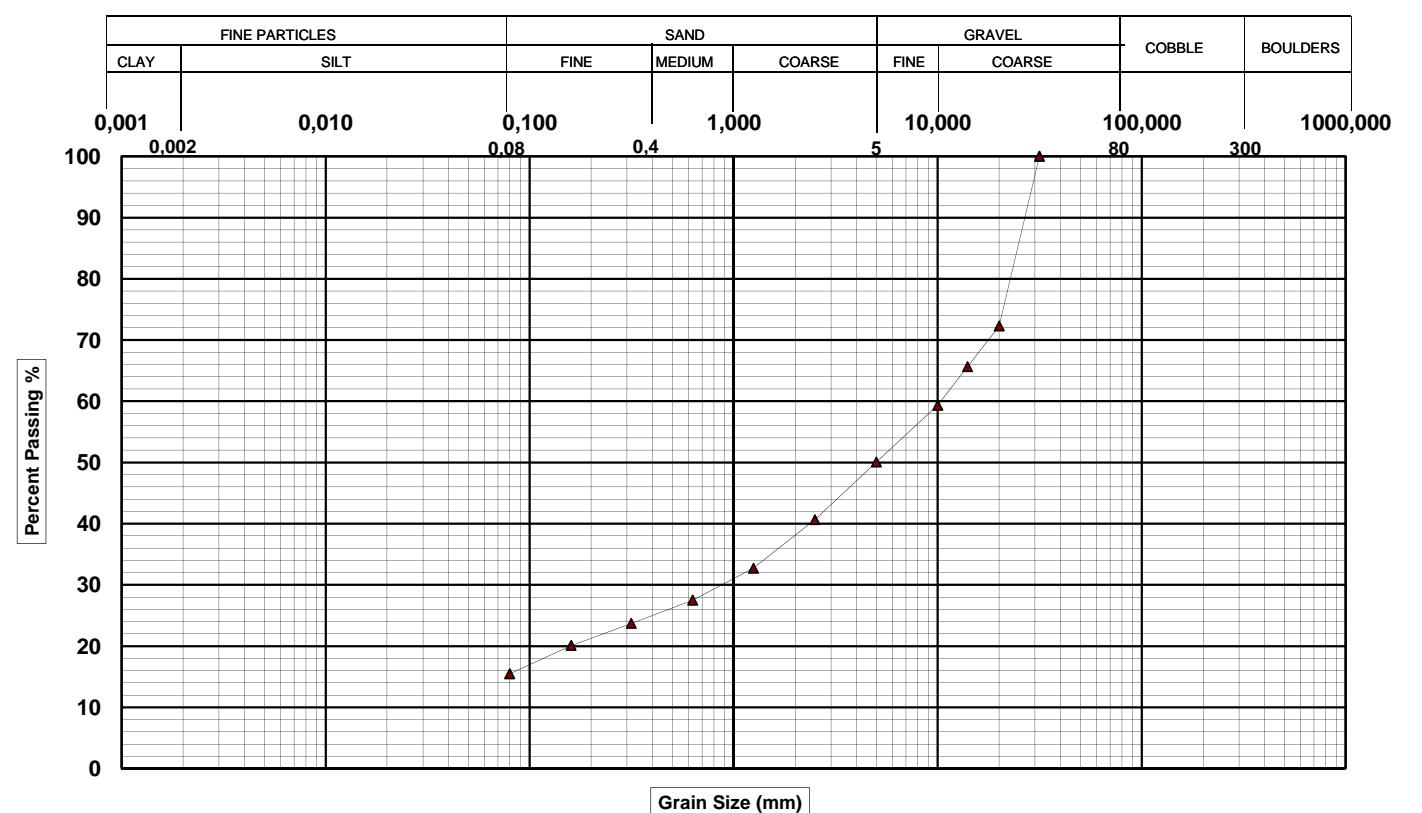
SAMPLE IDENTIFICATION										
Sample	10BH-22 (SS-04)									
Depth	2,44 - 3,05 m									
Soil Description										
Sandy silt, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-05-04

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36869



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	15,5	34,6	49,9	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	0,90	N/A	N/A	N/A	6

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	41		
56,00	100	1,250	33		
40,00	100	0,630	27		
31,50	100	0,315	24		
20,00	72	0,160	20		
14,00	66	0,080	15,5		
10,00	59				
5,00	50				

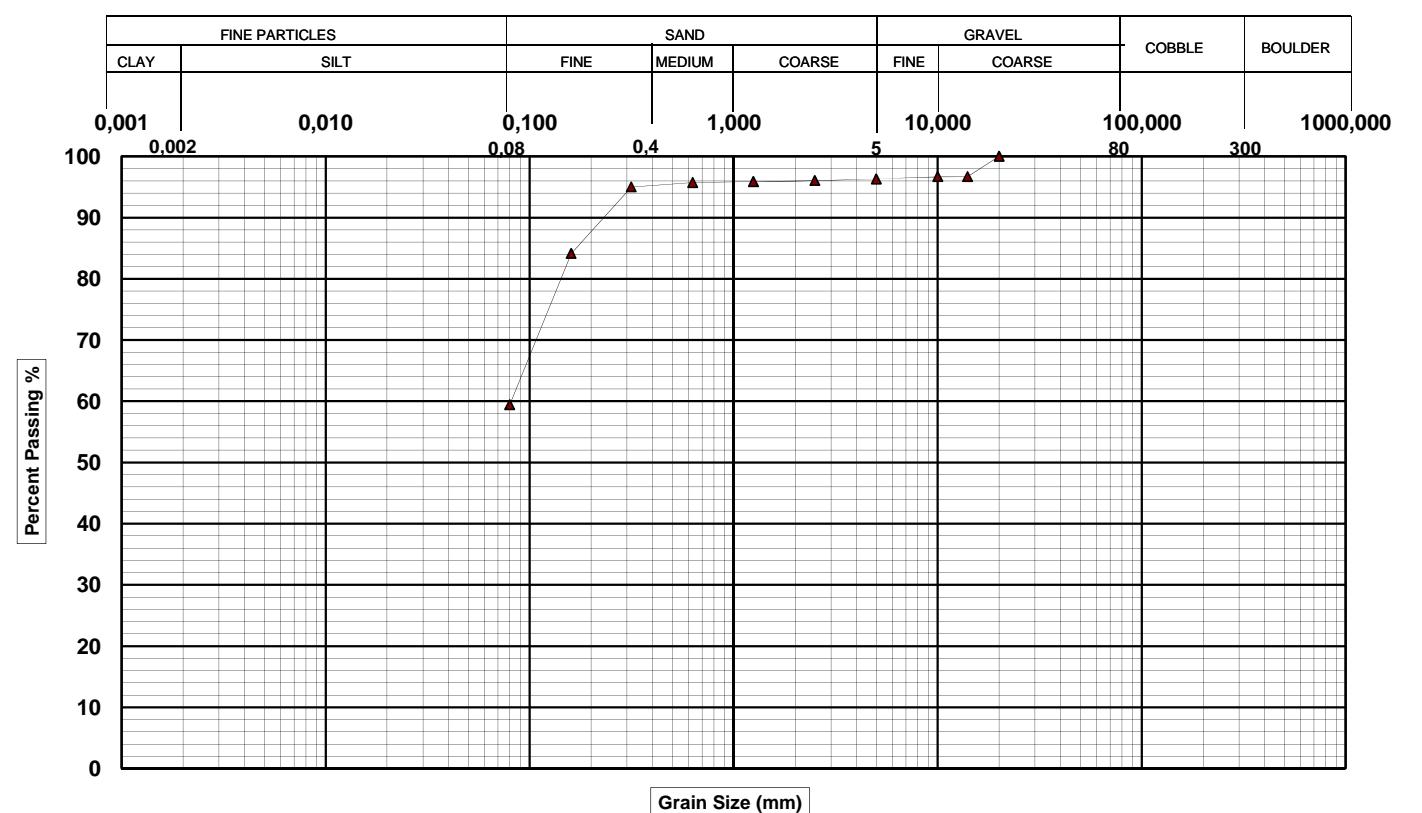
SAMPLE IDENTIFICATION										
Sample	10BH-22 (SS-08)									
Depth	6,10 - 6,71 m									
Soil Description										
Gravel and sand, some silt										

Prepared by Benoit St-pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-05-04

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36873



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	59,4	36,9	3,7	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,08	N/A	N/A	15

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	96		
56,00	100	1,250	96		
40,00	100	0,630	96		
31,50	100	0,315	95		
20,00	100	0,160	84		
14,00	97	0,080	59,4		
10,00	97				
5,00	96				

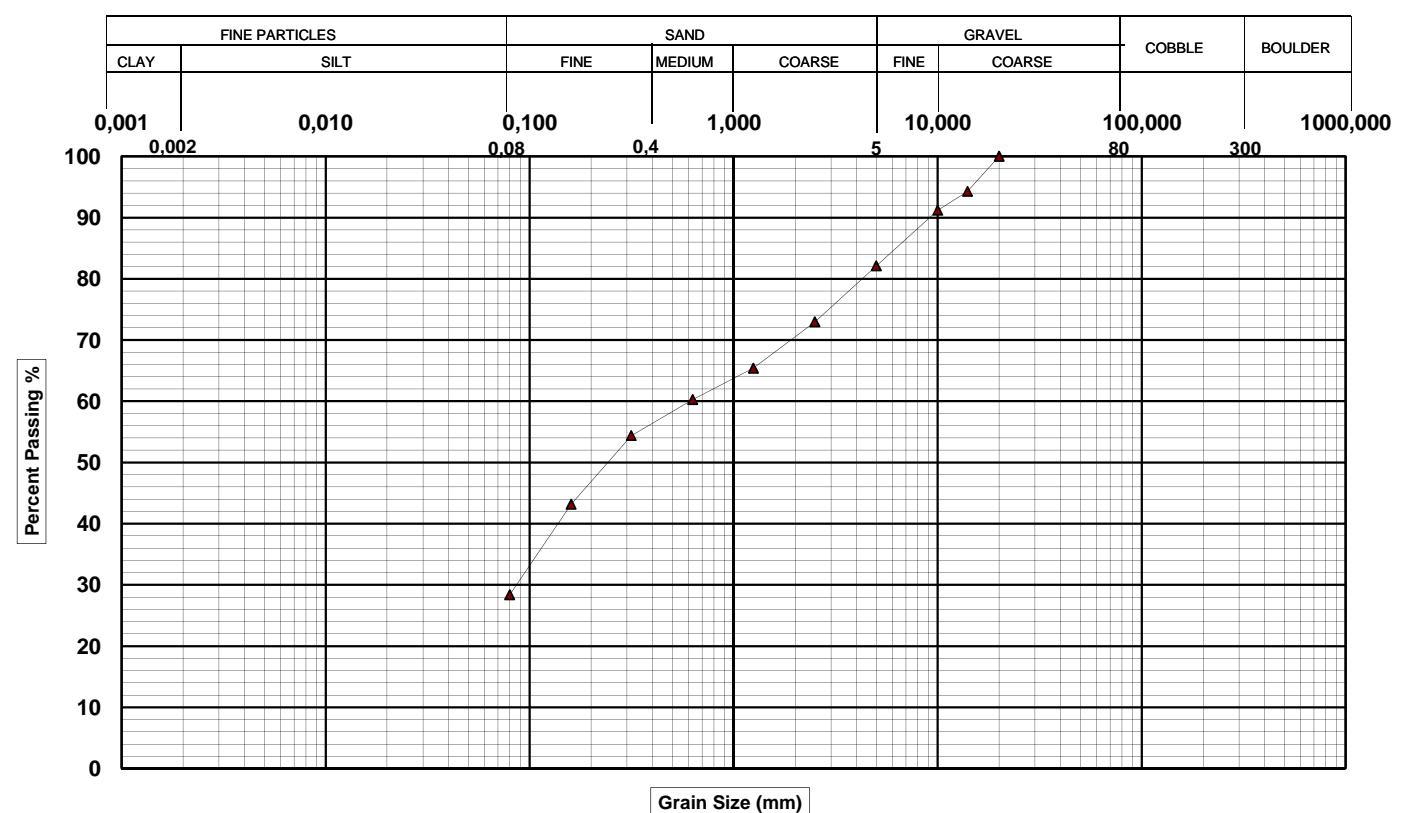
SAMPLE IDENTIFICATION	
Sample	10BH-28 (SS-09)
Depth	7,01 - 7,62 m
Soil Description	
Silt and sand, traces of gravel	

Prepared by Benoit St-Pierre, tech.

Approved by Ibrahim Ja'far, ing.

Date 2010-05-04

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36880



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	28,4	53,7	17,9	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	0,09	0,60	N/A	N/A	9

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	73		
56,00	100	1,250	65		
40,00	100	0,630	60		
31,50	100	0,315	54		
20,00	100	0,160	43		
14,00	94	0,080	28,4		
10,00	91				
5,00	82				

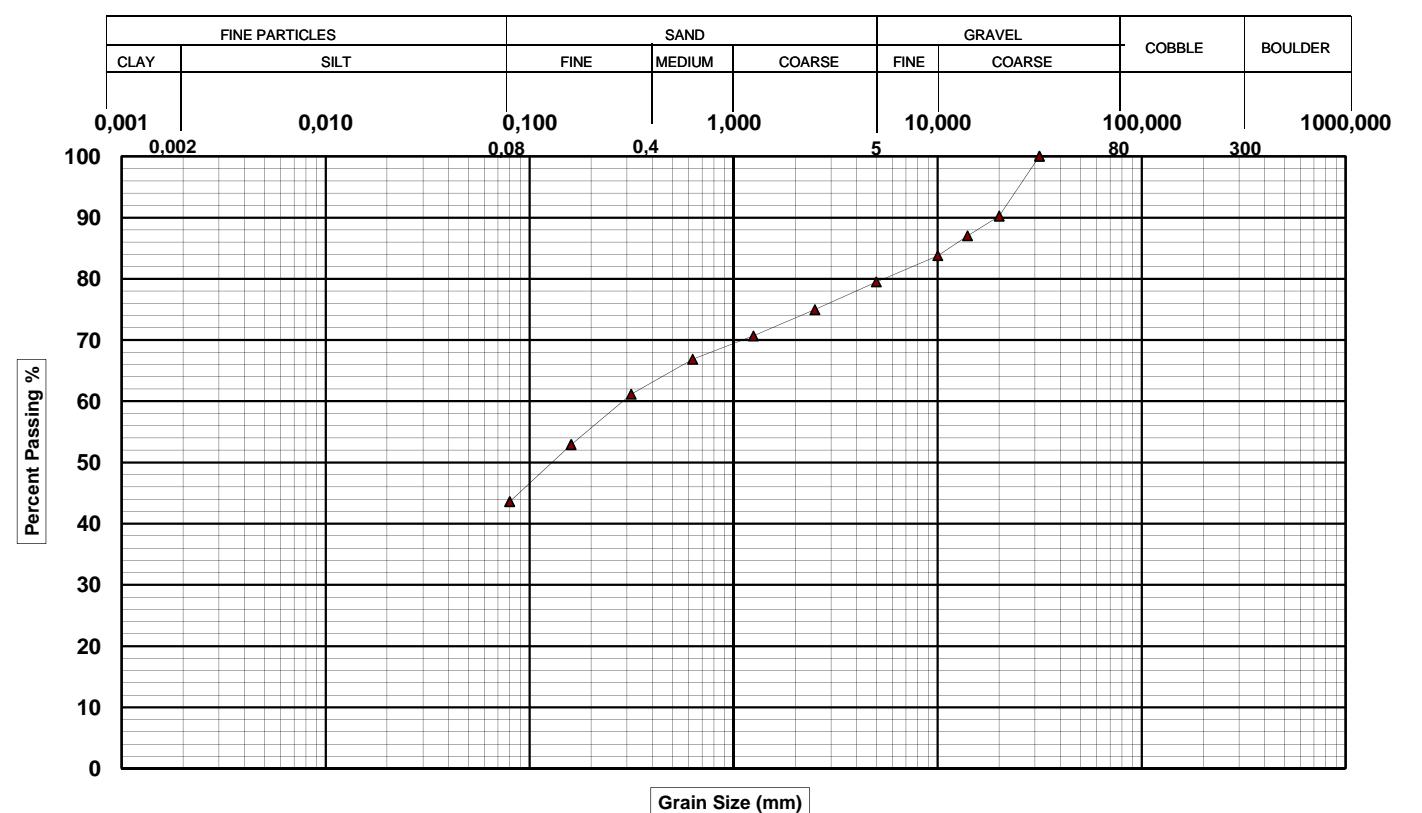
SAMPLE IDENTIFICATION										
Sample	10BH-31 (SS-08)									
Depth	7,09 - 7,70 m									
Soil Description										
Silty sand, trace of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-05-04

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36884



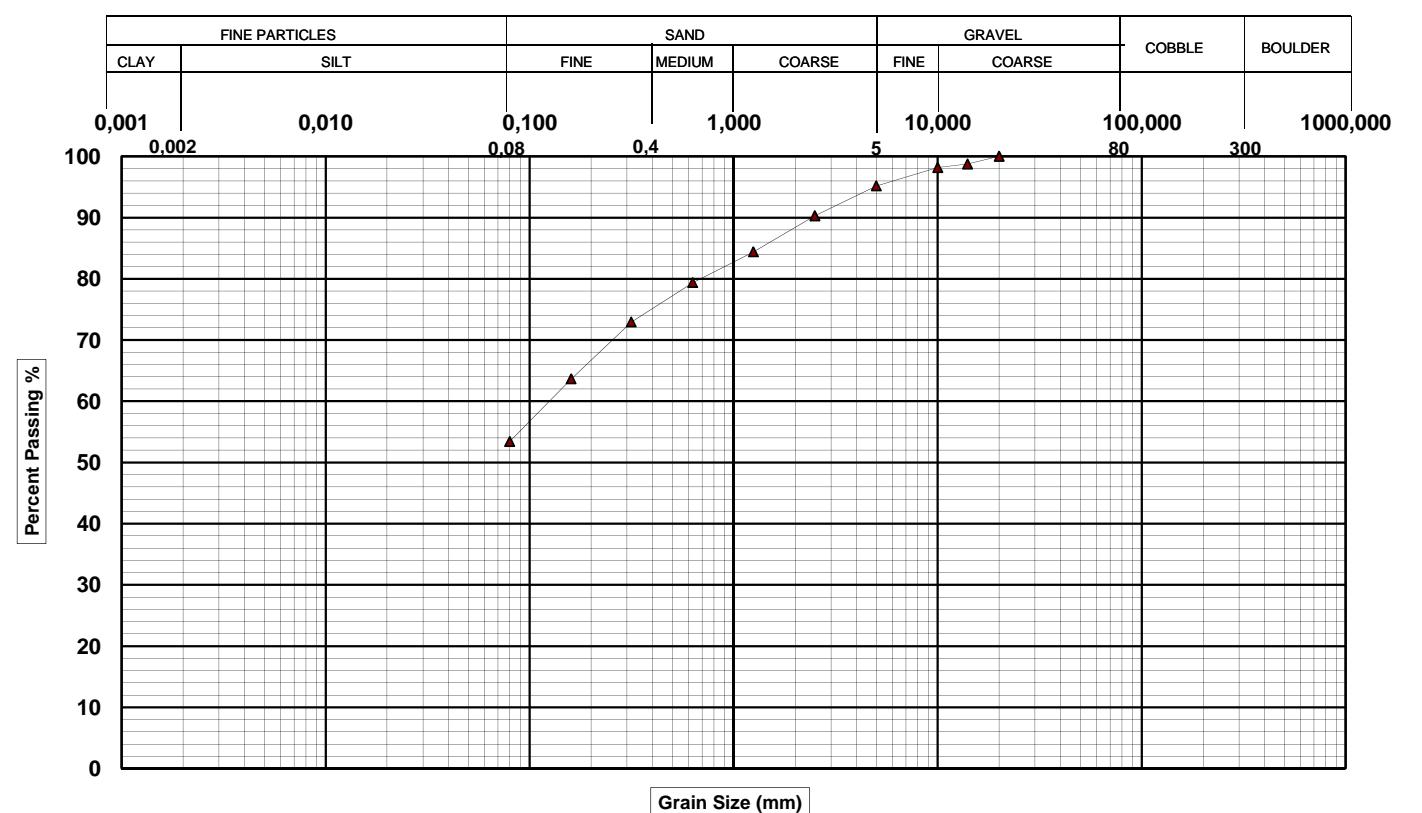
GRAIN-SIZE DISTRIBUTION										
Fine Particles		Coarse Particles								
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)					
-	43,6	35,9	20,5	0,0	0,0					
PERCENT PASSING										
(mm)	(%)	(mm)	(%)	(mm)	(%)					
80,00	100	2,500	75							
56,00	100	1,250	71							
40,00	100	0,630	67							
31,50	100	0,315	61							
20,00	90	0,160	53							
14,00	87	0,080	43,6							
10,00	84									
5,00	79									
SAMPLE IDENTIFICATION										
Sample	10BH-31A (SS-08)									
Depth	6,10 - 6,71 m									
Soil Description										
Gravelly silt and sand										

Prepared by Benoit St-Pierre, tech.

Approved by Ibrahim Ja'far, ing.

Date 2010-05-04

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36929



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	53,4	41,7	4,8	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,13	N/A	N/A	13

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	90		
56,00	100	1,250	84		
40,00	100	0,630	79		
31,50	100	0,315	73		
20,00	100	0,160	64		
14,00	99	0,080	53,4		
10,00	98				
5,00	95				

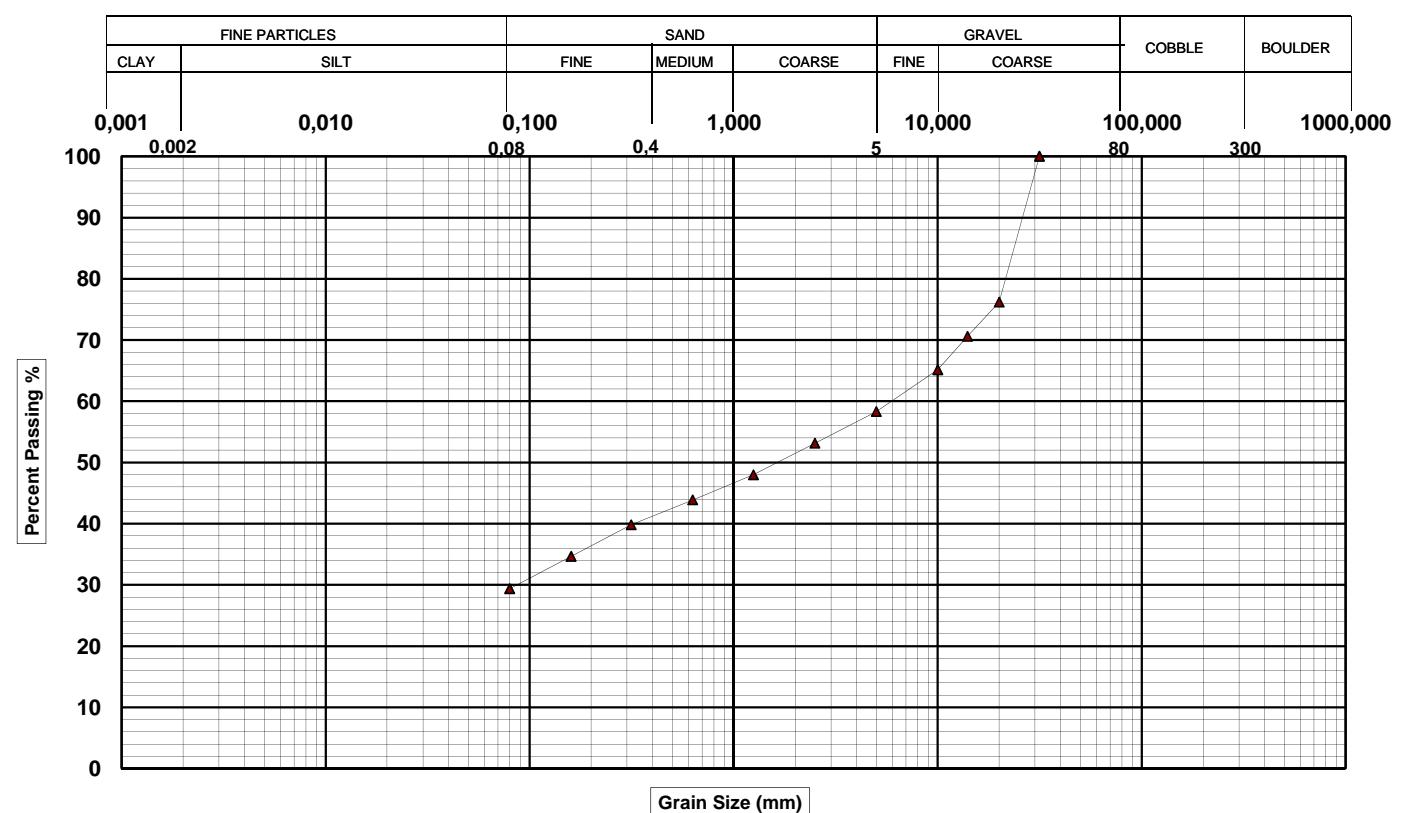
SAMPLE IDENTIFICATION										
Sample	10BH-37 (SS-03)									
Depth	1,52 - 2,13 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-Pierre, tech.

Approved by Ibrahim Ja'far, ing.

Date 2010-05-04

CLIENT	TransAlta	N/D	G1-10-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36930



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	29,4	28,9	41,7	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	0,09	6,00	N/A	N/A	7

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	53		
56,00	100	1,250	48		
40,00	100	0,630	44		
31,50	100	0,315	40		
20,00	76	0,160	35		
14,00	71	0,080	29,4		
10,00	65				
5,00	58				

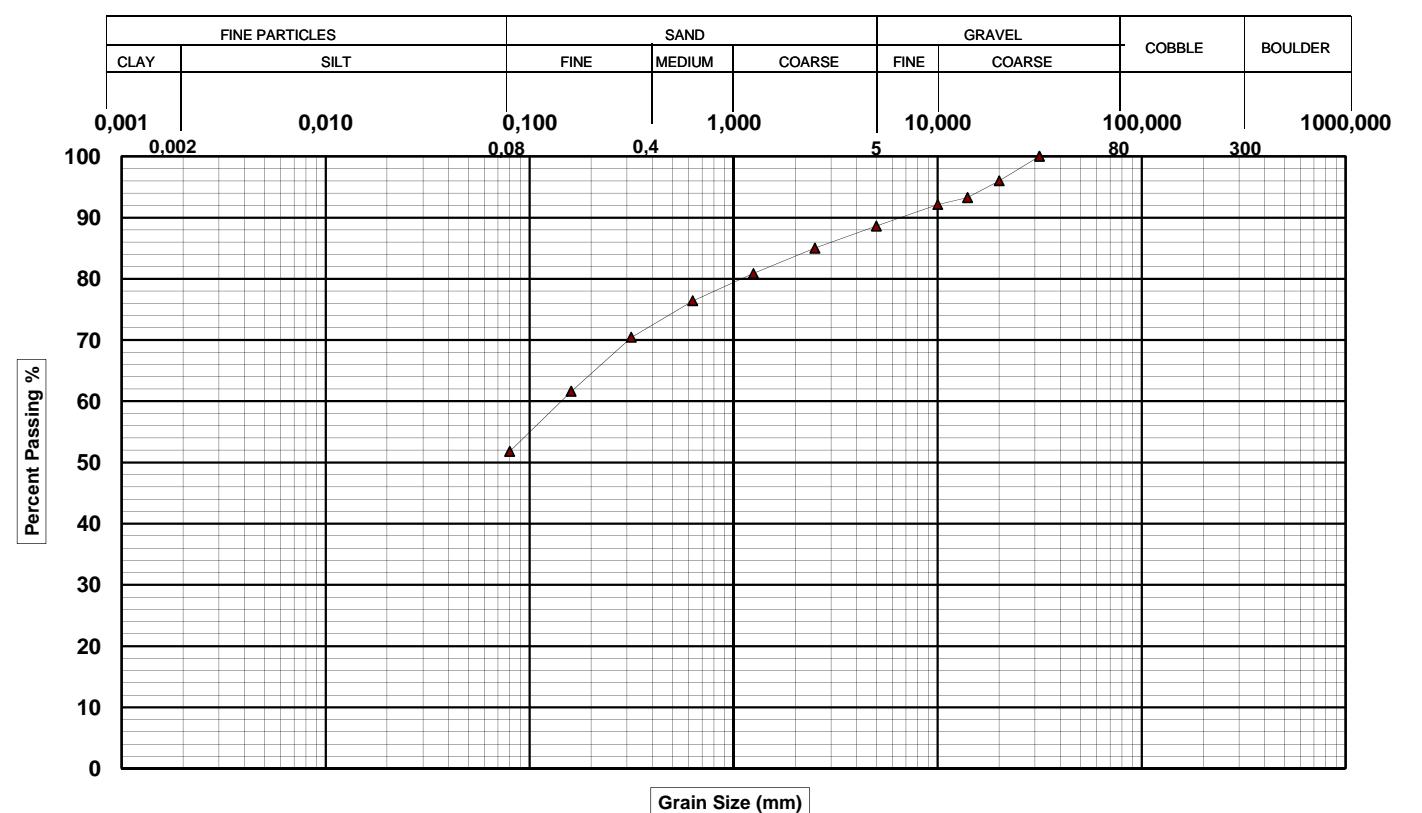
SAMPLE IDENTIFICATION										
Sample	10BH-37 (SS-07)									
Depth	5,18 - 5,79 m									
Soil Description										
Sandy silty gravel										

Prepared by Benoit St-Pierre, tech.

Approved by Ibrahim Ja'far, ing.

Date 2010-05-04

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36671



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
0,0	51,8	36,8	11,4	0,0	0,0
D₁₀ (mm)	D₃₀ (mm)	D₆₀ (mm)	C_u	C_c	W_n (%)
N/A	N/A	0,15	N/A	N/A	10

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	85		
56,00	100	1,250	81		
40,00	100	0,630	76		
31,50	100	0,315	70		
20,00	96	0,160	62		
14,00	93	0,080	51,8		
10,00	92				
5,00	89				

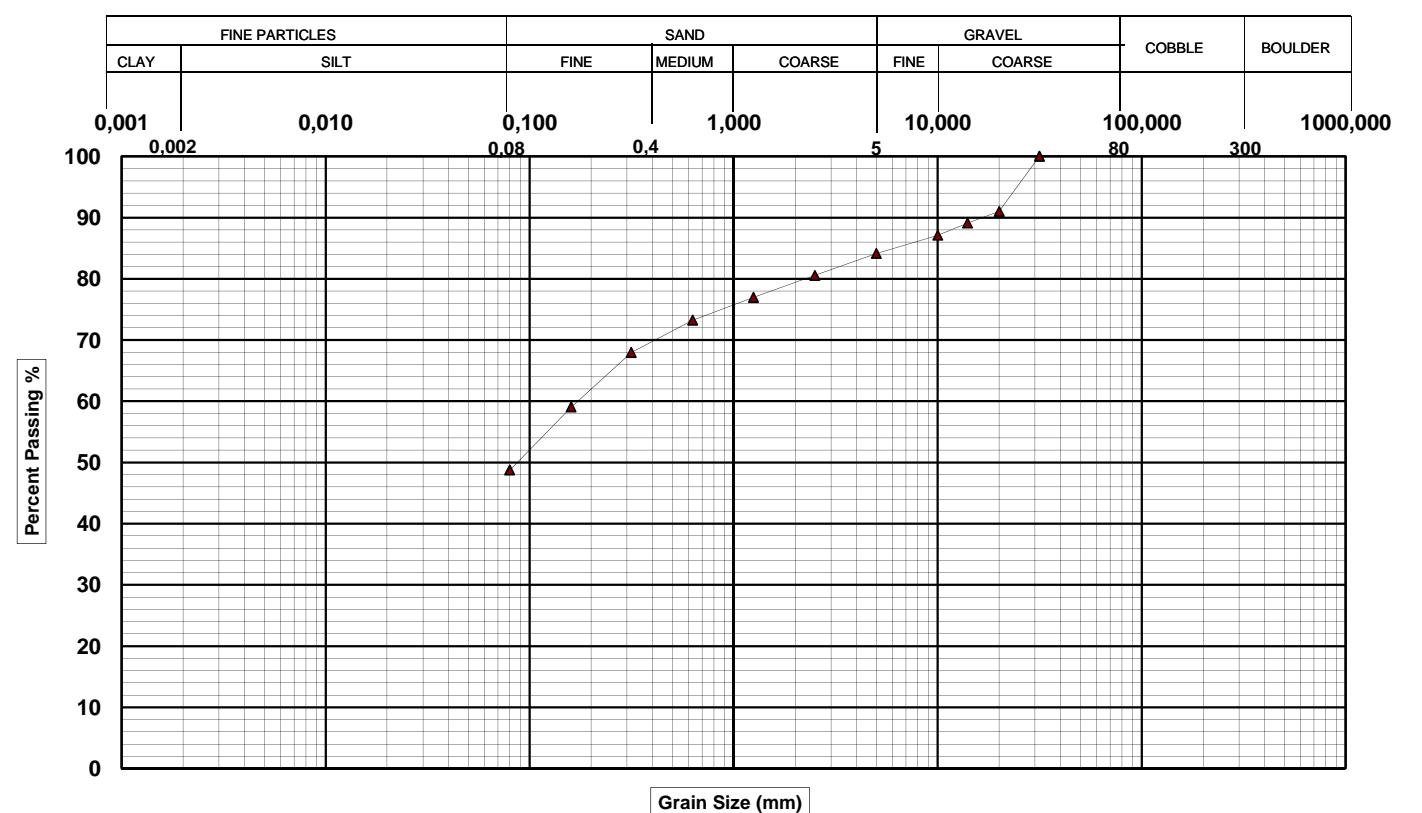
SAMPLE IDENTIFICATION										
Sample	10BH-35 (SS-02)									
Depth	0,61 - 1,22 m									
Soil Description										
Silt and sand, some gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-21

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36772



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	48,8	35,4	15,9	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,19	N/A	N/A	8

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	81		
56,00	100	1,250	77		
40,00	100	0,630	73		
31,50	100	0,315	68		
20,00	91	0,160	59		
14,00	89	0,080	48,8		
10,00	87				
5,00	84				

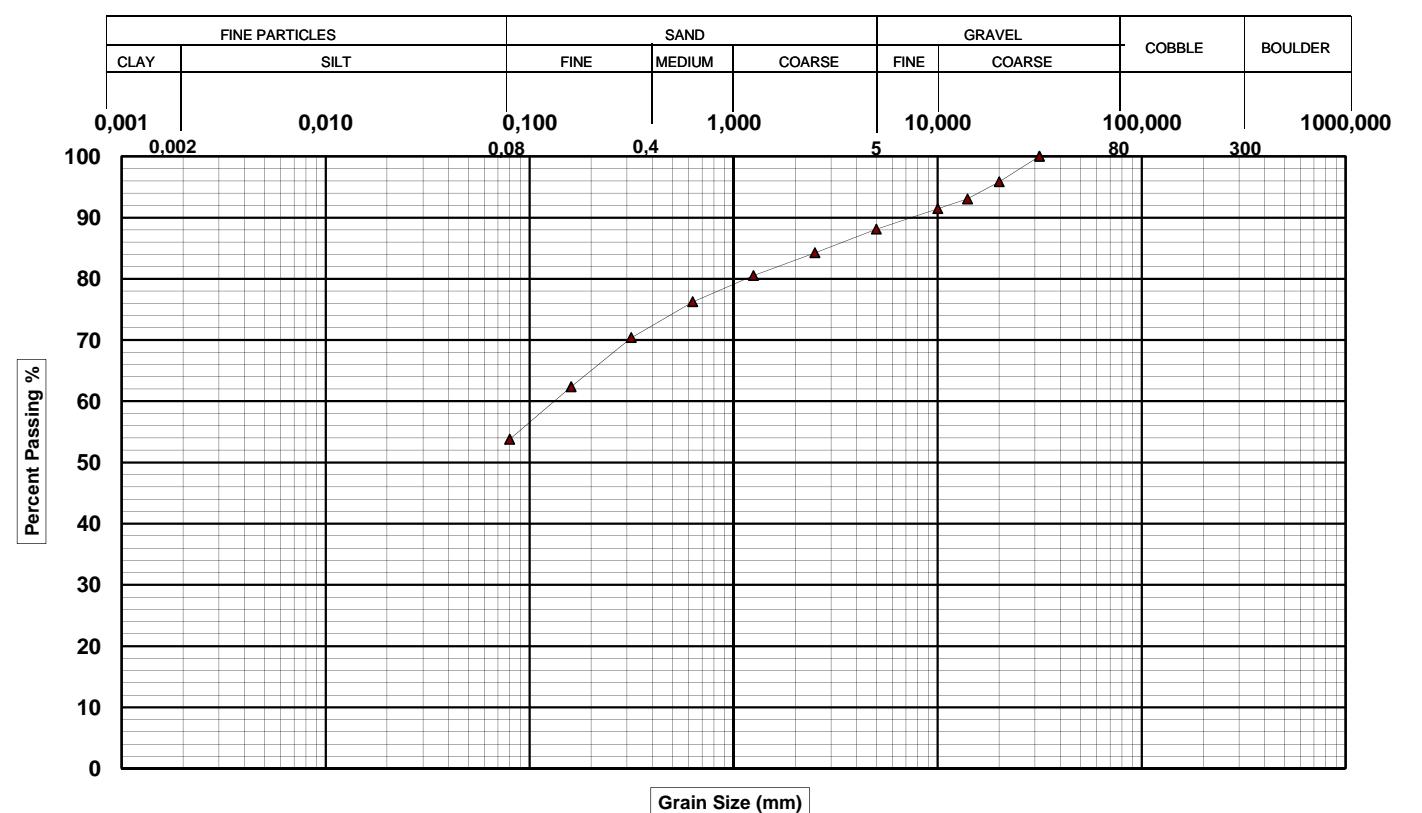
SAMPLE IDENTIFICATION										
Sample	10BH-35 (SS-04)									
Depth	2,44 - 3,05 m									
Soil Description										
Sand and silt, a little gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-21

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36674



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	53,8	34,3	11,9	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,14	N/A	N/A	12

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	84		
56,00	100	1,250	81		
40,00	100	0,630	76		
31,50	100	0,315	70		
20,00	96	0,160	62		
14,00	93	0,080	53,8		
10,00	91				
5,00	88				

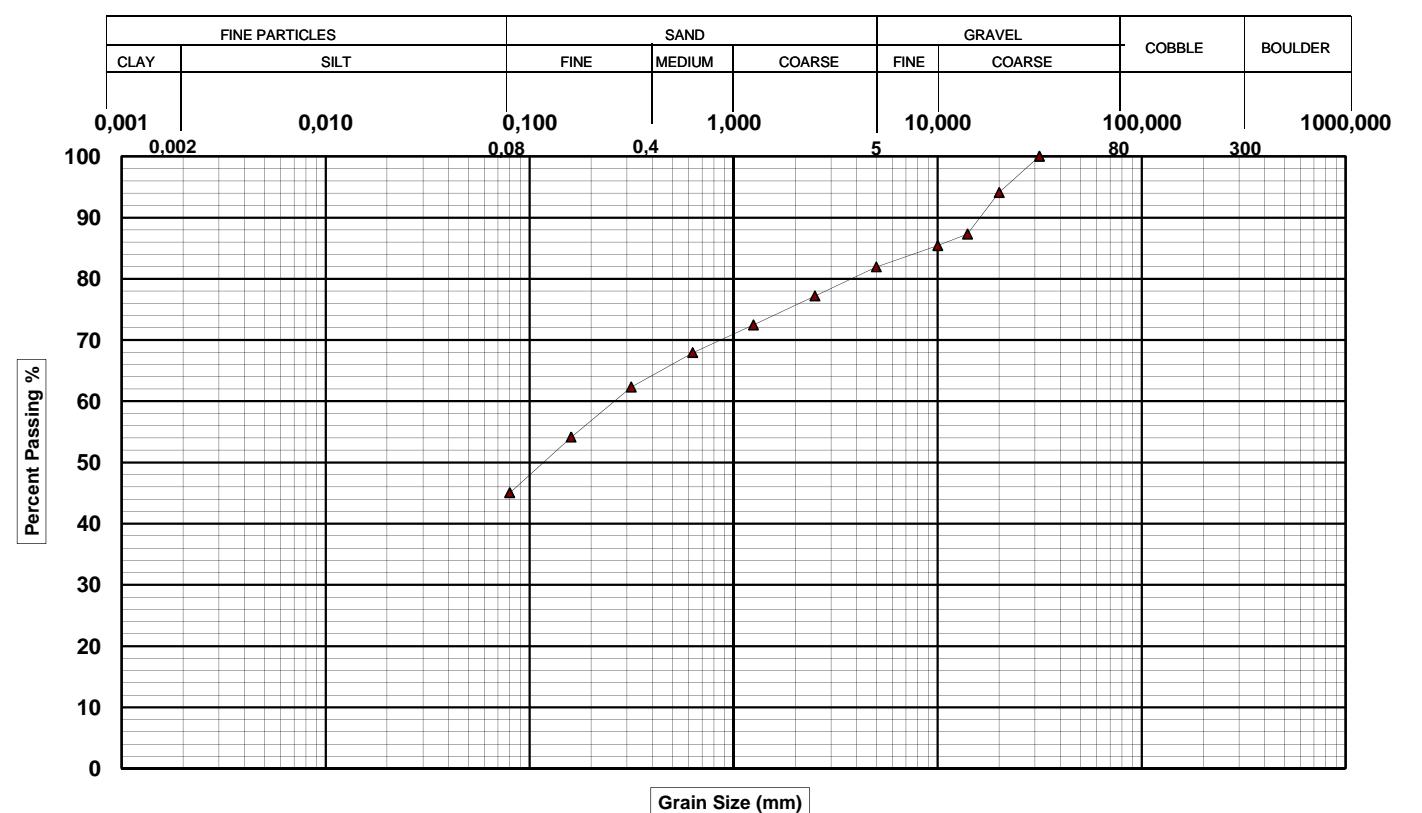
SAMPLE IDENTIFICATION										
Sample	10BH-34 (SS-02)									
Depth	0,61 - 1,22 m									
Soil Description										
Silt and sand, some gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-21

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin	NO. LAB.	36675



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	45,0	36,9	18,1	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,28	N/A	N/A	9

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	77		
56,00	100	1,250	72		
40,00	100	0,630	68		
31,50	100	0,315	62		
20,00	94	0,160	54		
14,00	87	0,080	45,0		
10,00	85				
5,00	82				

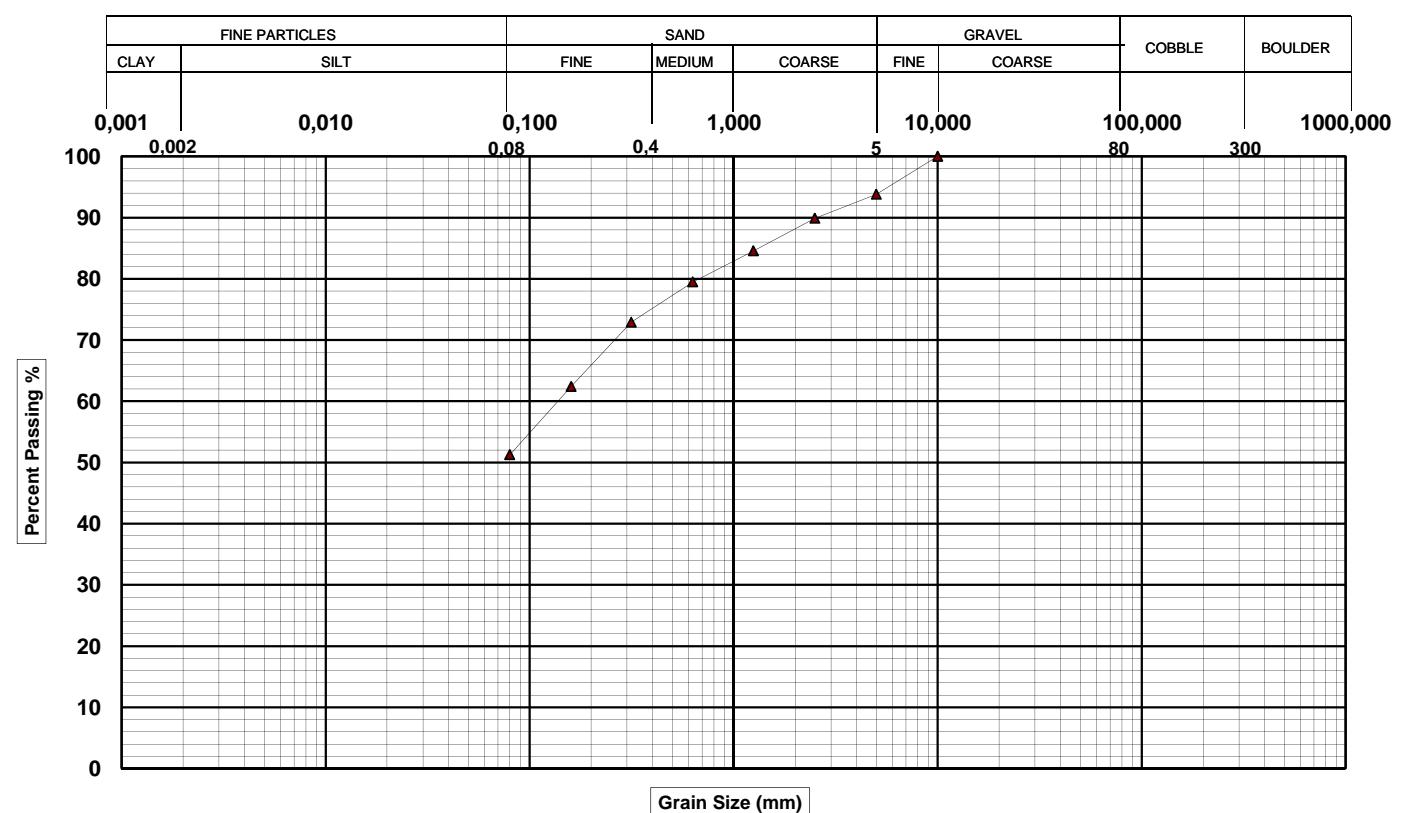
SAMPLE IDENTIFICATION										
Sample	10BH-34 (SS-04)									
Depth	2,44 - 3,05 m									
Soil Description										
Silt and sand, some gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-21

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36604



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	51,3	42,5	6,2	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,14	N/A	N/A	14

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	90		
56,00	100	1,250	85		
40,00	100	0,630	79		
31,50	100	0,315	73		
20,00	100	0,160	62		
14,00	100	0,080	51,3		
10,00	100				
5,00	94				

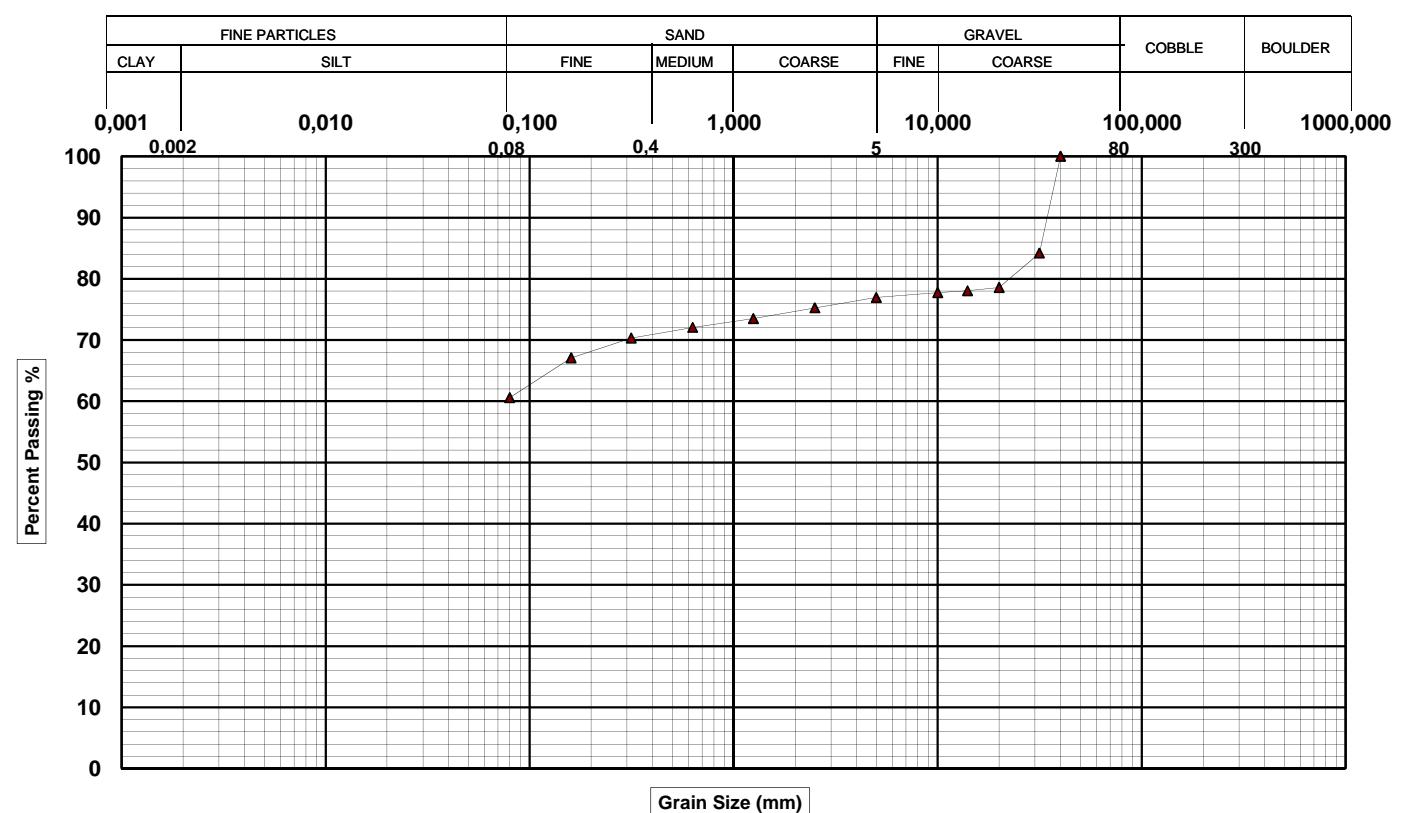
SAMPLE IDENTIFICATION										
Sample	10BH-21 (SS-05)									
Depth	3,35 - 3,96 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-22

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36607



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	60,6	16,3	23,0	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	N/A	N/A	N/A	10

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	75		
56,00	100	1,250	73		
40,00	100	0,630	72		
31,50	84	0,315	70		
20,00	79	0,160	67		
14,00	78	0,080	60,6		
10,00	78				
5,00	77				

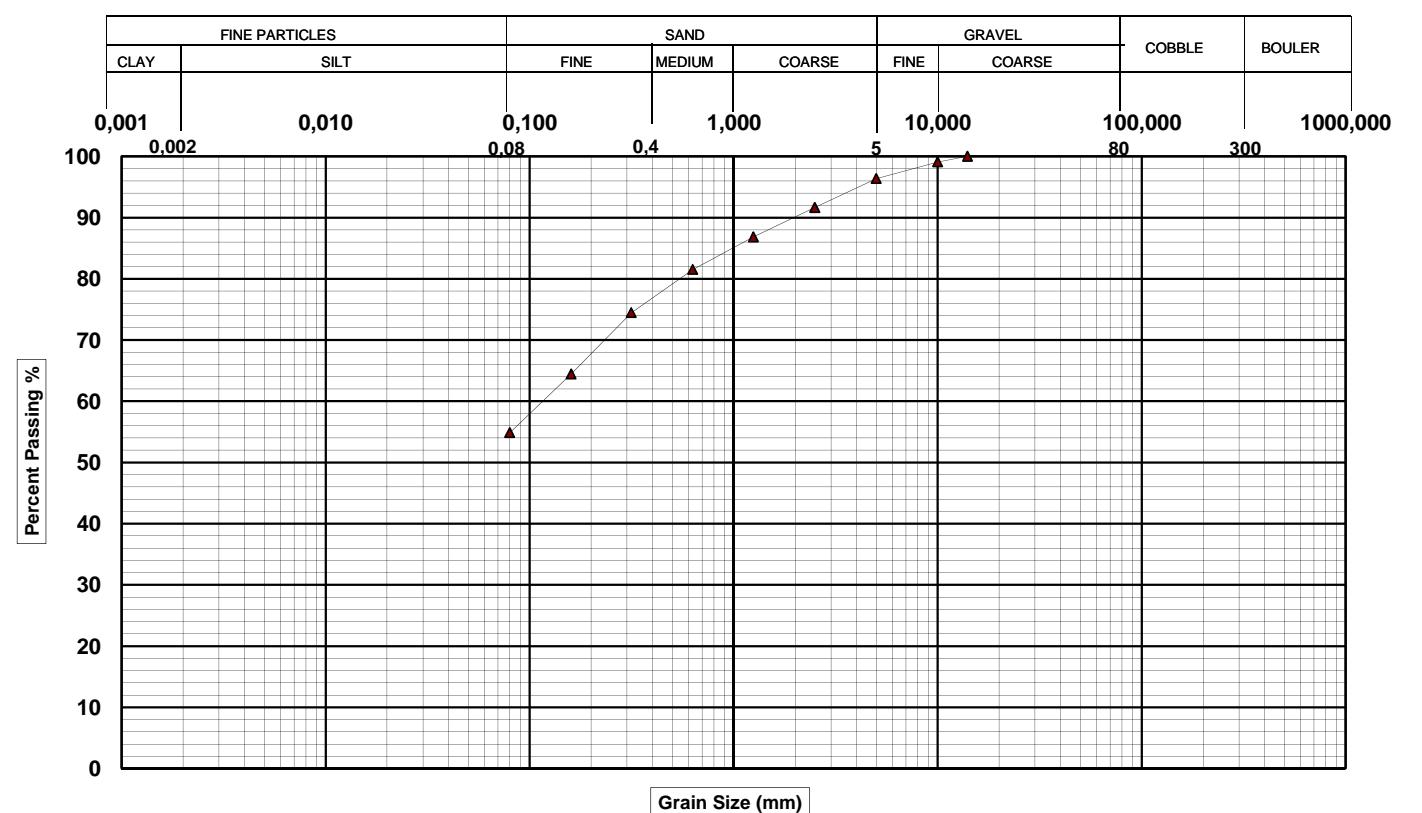
SAMPLE IDENTIFICATION										
Sample	10BH-21 (SS-11)									
Depth	9,14 - 9,75 m									
Soil Description										
Gravelly silt, some sand										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-22

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36601



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	54,9	41,5	3,6	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,12	N/A	N/A	12

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	92		
56,00	100	1,250	87		
40,00	100	0,630	82		
31,50	100	0,315	74		
20,00	100	0,160	64		
14,00	100	0,080	54,9		
10,00	99				
5,00	96				

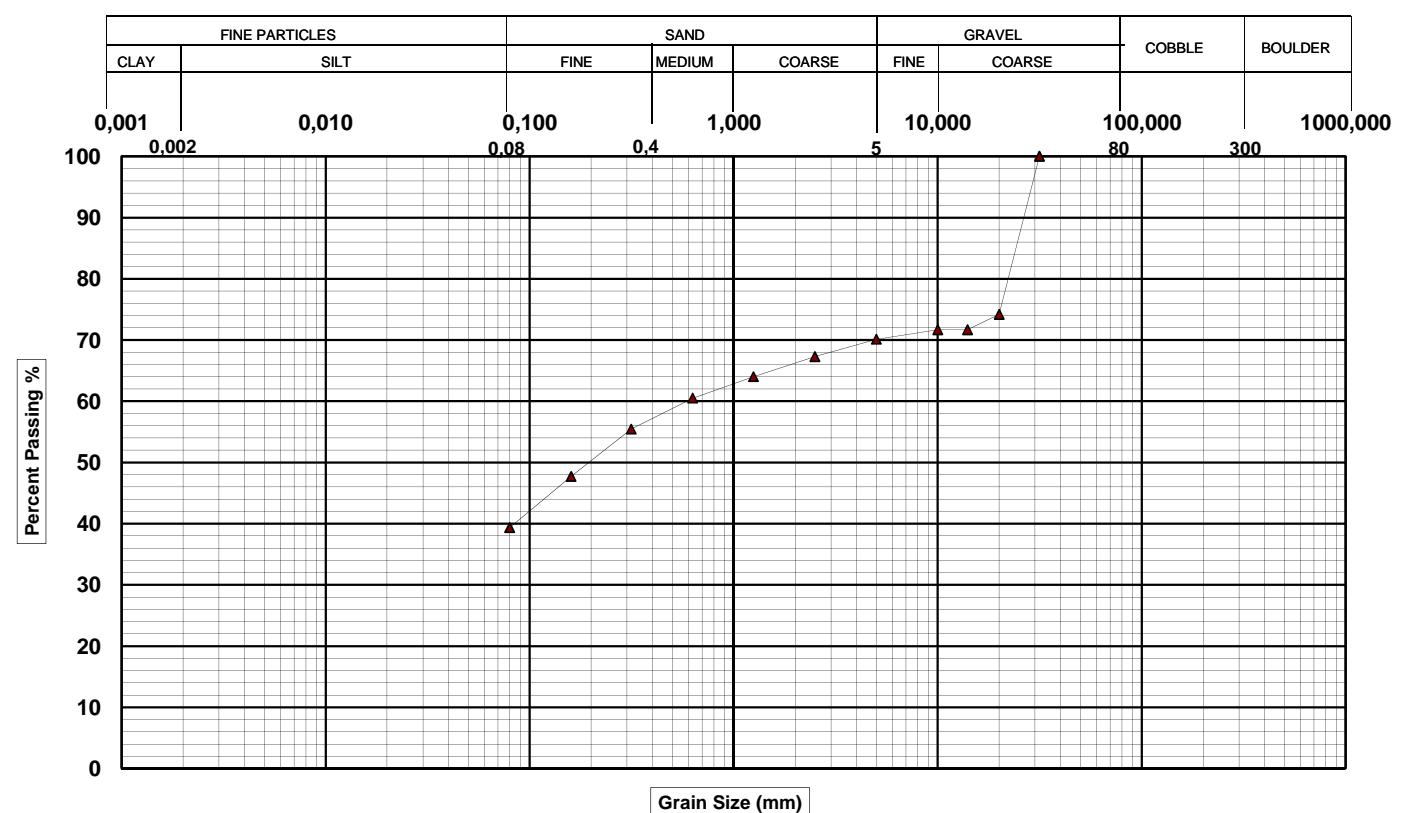
SAMPLE IDENTIFICATION										
Sample	10BH-20 (SS-04)									
Depth	2,44 - 3,05 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-22

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36602



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	39,4	30,8	29,9	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,60	N/A	N/A	7

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	67		
56,00	100	1,250	64		
40,00	100	0,630	61		
31,50	100	0,315	55		
20,00	74	0,160	48		
14,00	72	0,080	39,4		
10,00	72				
5,00	70				

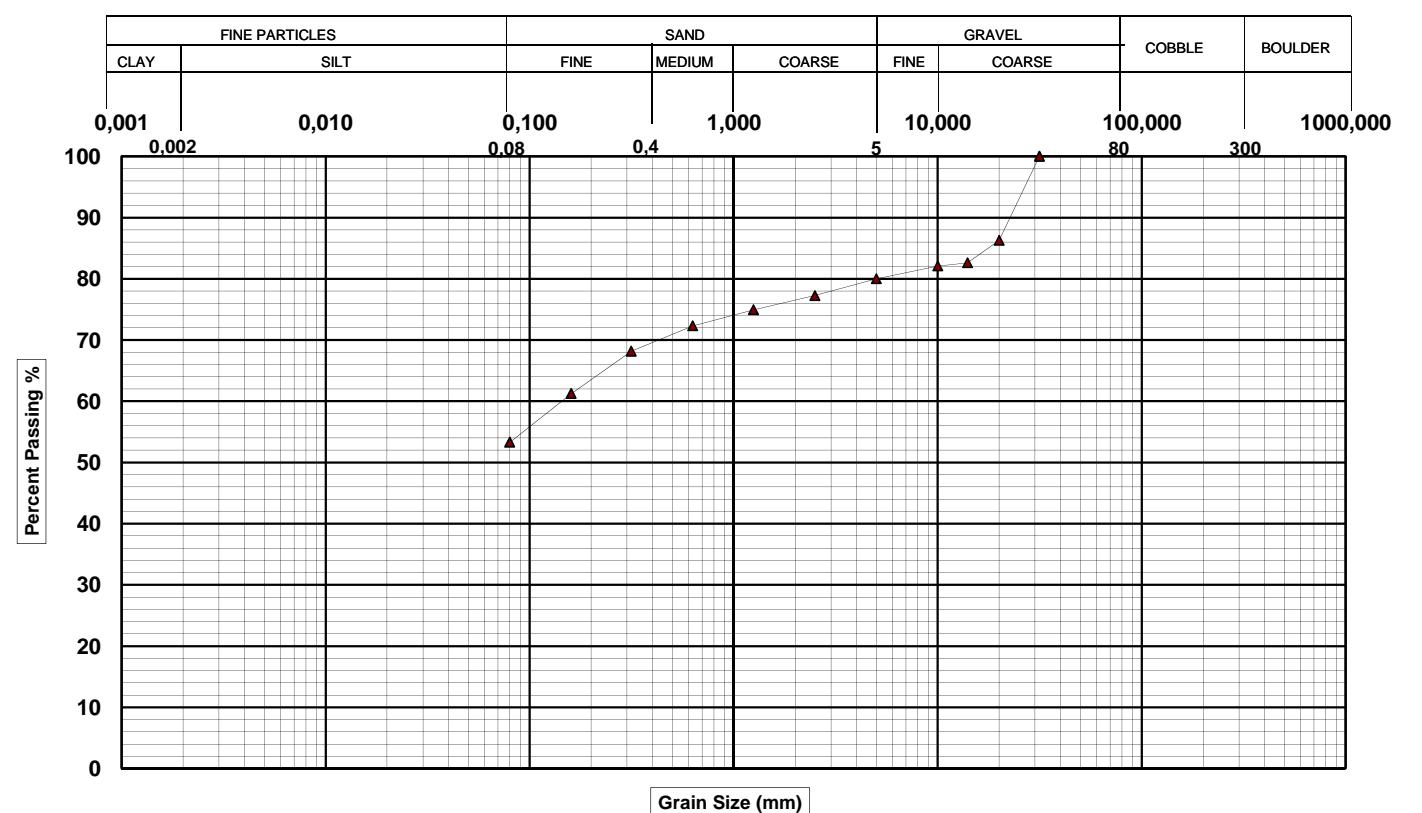
SAMPLE IDENTIFICATION										
Sample	10BH-20 (SS-07)									
Depth	5,18 - 5,79 m									
Soil Description										
Gravelly sandy silt										

Prepared by Benoit St-Pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-22

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36603



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	53,3	26,7	20,0	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,15	N/A	N/A	15

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	77		
56,00	100	1,250	75		
40,00	100	0,630	72		
31,50	100	0,315	68		
20,00	86	0,160	61		
14,00	83	0,080	53,3		
10,00	82				
5,00	80				

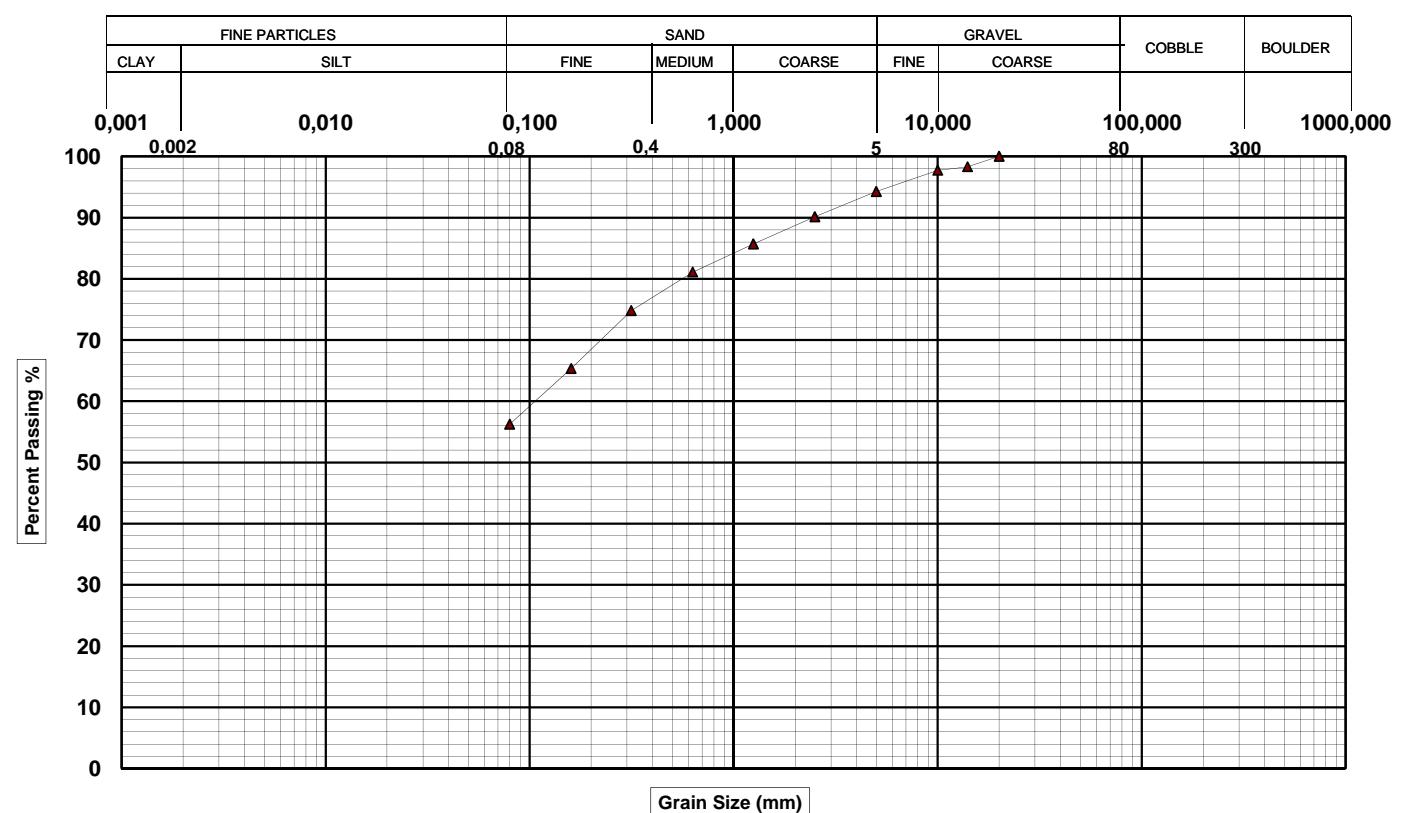
SAMPLE IDENTIFICATION										
Sample	10BH-20 (SS-10)									
Depth	7,92 - 8,53 m									
Soil Description										
Sandy silt, some gravel										

Prepared by Benoit St-pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-22

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36605



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	56,2	38,0	5,8	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,10	N/A	N/A	11

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	90		
56,00	100	1,250	86		
40,00	100	0,630	81		
31,50	100	0,315	75		
20,00	100	0,160	65		
14,00	98	0,080	56,2		
10,00	98				
5,00	94				

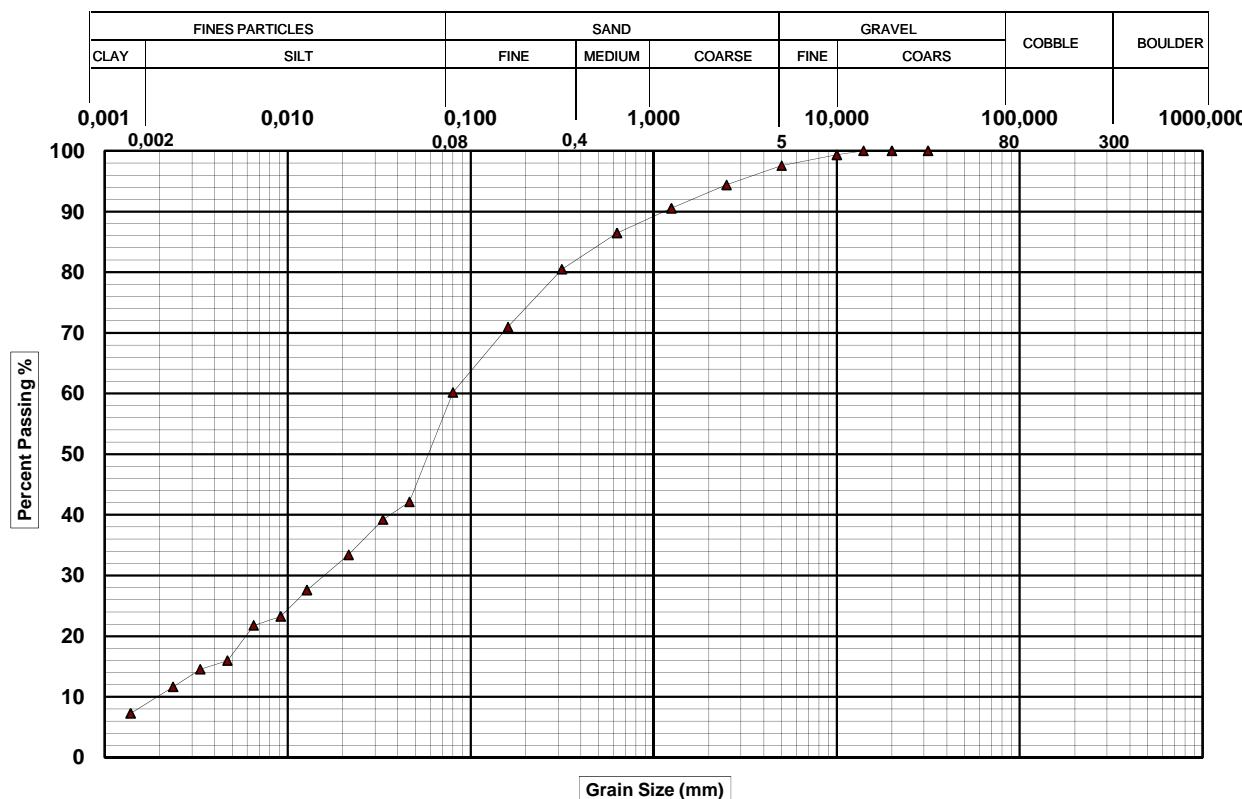
SAMPLE IDENTIFICATION										
Sample	10BH-21 (SS-07)									
Depth	5,18 - 5,79 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-22

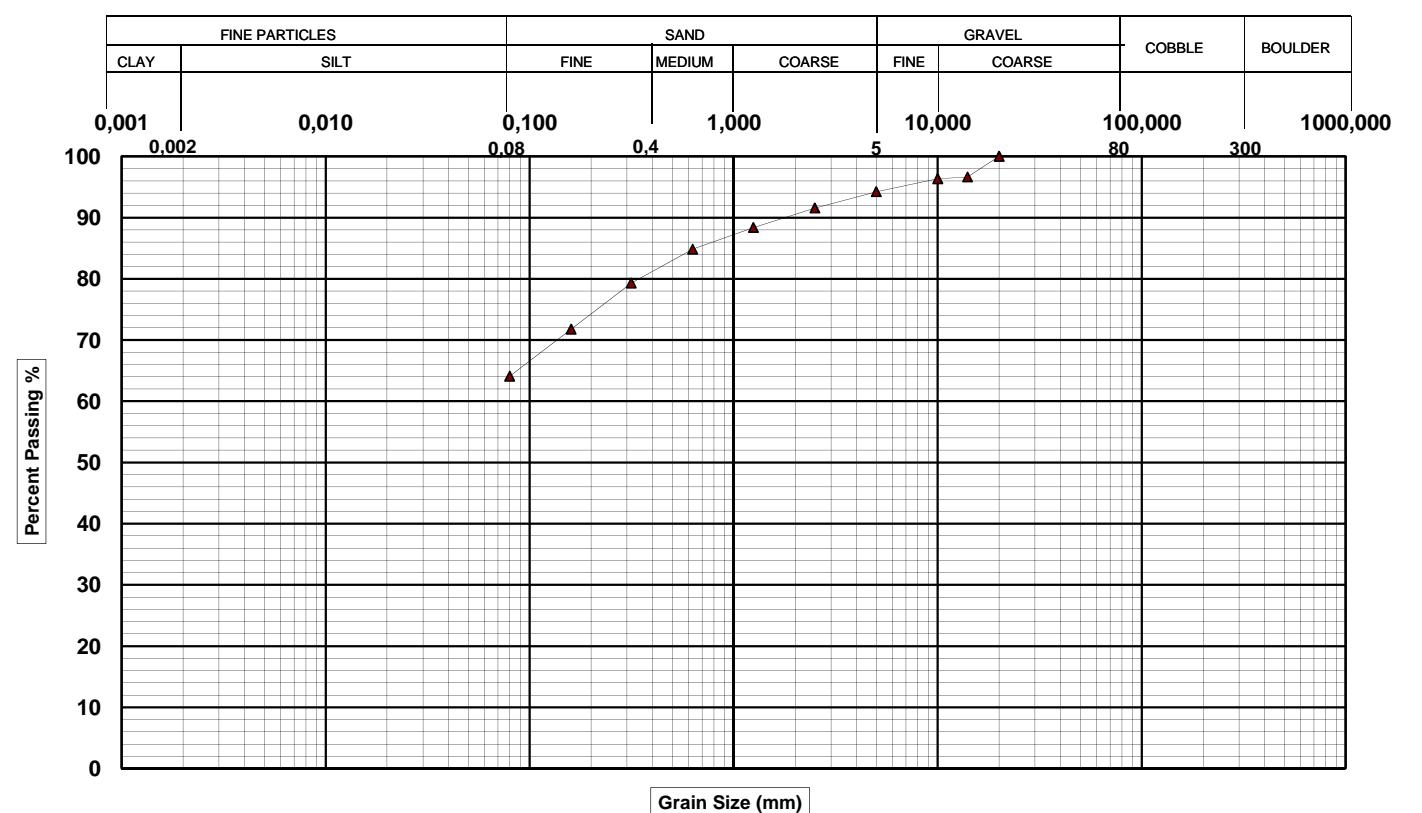
CLIENT	TranAlta	N/D G1-10-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)	
LOCATION	St-Valentin	NO. LAB. G1-09-15



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
10,0	50,2	37,4	2,4	0,0	0,0
D₁₀ (mm)	D₃₀ (mm)	D₆₀ (mm)	C_u	C_c	W_n (%)
0,0020	0,018	0,08	40,00	2,03	13

PERCENT PASSING						SAMPLE IDENTIFICATION	
(mm)	(%)	(mm)	(%)	(mm)	(%)	Sample	10BH-21 (SS-10)
80,00	100	2,500	94	0,0215	33	Depth	7,92 - 8,53 m
56,00	100	1,250	91	0,0127	28	Soil Description	
40,00	100	0,630	86	0,0092	23	Silt and sand, traces of caly and gravel	
31,50	100	0,315	80	0,0065	22		
20,00	100	0,160	71	0,0047	16		
14,00	100	0,080	60	0,0033	15		
10,00	99	0,046	42	0,0024	11,6		
5,00	98	0,033	39	0,0014	7,3		

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36713



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	64,1	30,1	5,8	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	N/A	N/A	N/A	13

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	92		
56,00	100	1,250	88		
40,00	100	0,630	85		
31,50	100	0,315	79		
20,00	100	0,160	72		
14,00	97	0,080	64,1		
10,00	96				
5,00	94				

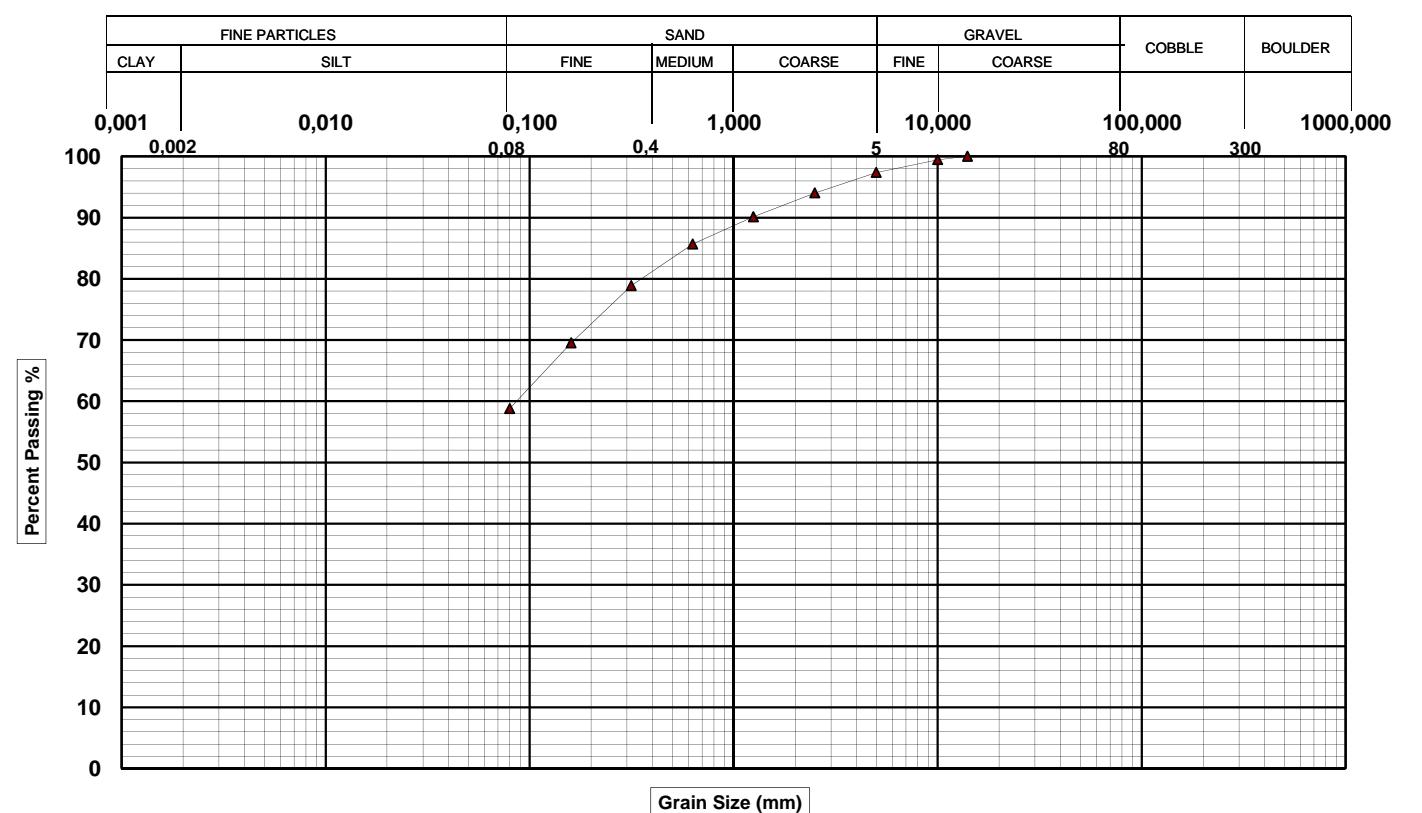
SAMPLE IDENTIFICATION										
Sample	10BH-23 (SS-02)									
Depth	0,61 - 1,22 m									
Soil Description										
Sandy silt, traces of gravel										

Prepared by Benoit St-pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-22

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36714



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	58,8	38,5	2,6	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	0,09	N/A	N/A	12

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	94		
56,00	100	1,250	90		
40,00	100	0,630	86		
31,50	100	0,315	79		
20,00	100	0,160	70		
14,00	100	0,080	58,8		
10,00	99				
5,00	97				

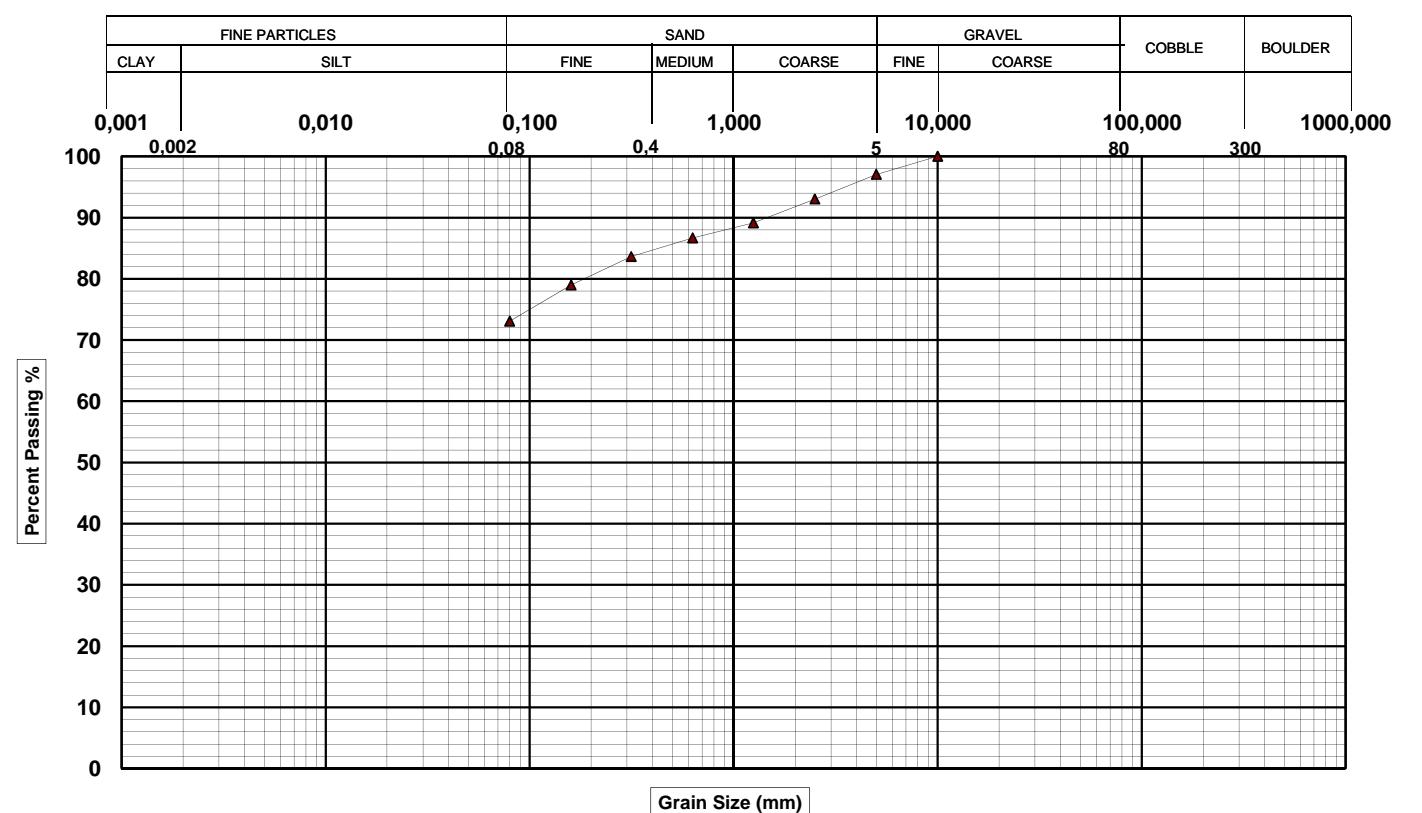
SAMPLE IDENTIFICATION										
Sample	10BH-23 (SS-05)									
Depth	3,35 - 3,96 m									
Soil Description										
Silt and sand, traces of gravel										

Prepared by Benoit St-pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-22

CLIENT	TransAlta	N/D	G1-09-1532
PROJECT	Geotechnical study - Wind energy converters (WEC)		
LOCATION	St-Valentin (Québec)	NO. LAB.	36715



GRAIN-SIZE DISTRIBUTION					
Fine Particles		Coarse Particles			
Clay (%)	Silt (%)	Sand (%)	Gravel (%)	Cobble (%)	Boulder (%)
-	73,1	24,0	2,9	0,0	0,0
D ₁₀ (mm)	D ₃₀ (mm)	D ₆₀ (mm)	C _u	C _c	W _n (%)
N/A	N/A	N/A	N/A	N/A	14

PERCENT PASSING					
(mm)	(%)	(mm)	(%)	(mm)	(%)
80,00	100	2,500	93		
56,00	100	1,250	89		
40,00	100	0,630	87		
31,50	100	0,315	84		
20,00	100	0,160	79		
14,00	100	0,080	73,1		
10,00	100				
5,00	97				

SAMPLE IDENTIFICATION										
Sample	10F-23 (CF-10)									
Depth	9,14 - 9,75 m									
Soil Description										
Sandy silt, traces of gravel										

Prepared by Benoit St-pierre

Approved by Ibrahim Ja'far, ing.

Date 2010-04-22

Appendix E

Geophysical investigation report

**SHEAR WAVE VELOCITY SOUNDING RESULTS – WIND ENERGY CONVERTERS
PROJECT, SAINT-VALENTIN, QUÉBEC**

Presented to :

GROUPE ABS INC.
17, rue de l'Industrie
St-Rémi-de-Napierville (Québec)
J0L 2L0

Presented by :

GEOPHYSICS GPR INTERNATIONAL INC.
100 – 2545, rue Delorimier
Longueuil (Québec)
J4K 3P7

JUNE 2010

M09789



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APPENDIX A MASW sounding results



1. INTRODUCTION

Geophysics GPR International Inc. has been requested by Groupe ABS Inc. to carry out shear wave velocity soundings at 31 locations in the vicinity of the town of Saint-Valentin, Québec. This work is part of the geotechnical studies for a future wind farm. The geophysical investigations utilized the Multi-channel Analysis of Surface Waves (MASW) method to generate a shear wave velocity depth profile. The study aimed to obtain the average shear wave velocity for the first 30 metres of soil and rock.

The surveys were carried out between March 15 and 27, 2010 and on June 2nd, 2010.

2. SITE LOCATION

The town of Saint-Valentin is located about 60 km South-East of Montréal in the Montérégie administrative region. The soundings are located approximately within a 5 km radius from Saint-Valentin. Figure 1 shows a regional map of the Montérégie region. Figure 2 shows a local map with the position of each sounding site.

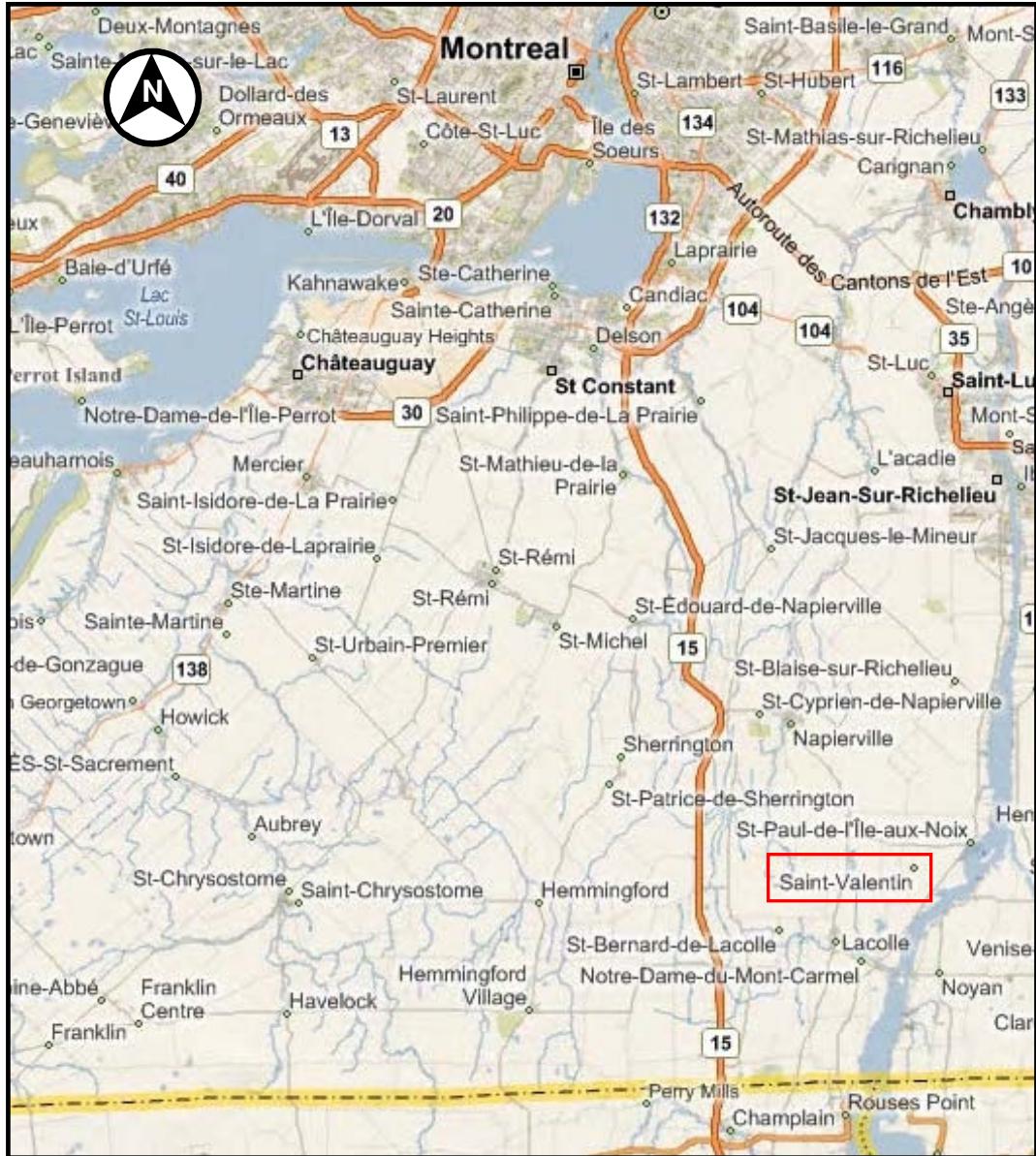
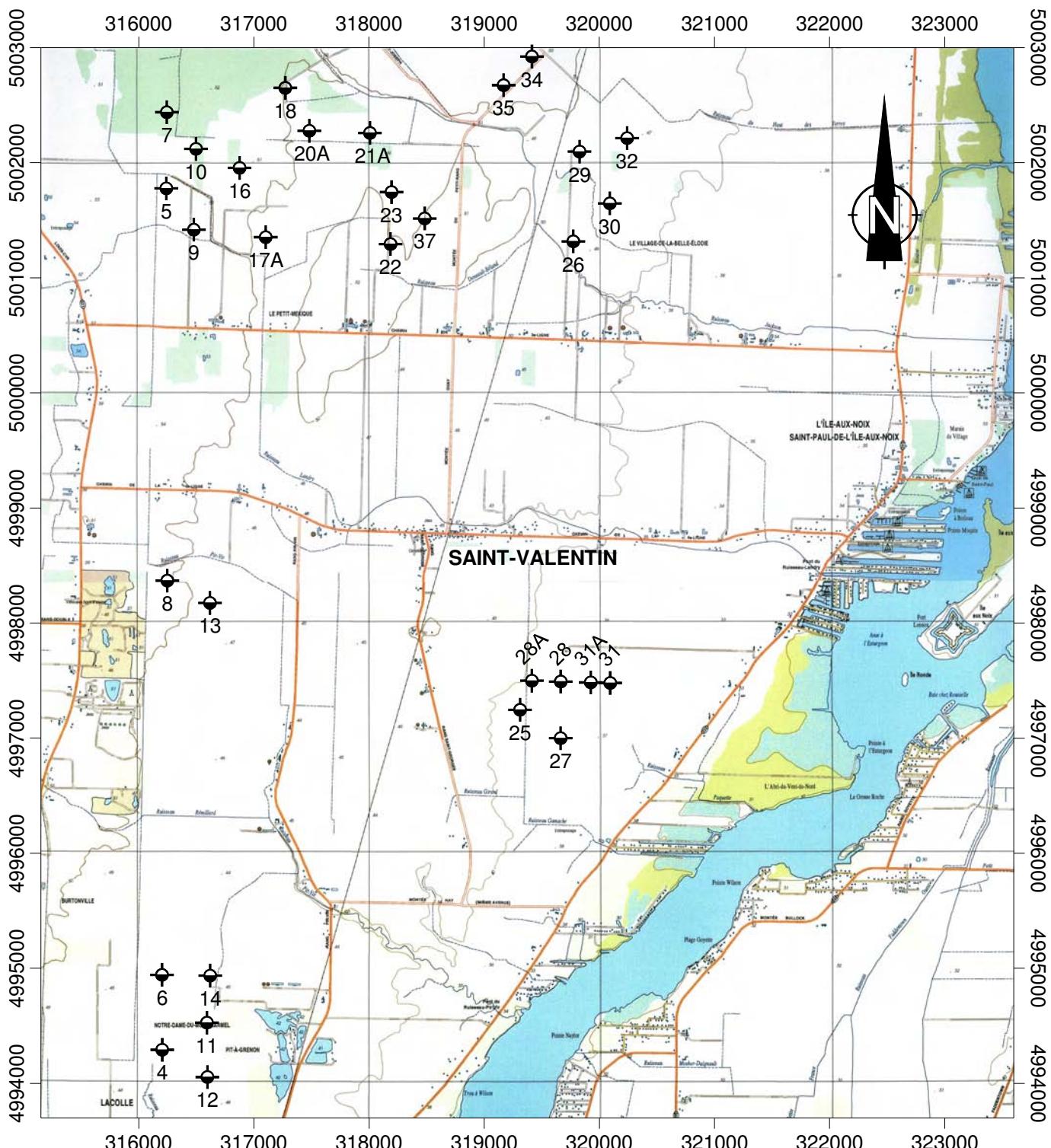


FIGURE 1
Location of Saint-Valentin within the Montérégie region (source: Bing Maps™)



Site coordinates provided by Groupe ABS

Scale 1 : 50 000
MTM NAD83 zone 8

FIGURE 2
MASW sounding locations



3. METHODOLOGY

3.1 Basic Theory

The Multi-channel Analysis of Surface Waves (MASW) and the Extended Spatial Autocorrelation Method (ESPAC) are seismic methods used to evaluate the shear wave velocities of subsurface materials through the analysis of the dispersion properties of Rayleigh surface waves ("ground roll"). The MASW is considered as an "active" method, as the seismic signal is induced at known location and time in the geophones spread axis. Conversely, the ESPAC is considered as a "passive" method, using the low frequency "noises" produced far away.

The dispersion properties are measured as a change in phase velocity with frequency. Surface wave energy will decay exponentially with depth. Lower frequency surface waves will travel deeper and thus be more influenced by deeper velocity layering than the shallow higher frequency waves. Inversion of the Rayleigh wave dispersion curve yields a shear wave (V_s) velocity depth profile (sounding). Figure 3 outlines the basic operating procedure for the MASW method. Figure 4 is an example image of a typical MASW record and resulting 1D V_s model.

The ESPAC method allows deeper V_s soundings, but with a poor resolution for the surface portion. Its dispersion curve can then be merged with the higher frequency curve from the MASW to allow a more complete inversion of the data. A detailed description of the MASW method can be found in the paper *Multi-channel Analysis of Surface Waves*, Park, C.B., Miller, R.D. and Xia, J. Geophysics, Vol. 64, No. 3 (May-June 1999); P. 800–808. For the SPAC method, one can refer to the paper *Shear Velocity Profiles Obtained from Microtremor Array Data with an Example from Direct Fitting of SPAC Curves*, Asten, M.W., 2007, Proceedings of the 20th SAGEEP Conference, Denver, Environmental and Engineering Geophysical Society.



3.2 Survey Design

The MASW survey utilizes a similar set-up to a seismic refraction investigation (i.e. 24 geophones in a linear array). The principle consists of intentionally generating a seismic wave at the surface and digitally recording the surface waves from the moment of source impact with a linear series of geophones on the surface.

A 12 pound sledgehammer was used as the primary energy source with traces being recorded off both ends of the seismic spread (4 shots per spread). Two geophone spacing values (1m and 3m) were used in order to get good resolution of surface velocities as well as good depth penetration. The total spread length was 23 m for the 1 m spacing and 69m for the 3m spacing. Unlike the refraction method, which produces a data point beneath each geophone, the shear wave depth profile is the average of the bulk area within the geophone spread, especially for its central half-length.

The orientation of the MASW spreads was determined on-site, depending on site access and clearance available.

3.3 Interpretation Method

The main processing sequence involved plotting, picking and 1D inversion of the MASW shot records using the SeisImagerSW™ software package. In theory, all the MASW shot records for a given spread should produce a similar shear wave velocity profile. In practice, however, differences can arise due to energy dissipation, localized surface variations, and/or dipping of overburden layers or rock. In general, the precision of the calculated seismic shear wave velocities (V_s) is of the order of 15% or better. When the penetration of the MASW shots was not sufficient, the same data points were processes using the ESPAC method to obtain greater depth penetration.



The results of the MASW tests are normally presented in chart format. It presents the 1-D shear wave velocity values from the inversion models of dispersion curves of the active MASW.

The V_{S30} value is based on the harmonic mean of the shear wave velocities, from the surface to a depth of 30 metres. The V_{S30} value is calculated by dividing the total depth of interest (e.g. 30m) by the sum of the time spent in each velocity layer from the surface up to that depth. This harmonic mean value reflects an equivalent single layer response.

The V_{S30} is used to determine the Site Classification for Seismic Site Response, as presented in the National Building Code of Canada (NBCC, 2005 ed.), as specified in table 4.1.8.4.A of the mentioned document¹.

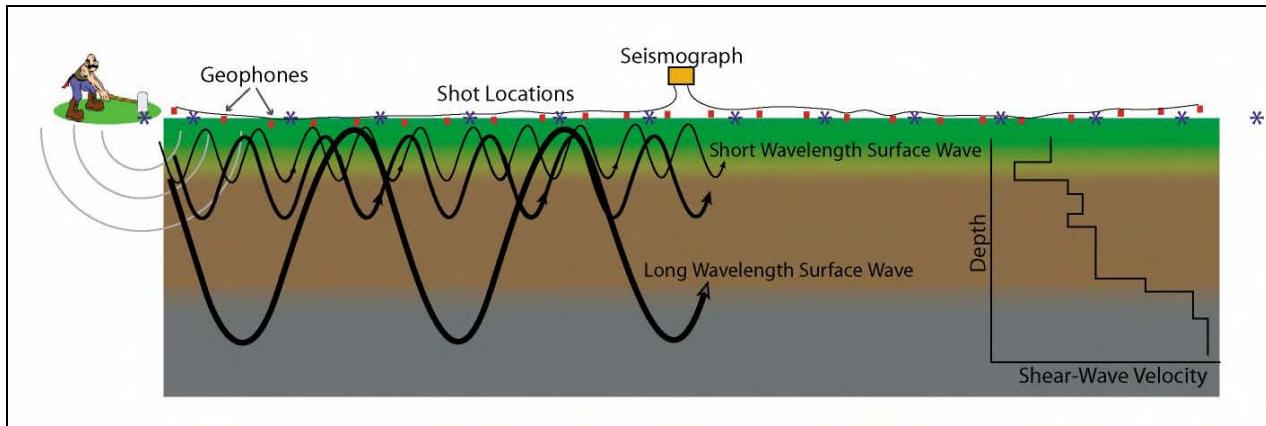


FIGURE 3
MASW Operating Principle

¹ NBCC. 2005. National Building Code of Canada 2005. Institute for Research in Construction, National Research Council of Canada, Ottawa, Ont.



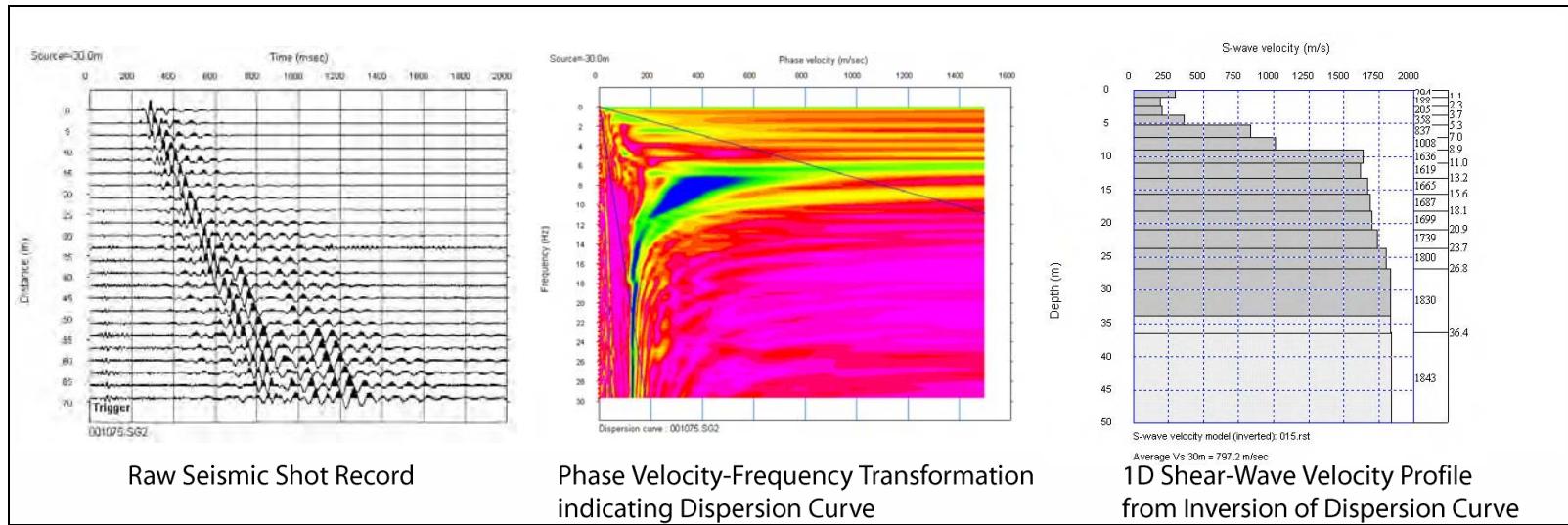


FIGURE 4

Example of a typical MASW shot record, phase velocity/frequency curve and resulting 1D shear wave velocity model



4. **RESULTS**

The MASW sounding results for each site investigated are presented in Appendix A. For each site, details of the V_{S30} calculations are presented in the table at the left of the 1D sounding profile. Site specific notes are included in each result sheet. As reference, the NBCC site classification is also indicated.

Table 1 shows the site coordinates provided by Groupe ABS.

The majority of the sites investigated show a similar velocity vs. depth distribution. This trend is characterized by a low velocity surface layer of a thickness of about 4 to 10 metres. In most cases, this layer shows abnormally low values that could be associated with a soil with liquefaction potential.

The low velocity layer is followed by an intermediate layer of variable thickness with an increasing V_s velocity in function of depth. Finally, a high velocity layer (bedrock in most cases) is detected beneath the intermediate layer. The high velocity layer is characterized by almost constant V_s . The velocity of this layer increases slightly with depth.

The MASW soundings were divided into five (5) groups in relation to their geographical position within the Saint-Valentin region. Average velocities for the three main layers and the average V_{S30} were computed and are presented in Table 2. These results indicate that the sounding sites within groups M and O show very low V_s velocities within the surface layer. Groups M and O are located to the South and South-East of Saint-Valentin.

In the case of the intermediate layer, it is groups N and O that show the lowest V_s velocities. These groups are located to the East and South of Saint-Valentin.

Group N shows the lowest average velocities for the hard layer. Borehole results indicate that the bedrock is located at depths over 30 metres in this area. Therefore, the measured shear wave velocities are only representative of the overburden in this area. This group also shows the lowest V_{S30} values of all five groups.



Overall, it is the sounding sites within group Q that show the highest shear wave velocities for all three principal layers as well as the average V_{S30} value. Group Q is the only group that does not have one or several sites with abnormally low V_S values for the surface layer that could be associated with a soil with liquefaction potential. Group Q is located at the North-East of Saint-Valentin.



TABLE 1 - MASW sounding site coordinates (MTM, NAD83, zone 8)

Site	Xc_MTM	Yc_MTM
4	316203	4994292
5	316239	5001777
6	316202	4994943
7	316244	5002438
8	316248	4998369
9	316478	5001418
10	316497	5002120
11	316592	4994528
12	316596	4994055
13	316618	4998175
14	316620	4994936
16	316876	5001955
17A	317102	5001353
18	317273	5002650
20A	317482	5002277
21A	318008	5002258
22	318187	5001293
23	318195	5001745
25	319312	4997246
26	319774	5001316
27	319664	4996999
28	319665	4997492
28A	319414	4997499
29	319828	5002096
30	320091	5001646
31	320095	4997479
31A	319926	4997484
32	320241	5002214
34	319415	5002922
35	319169	5002673
37	318483	5001515

coordinates provided by Groupe ABS



TABLE 2 – Average velocities vs. geographical groups

GROUP	SITES	AVERAGE VELOCITIES (m/s)			
		surface layer	intermediate layer	hard layer or bedrock	V_{S30}
M	4, 6, 11, 12, 14	134	742	1426	399
N	8, 13	245	590	1105	386
O	25, 27, 28, 28A, 31, 31A	150	575	1343	480
P	5, 7, 9, 10, 16, 17A, 18, 20A, 21A, 22, 23, 37	207	756	1400	606
Q	26, 29, 30, 32, 34, 35	264	880	1548	802
Average for all 31 sites		198	732	1403	572



5. **CONCLUSION**

Geophysical investigations with the MASW seismic method were carried out on 31 sites in the region of the town of Saint-Valentin, Québec. These surveys were part of the geotechnical studies for a wind farm project in the area.

The surveys allowed calculating the average shear wave velocities from the surface to a depth of 30 metres (V_{S30}). These values can be used to determine the Site Classification for Seismic Site Response, as presented in the National Building Code of Canada.

Results show that the 18 sites located at the north of the town of Saint-Valentin show higher V_{S30} values than the 13 sites located at the south of the town. A high number of the sites investigated show the presence of a surface layer with abnormally low shear wave velocity values that could be associated with a soil with liquefaction potential. Further geotechnical assessments are recommended for these sites.

It must be noted that other geotechnical information gleaned onsite; including the rock depth, the presence of liquefiable soils, soft clays, high moisture content etc. can supersede the site classification provided in this report based on V_{S30} value.

This report has been written by Daniel Campos Halas, Eng., M.A.Sc., with the collaboration of Jean-Luc Arsenault, Eng., M.A.Sc.

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APPENDIX A – MASW SOUNDING RESULTS



Groupe ABS / Wind Energy Converters (WEC) / Saint-Valentin, Qc

Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	78.4					
1.07	79.3	1.07	1.07	0.013658	0.013658	78.4
2.31	78.4	1.24	2.31	0.015584	0.029242	78.9
3.71	128.7	1.40	3.71	0.017871	0.047113	78.7
5.27	433.1	1.57	5.27	0.012164	0.059276	89.0
7.01	699.1	1.73	7.01	0.003996	0.063272	110.7
8.90	867.2	1.90	8.90	0.002712	0.065984	134.9
10.96	1599.3	2.06	10.96	0.002376	0.068360	160.4
13.19	1613.4	2.23	13.19	0.001391	0.069751	189.1
15.58	1600.6	2.39	15.58	0.001481	0.071233	218.7
18.13	1582.1	2.55	18.13	0.001596	0.072829	249.0
20.85	1572.5	2.72	20.85	0.001719	0.074548	279.7
23.74	1748.5	2.88	23.74	0.001834	0.076382	310.8
26.79	1801.1	3.05	26.79	0.001744	0.078126	342.9
30.00	1952.1	3.21	30.00	0.001785	0.079911	375.4

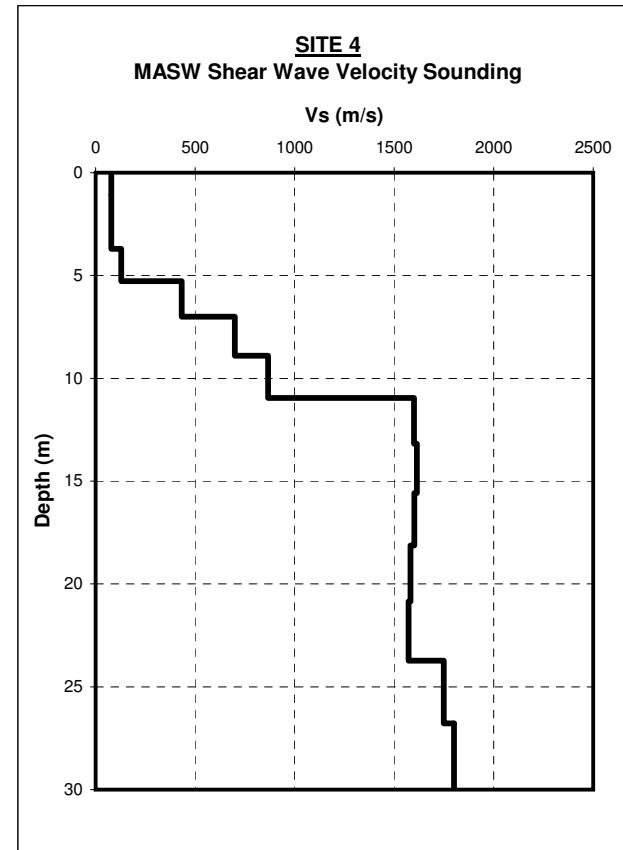
Location

Sounding: X (m) Y (m)
MTM/Nad83 316203 4994292

Vs30 (m/s) = 375.4
Class : C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 4-5 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	205.9					
1.07	190.3	1.07	1.07	0.005204	0.005204	205.9
2.31	165.8	1.24	2.31	0.006496	0.011701	197.2
3.71	175.9	1.40	3.71	0.008450	0.020151	184.1
5.27	315.4	1.57	5.27	0.008901	0.029051	181.6
7.01	589.9	1.73	7.01	0.005488	0.034539	202.8
8.90	1060.5	1.90	8.90	0.003214	0.037753	235.8
10.96	1267.8	2.06	10.96	0.001943	0.039696	276.1
13.19	1294.8	2.23	13.19	0.001755	0.041451	318.1
15.58	1377.5	2.39	15.58	0.001846	0.043297	359.8
18.13	1444.0	2.55	18.13	0.001855	0.045152	401.6
20.85	1492.5	2.72	20.85	0.001883	0.047035	443.3
23.74	1513.7	2.88	23.74	0.001933	0.048968	484.7
26.79	1528.6	3.05	26.79	0.002015	0.050983	525.4
30.00	1546.9	3.21	30.00	0.002103	0.053085	565.1

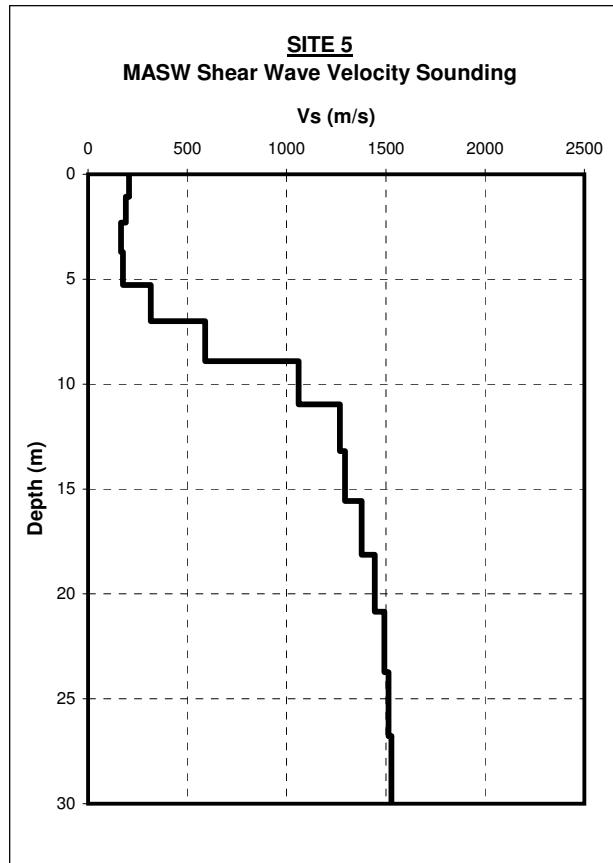
Location

Sounding: X (m) Y (m)
 MTM/Nad83 316239 5001777

Vs30 (m/s) 565.1
Class : C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 4-5 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.
- 3- The site coordinates were provided by the client.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	136.2726					
1.07	81.73054	1.07	1.07	0.007862	0.007862	136.3
2.31	133.5603	1.24	2.31	0.015126	0.022988	100.4
3.71	129.1482	1.40	3.71	0.010490	0.033479	110.8
5.27	240.9045	1.57	5.27	0.012125	0.045604	115.7
7.01	239.3755	1.73	7.01	0.007184	0.052788	132.7
8.90	259.3235	1.90	8.90	0.007919	0.060707	146.6
10.96	615.7848	2.06	10.96	0.007945	0.068653	159.7
13.19	1085.137	2.23	13.19	0.003614	0.072267	182.5
15.58	1297.528	2.39	15.58	0.002203	0.074469	209.2
18.13	1372.757	2.55	18.13	0.001969	0.076438	237.2
20.85	1371.588	2.72	20.85	0.001981	0.078419	265.9
23.74	1388.833	2.88	23.74	0.002103	0.080523	294.8
26.79	1390.087	3.05	26.79	0.002196	0.082718	323.8
30.00	1641.913	3.21	30.00	0.002312	0.085031	352.8

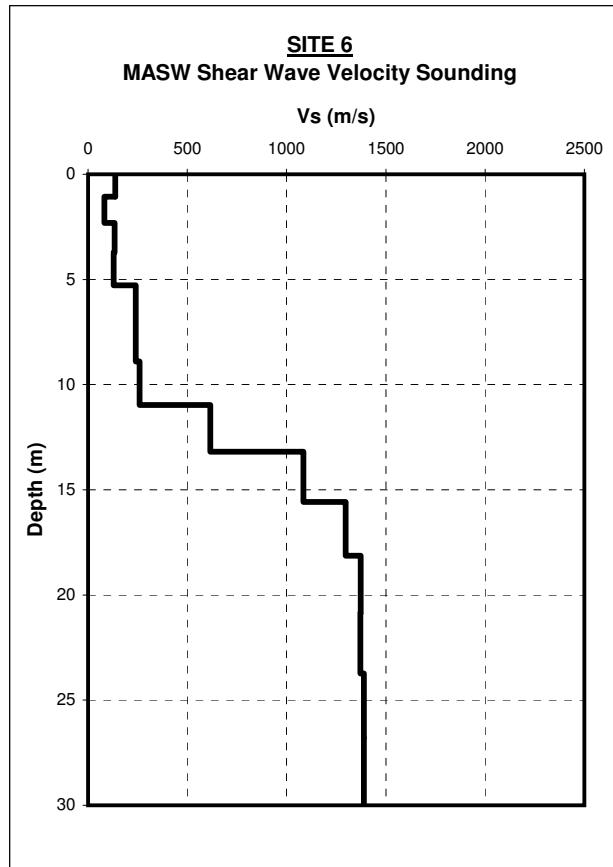
Location

Sounding: X (m) Y (m)
 MTM/Nad83 316202 4994943

Vs30 (m/s) 352.8
 Class : D

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 4-5 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains D, or be re-classified as a F.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	258.6					258.6
1.07	149.0	1.07	1.07	0.004144	0.004144	258.6
2.31	167.1	1.24	2.31	0.008297	0.012441	185.5
3.71	270.7	1.40	3.71	0.008386	0.020827	178.1
5.27	374.1	1.57	5.27	0.005785	0.026612	198.2
7.01	492.8	1.73	7.01	0.004627	0.031238	224.3
8.90	385.9	1.90	8.90	0.003847	0.035085	253.7
10.96	691.3	2.06	10.96	0.005340	0.040425	271.2
13.19	1307.8	2.23	13.19	0.003219	0.043644	302.1
15.58	1401.2	2.39	15.58	0.001828	0.045471	342.6
18.13	1464.8	2.55	18.13	0.001823	0.047295	383.4
20.85	1485.6	2.72	20.85	0.001857	0.049152	424.2
23.74	1490.0	2.88	23.74	0.001942	0.051093	464.6
26.79	1667.5	3.05	26.79	0.002047	0.053140	504.1
30.00	2141.1	3.21	30.00	0.001928	0.055068	544.8

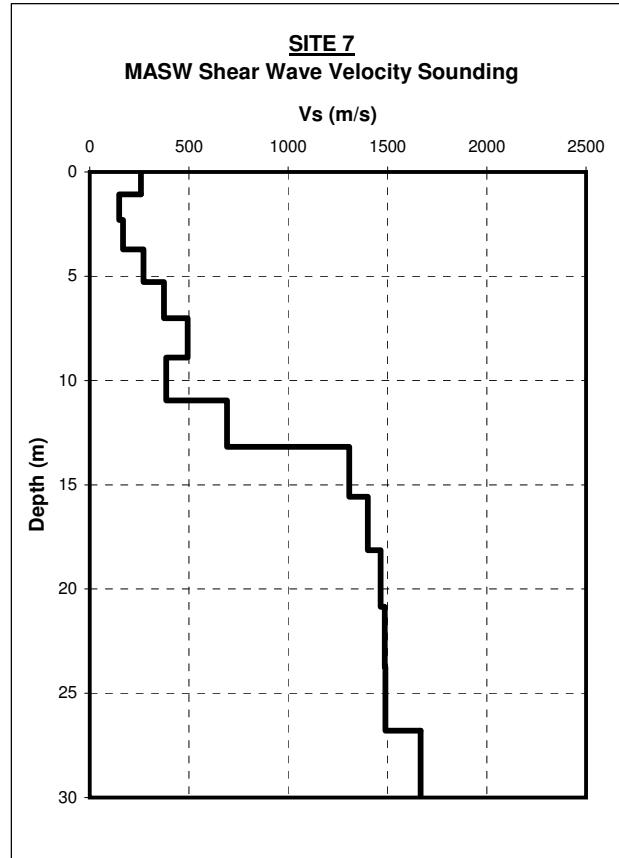
Location

Sounding: X (m) Y (m)
MTM/Nad83 316244 5002438

Vs30 (m/s) 544.8
Class : C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 3-4 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.
- 3- The site coordinates were provided by the client.



Groupe ABS / Wind Energy Converters (WEC) / Saint-Valentin, Qc

Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	153.4					153.4
1.07	194.3	1.07	1.07	0.006984	0.006984	153.4
2.31	229.9	1.24	2.31	0.006362	0.013347	172.9
3.71	258.1	1.40	3.71	0.006095	0.019442	190.8
5.27	246.4	1.57	5.27	0.006067	0.025509	206.8
7.01	261.6	1.73	7.01	0.007024	0.032534	215.3
8.90	346.6	1.90	8.90	0.007245	0.039779	223.8
10.96	480.9	2.06	10.96	0.005944	0.045723	239.7
13.19	501.4	2.23	13.19	0.004627	0.050350	261.9
15.58	518.2	2.39	15.58	0.004767	0.055117	282.6
18.13	546.1	2.55	18.13	0.004931	0.060048	302.0
20.85	649.1	2.72	20.85	0.004980	0.065028	320.7
23.74	974.0	2.88	23.74	0.004444	0.069472	341.7
26.79	1336.1	3.05	26.79	0.003131	0.072603	368.9
30.00	1365.0	3.21	30.00	0.002406	0.075008	400.0

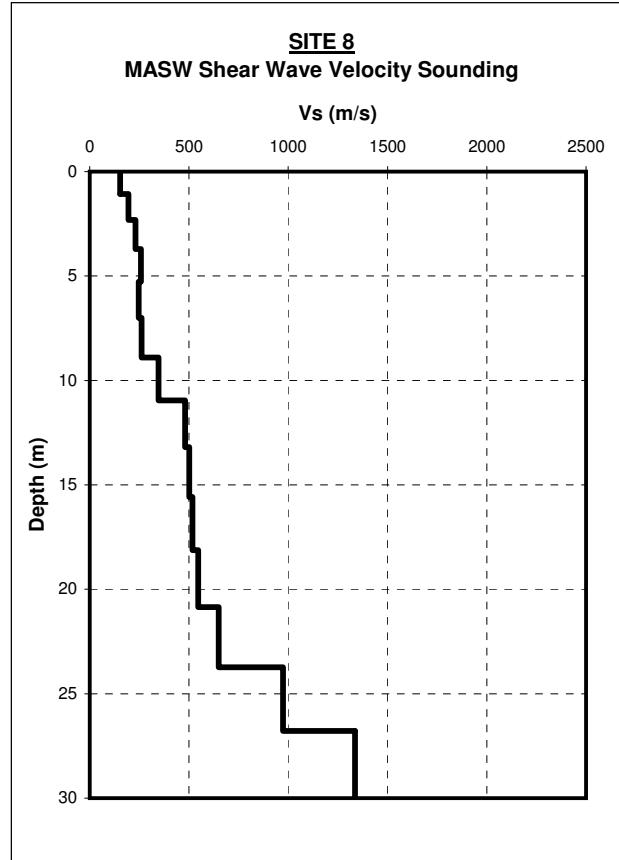
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	316248	4998369

Vs30 (m/s)	400.0
Class :	C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.



Groupe ABS / Wind Energy Converters (WEC) / Saint-Valentin, Qc

Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	277.3					277.3
1.07	156.0	1.07	1.07	0.003864	0.003864	277.3
2.31	172.6	1.24	2.31	0.007924	0.011789	195.8
3.71	438.9	1.40	3.71	0.008118	0.019907	186.3
5.27	242.0	1.57	5.27	0.003568	0.023474	224.7
7.01	579.4	1.73	7.01	0.007153	0.030627	228.7
8.90	989.6	1.90	8.90	0.003272	0.033899	262.6
10.96	1311.4	2.06	10.96	0.002082	0.035981	304.6
13.19	1364.2	2.23	13.19	0.001697	0.037678	350.0
15.58	1602.4	2.39	15.58	0.001752	0.039430	395.1
18.13	1600.3	2.55	18.13	0.001594	0.041024	442.0
20.85	1685.3	2.72	20.85	0.001699	0.042724	488.1
23.74	1601.3	2.88	23.74	0.001712	0.044435	534.2
26.79	1551.2	3.05	26.79	0.001904	0.046340	578.0
30.00	2728.1	3.21	30.00	0.002072	0.048412	619.7

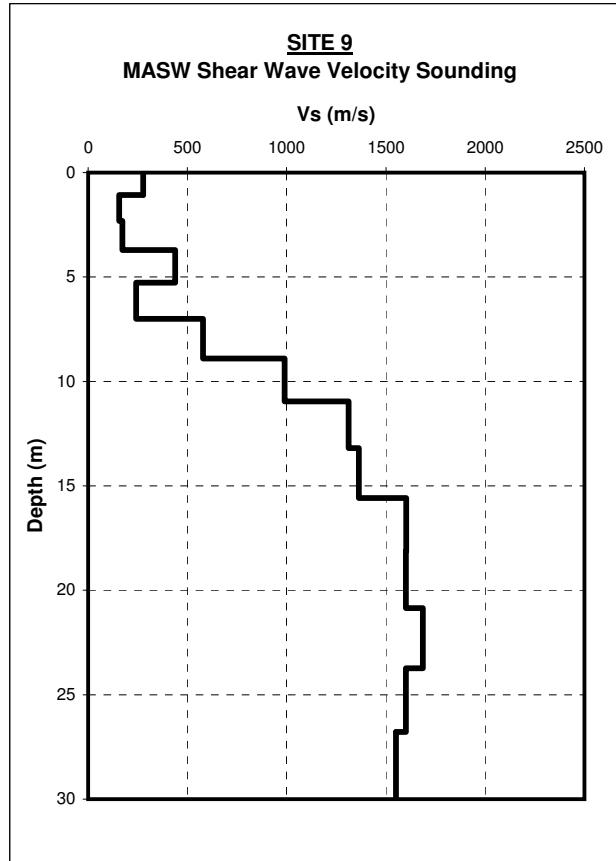
Location

Sounding: X (m) Y (m)
MTM/Nad83 316478 5001418

Vs30 (m/s) 619.7
Class : C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 2-4 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



Groupe ABS / Wind Energy Converters (WEC) / Saint-Valentin, Qc

Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	310.9					
1.07	140.2	1.07	1.07	0.003446	0.003446	310.9
2.31	341.8	1.24	2.31	0.008818	0.012264	188.2
3.71	297.5	1.40	3.71	0.004099	0.016362	226.7
5.27	400.3	1.57	5.27	0.005264	0.021626	243.9
7.01	501.6	1.73	7.01	0.004324	0.025950	270.0
8.90	545.6	1.90	8.90	0.003779	0.029729	299.4
10.96	679.2	2.06	10.96	0.003776	0.033505	327.2
13.19	778.2	2.23	13.19	0.003276	0.036781	358.5
15.58	827.0	2.39	15.58	0.003071	0.039853	390.9
18.13	853.9	2.55	18.13	0.003090	0.042942	422.2
20.85	826.7	2.72	20.85	0.003185	0.046127	452.0
23.74	840.3	2.88	23.74	0.003489	0.049617	478.4
26.79	1136.0	3.05	26.79	0.003629	0.053246	503.1
30.00	1492.2	3.21	30.00	0.002829	0.056075	535.0

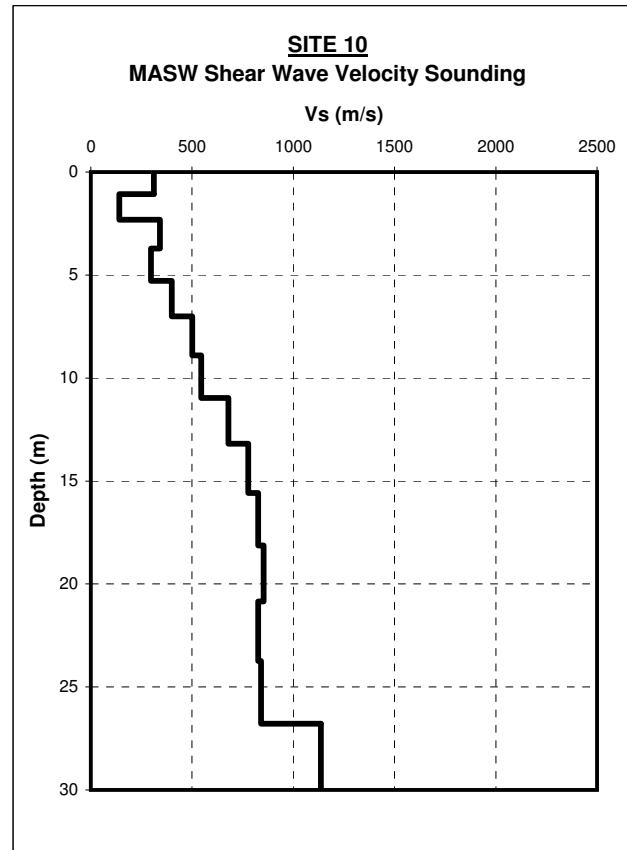
Location

Sounding: X (m) Y (m)
 MTM/Nad83 316497 5002120

Vs30 (m/s)	535.0
Class :	C

NOTES:

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	98.2					
1.07	111.7	1.07	1.07	0.010915	0.010915	98.2
2.31	108.4	1.24	2.31	0.011066	0.021980	105.0
3.71	170.0	1.40	3.71	0.012924	0.034904	106.3
5.27	203.8	1.57	5.27	0.009212	0.044116	119.6
7.01	226.4	1.73	7.01	0.008492	0.052608	133.2
8.90	621.0	1.90	8.90	0.008374	0.060982	146.0
10.96	833.5	2.06	10.96	0.003318	0.064300	170.5
13.19	1179.2	2.23	13.19	0.002670	0.066970	196.9
15.58	1415.3	2.39	15.58	0.002027	0.068997	225.8
18.13	1435.3	2.55	18.13	0.001805	0.070802	256.1
20.85	1447.4	2.72	20.85	0.001895	0.072697	286.8
23.74	1456.4	2.88	23.74	0.001993	0.074690	317.8
26.79	1471.5	3.05	26.79	0.002094	0.076784	348.8
30.00	1507.5	3.21	30.00	0.002184	0.078968	379.9

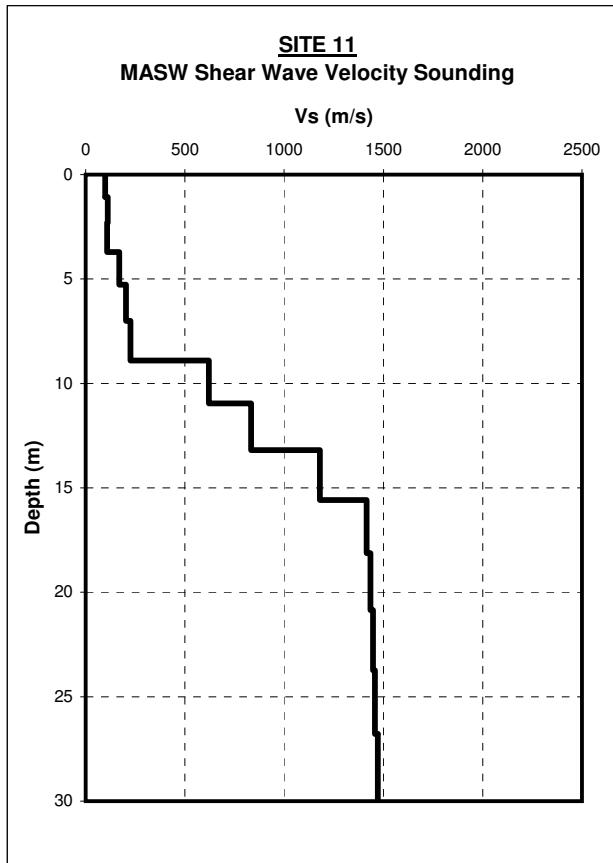
Location

Sounding: X (m) Y (m)
MTM/Nad83 316592 4994528

Vs30 (m/s) 379.9
Class : C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 4-5 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	129.2					
1.07	96.3	1.07	1.07	0.008291	0.008291	129.2
2.31	111.0	1.24	2.31	0.012842	0.021133	109.2
3.71	223.8	1.40	3.71	0.012621	0.033753	109.9
5.27	236.8	1.57	5.27	0.006998	0.040752	129.4
7.01	728.5	1.73	7.01	0.007310	0.048061	145.8
8.90	753.7	1.90	8.90	0.002602	0.050663	175.7
10.96	764.1	2.06	10.96	0.002734	0.053397	205.3
13.19	774.5	2.23	13.19	0.002912	0.056309	234.2
15.58	1173.5	2.39	15.58	0.003086	0.059395	262.3
18.13	1204.7	2.55	18.13	0.002177	0.061573	294.5
20.85	1237.6	2.72	20.85	0.002258	0.063830	326.7
23.74	1250.7	2.88	23.74	0.002331	0.066161	358.8
26.79	1265.4	3.05	26.79	0.002438	0.068599	390.5
30.00	1284.4	3.21	30.00	0.002540	0.071140	421.7

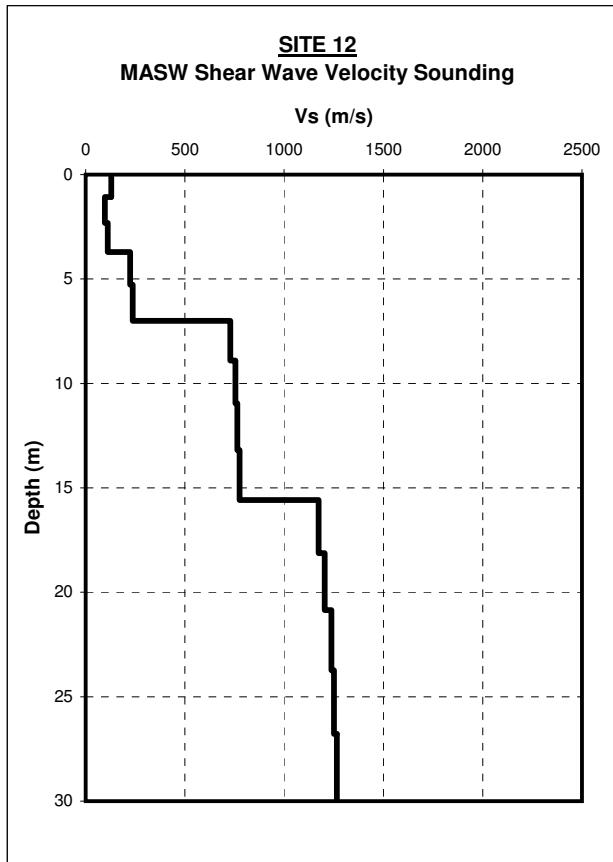
Location

Sounding: X (m) Y (m)
MTM/Nad83 316596 4994055

Vs30 (m/s) 421.7
Class : C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 4-7 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	354.5					
1.07	191.0	1.07	1.07	0.003022	0.003022	354.5
2.31	212.2	1.24	2.31	0.006474	0.009496	243.0
3.71	269.7	1.40	3.71	0.006602	0.016098	230.4
5.27	239.4	1.57	5.27	0.005806	0.021904	240.8
7.01	234.2	1.73	7.01	0.007230	0.029134	240.5
8.90	247.2	1.90	8.90	0.008095	0.037229	239.1
10.96	379.9	2.06	10.96	0.008336	0.045565	240.6
13.19	392.9	2.23	13.19	0.005858	0.051423	256.4
15.58	395.5	2.39	15.58	0.006083	0.057506	270.9
18.13	629.8	2.55	18.13	0.006460	0.063966	283.5
20.85	638.3	2.72	20.85	0.004319	0.068285	305.4
23.74	740.7	2.88	23.74	0.004519	0.072804	326.0
26.79	882.0	3.05	26.79	0.004117	0.076921	348.2
30.00	1468.3	3.21	30.00	0.003644	0.080565	372.4

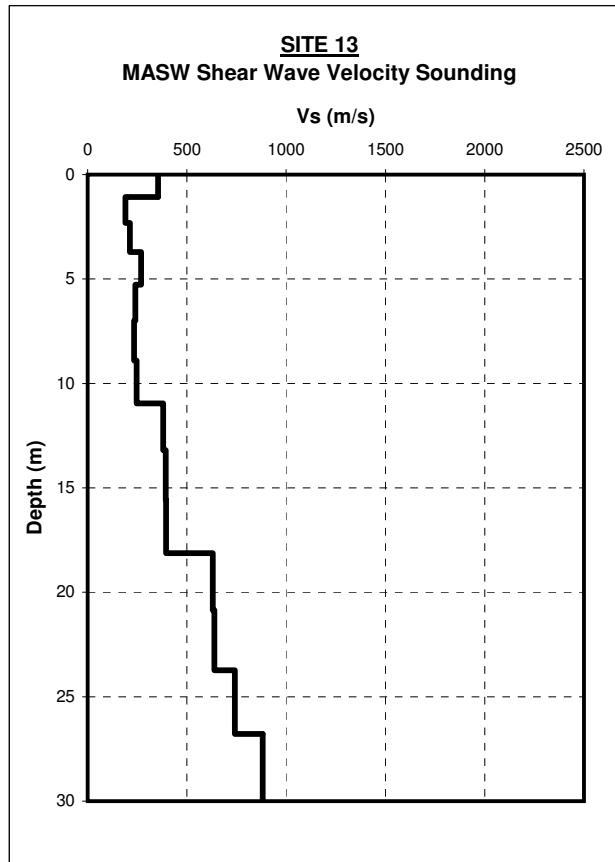
Location

Sounding: X (m) Y (m)
MTM/Nad83 316618 4998175

Vs30 (m/s) 372.4
Class : C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 2-9 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	131.3					
1.07	167.1	1.07	1.07	0.008159	0.008159	131.3
2.31	179.0	1.24	2.31	0.007398	0.015558	148.3
3.71	199.3	1.40	3.71	0.007825	0.023383	158.6
5.27	247.1	1.57	5.27	0.007858	0.031241	168.8
7.01	296.1	1.73	7.01	0.007003	0.038244	183.2
8.90	391.8	1.90	8.90	0.006402	0.044646	199.4
10.96	821.2	2.06	10.96	0.005258	0.049905	219.7
13.19	1210.4	2.23	13.19	0.002710	0.052614	250.6
15.58	1335.5	2.39	15.58	0.001975	0.054589	285.3
18.13	1398.5	2.55	18.13	0.001913	0.056502	320.9
20.85	1460.2	2.72	20.85	0.001945	0.058447	356.8
23.74	1560.7	2.88	23.74	0.001976	0.060422	392.8
26.79	1594.2	3.05	26.79	0.001954	0.062376	429.4
30.00	1648.6	3.21	30.00	0.002016	0.064392	465.9

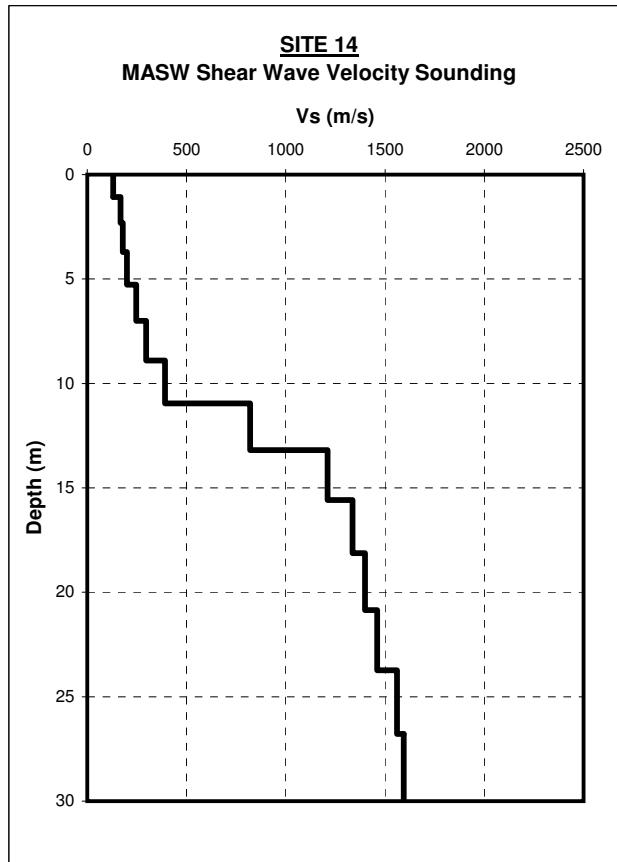
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	316620	4994936

Vs30 (m/s)	465.9
Class :	C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 4-5 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



Groupe ABS / Wind Energy Converters (WEC) / Saint-Valentin, Qc

Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	245.8					
1.07	181.4	1.07	1.07	0.004358	0.004358	245.8
2.31	506.1	1.24	2.31	0.006816	0.011174	206.5
3.71	256.7	1.40	3.71	0.002768	0.013942	266.0
5.27	584.1	1.57	5.27	0.006101	0.020044	263.2
7.01	772.2	1.73	7.01	0.002963	0.023007	304.5
8.90	529.8	1.90	8.90	0.002455	0.025461	349.6
10.96	737.2	2.06	10.96	0.003889	0.029351	373.5
13.19	1581.0	2.23	13.19	0.003018	0.032369	407.4
15.58	1638.5	2.39	15.58	0.001512	0.033881	459.8
18.13	1641.9	2.55	18.13	0.001559	0.035440	511.6
20.85	1716.3	2.72	20.85	0.001656	0.037097	562.1
23.74	1696.1	2.88	23.74	0.001681	0.038777	612.1
26.79	1646.8	3.05	26.79	0.001798	0.040575	660.2
30.00	1716.3	3.21	30.00	0.001952	0.042527	705.4

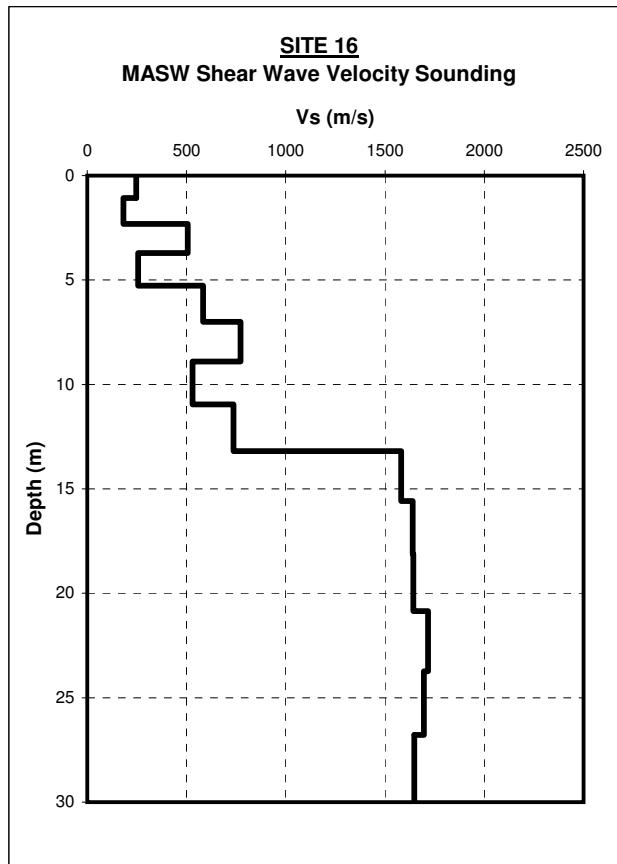
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	316876	5001955

Vs30 (m/s)	705.4
Class :	C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	115.0					
1.07	105.6	1.07	1.07	0.009318	0.009318	115.0
2.31	271.6	1.24	2.31	0.011706	0.021024	109.8
3.71	232.9	1.40	3.71	0.005158	0.026182	141.7
5.27	272.9	1.57	5.27	0.006725	0.032907	160.3
7.01	449.7	1.73	7.01	0.006342	0.039248	178.5
8.90	691.6	1.90	8.90	0.004215	0.043463	204.8
10.96	886.5	2.06	10.96	0.002979	0.046443	236.0
13.19	1010.1	2.23	13.19	0.002510	0.048953	269.4
15.58	1089.6	2.39	15.58	0.002366	0.051319	303.5
18.13	1137.1	2.55	18.13	0.002345	0.053664	337.9
20.85	1175.8	2.72	20.85	0.002392	0.056055	372.0
23.74	1295.0	2.88	23.74	0.002453	0.058509	405.7
26.79	1612.7	3.05	26.79	0.002355	0.060864	440.1
30.00	1751.3	3.21	30.00	0.001993	0.062857	477.3

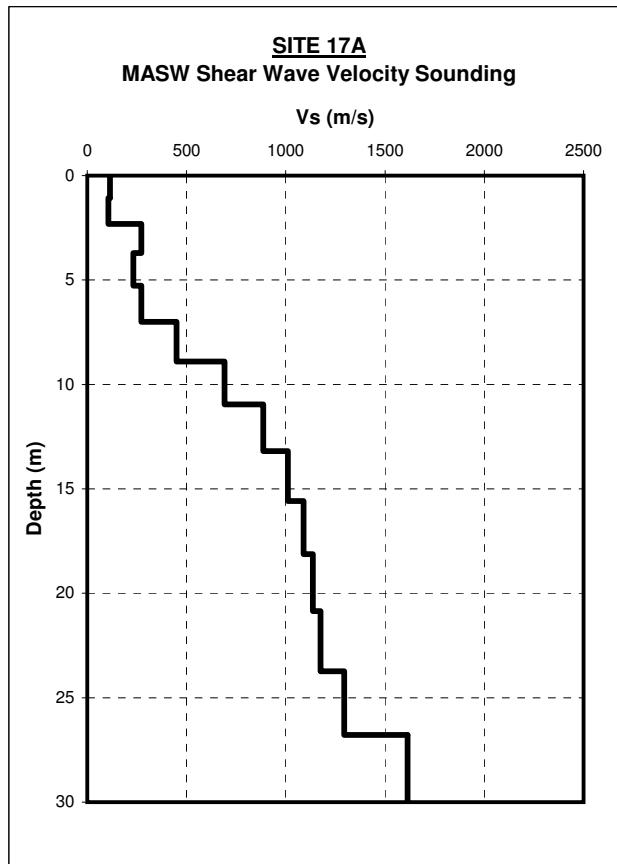
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	317102	5001353

Vs30 (m/s)	477.3
Class :	C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 2-5 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



Groupe ABS / Wind Energy Converters (WEC) / Saint-Valentin, Qc

Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	158.9					
1.07	197.8	1.07	1.07	0.006743	0.006743	158.9
2.31	257.8	1.24	2.31	0.006251	0.012994	177.6
3.71	421.7	1.40	3.71	0.005434	0.018428	201.3
5.27	515.8	1.57	5.27	0.003713	0.022142	238.2
7.01	1145.7	1.73	7.01	0.003355	0.025497	274.8
8.90	1406.6	1.90	8.90	0.001655	0.027152	327.8
10.96	1416.0	2.06	10.96	0.001465	0.028616	383.0
13.19	1427.8	2.23	13.19	0.001572	0.030188	436.8
15.58	1440.0	2.39	15.58	0.001674	0.031862	488.9
18.13	1466.9	2.55	18.13	0.001774	0.033636	539.1
20.85	1486.0	2.72	20.85	0.001854	0.035490	587.5
23.74	1518.1	2.88	23.74	0.001941	0.037432	634.1
26.79	1548.8	3.05	26.79	0.002009	0.039440	679.1
30.00	1716.2	3.21	30.00	0.002075	0.041516	722.6

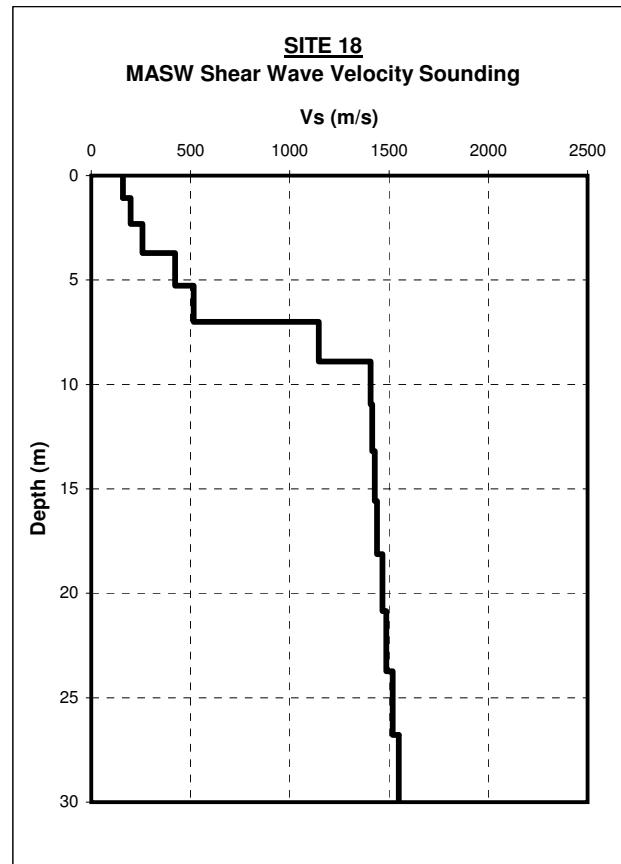
Location

Sounding: X (m) Y (m)
MTM/Nad83 317273 5002650

Vs30 (m/s) 722.6
Class : C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The site coordinates were provided by the client.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	155.2					
1.07	125.0	1.07	1.07	0.006902	0.006902	155.2
2.31	155.2	1.24	2.31	0.009888	0.016790	137.4
3.71	248.4	1.40	3.71	0.009026	0.025816	143.7
5.27	390.5	1.57	5.27	0.006305	0.032121	164.2
7.01	678.1	1.73	7.01	0.004432	0.036553	191.7
8.90	707.5	1.90	8.90	0.002795	0.039349	226.2
10.96	760.0	2.06	10.96	0.002912	0.042261	259.4
13.19	900.3	2.23	13.19	0.002928	0.045189	291.8
15.58	945.9	2.39	15.58	0.002655	0.047843	325.6
18.13	1111.1	2.55	18.13	0.002701	0.050544	358.7
20.85	1137.3	2.72	20.85	0.002448	0.052992	393.5
23.74	1330.1	2.88	23.74	0.002536	0.055529	427.5
26.79	1356.2	3.05	26.79	0.002293	0.057821	463.2
30.00	1790.8	3.21	30.00	0.002370	0.060191	498.4

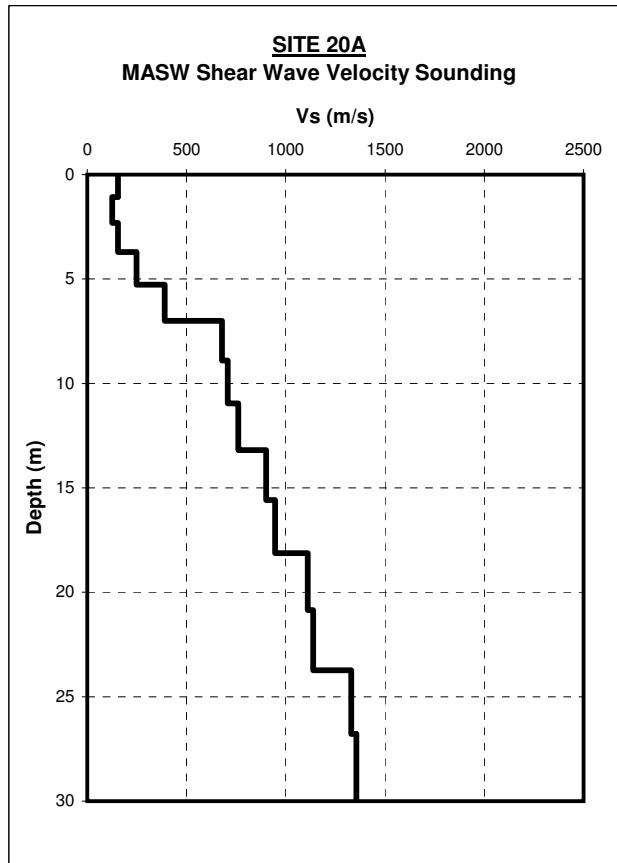
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	317482	5002277

Vs30 (m/s)	498.4
Class :	C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 2-4 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	820.2					
1.07	59.0	1.07	1.07	0.001306	0.001306	820.2
2.31	192.5	1.24	2.31	0.020965	0.022271	103.6
3.71	217.7	1.40	3.71	0.007279	0.029550	125.5
5.27	257.2	1.57	5.27	0.007192	0.036742	143.6
7.01	392.9	1.73	7.01	0.006728	0.043470	161.2
8.90	532.0	1.90	8.90	0.004825	0.048295	184.3
10.96	1395.4	2.06	10.96	0.003873	0.052168	210.1
13.19	1411.5	2.23	13.19	0.001595	0.053763	245.3
15.58	1411.5	2.39	15.58	0.001693	0.055456	280.9
18.13	1430.8	2.55	18.13	0.001810	0.057266	316.6
20.85	1442.7	2.72	20.85	0.001901	0.059167	352.4
23.74	1475.4	2.88	23.74	0.001999	0.061167	388.1
26.79	1515.5	3.05	26.79	0.002067	0.063234	423.6
30.00	1537.7	3.21	30.00	0.002121	0.065355	459.0

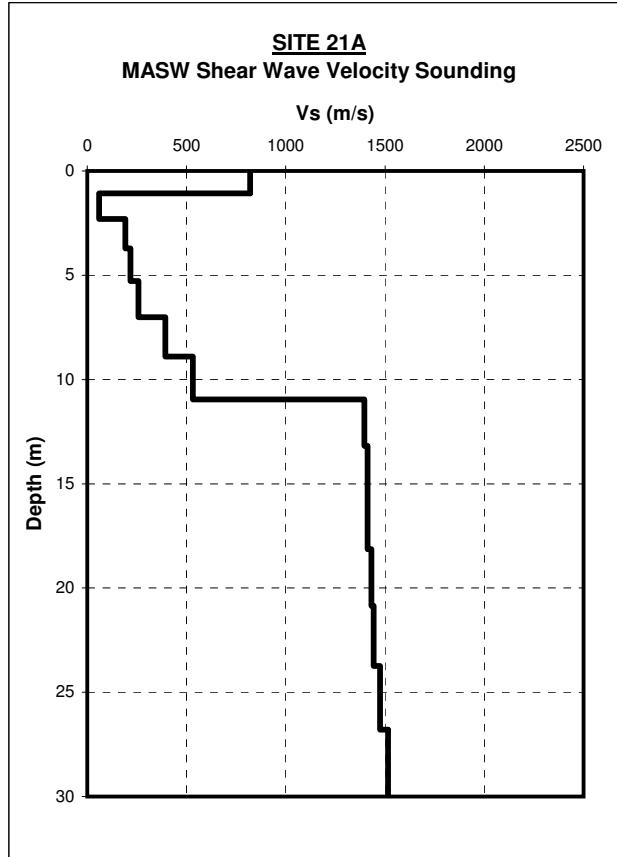
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	318008	5002258

Vs30 (m/s)	459.0
Class :	C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 4-5 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.
- 3- The site coordinates were provided by the client.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	225.7					
1.07	194.3	1.07	1.07	0.004748	0.004748	225.7
2.31	224.8	1.24	2.31	0.006363	0.011111	207.7
3.71	275.3	1.40	3.71	0.006233	0.017344	213.8
5.27	388.1	1.57	5.27	0.005687	0.023031	229.0
7.01	517.3	1.73	7.01	0.004460	0.027491	254.8
8.90	608.3	1.90	8.90	0.003664	0.031155	285.7
10.96	626.8	2.06	10.96	0.003387	0.034542	317.3
13.19	966.1	2.23	13.19	0.003550	0.038093	346.2
15.58	1099.7	2.39	15.58	0.002474	0.040567	384.0
18.13	1106.1	2.55	18.13	0.002323	0.042890	422.8
20.85	1121.1	2.72	20.85	0.002459	0.045349	459.8
23.74	1129.8	2.88	23.74	0.002573	0.047922	495.3
26.79	1199.6	3.05	26.79	0.002699	0.050621	529.1
30.00	1386.8	3.21	30.00	0.002680	0.053301	562.8

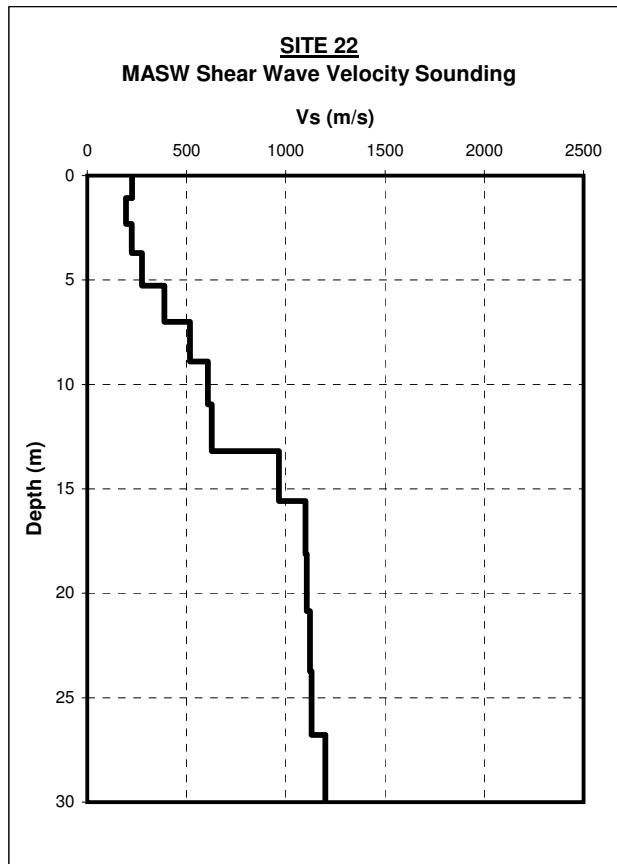
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	318187	5001293

Vs30 (m/s)	562.8
Class :	C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 4-5 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	119.6					
1.07	187.1	1.07	1.07	0.008957	0.008957	119.6
2.31	221.7	1.24	2.31	0.006606	0.015563	148.3
3.71	222.3	1.40	3.71	0.006321	0.021884	169.5
5.27	704.3	1.57	5.27	0.007045	0.028929	182.3
7.01	983.0	1.73	7.01	0.002457	0.031386	223.2
8.90	1212.6	1.90	8.90	0.001928	0.033315	267.2
10.96	1774.4	2.06	10.96	0.001699	0.035014	313.1
13.19	1862.9	2.23	13.19	0.001254	0.036268	363.6
15.58	1824.9	2.39	15.58	0.001283	0.037551	414.8
18.13	1798.4	2.55	18.13	0.001400	0.038951	465.5
20.85	1818.5	2.72	20.85	0.001512	0.040463	515.3
23.74	1901.6	2.88	23.74	0.001586	0.042050	564.5
26.79	1924.8	3.05	26.79	0.001604	0.043653	613.6
30.00	2437.9	3.21	30.00	0.001670	0.045323	661.9

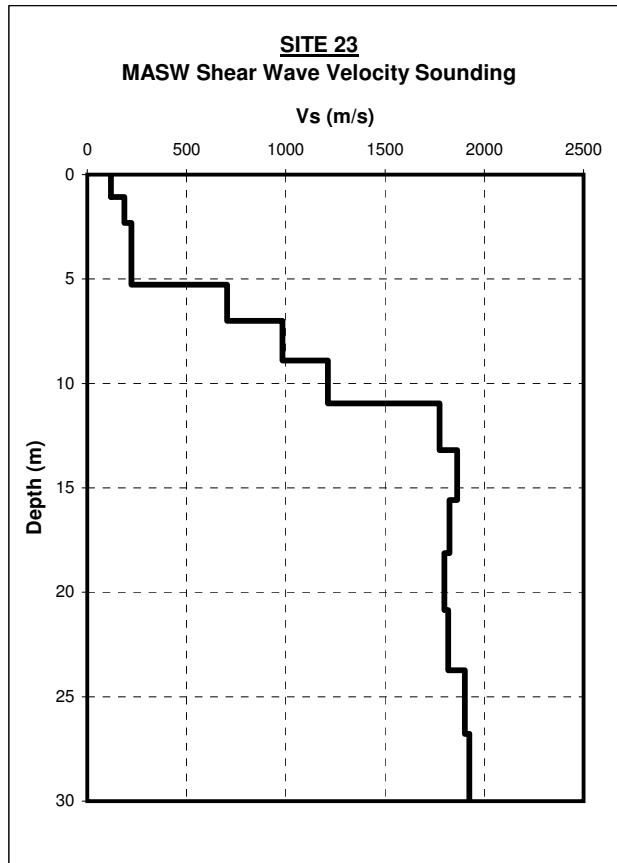
Location

Sounding: X (m) Y (m)
MTM/Nad83 318195 5001745

Vs30 (m/s) 661.9
Class : C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 4-5 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	123.0					
1.07	97.6	1.07	1.07	0.008714	0.008714	123.0
2.31	130.3	1.24	2.31	0.012669	0.021384	107.9
3.71	355.9	1.40	3.71	0.010754	0.032137	115.4
5.27	567.9	1.57	5.27	0.004400	0.036537	144.4
7.01	668.1	1.73	7.01	0.003048	0.039585	177.0
8.90	695.1	1.90	8.90	0.002837	0.042423	209.8
10.96	1014.1	2.06	10.96	0.002964	0.045387	241.5
13.19	1162.9	2.23	13.19	0.002194	0.047581	277.1
15.58	1166.1	2.39	15.58	0.002055	0.049637	313.8
18.13	1163.9	2.55	18.13	0.002191	0.051828	349.8
20.85	1196.4	2.72	20.85	0.002337	0.054164	385.0
23.74	1185.9	2.88	23.74	0.002411	0.056575	419.6
26.79	1182.8	3.05	26.79	0.002572	0.059147	452.9
30.00	1317.0	3.21	30.00	0.002717	0.061864	484.9

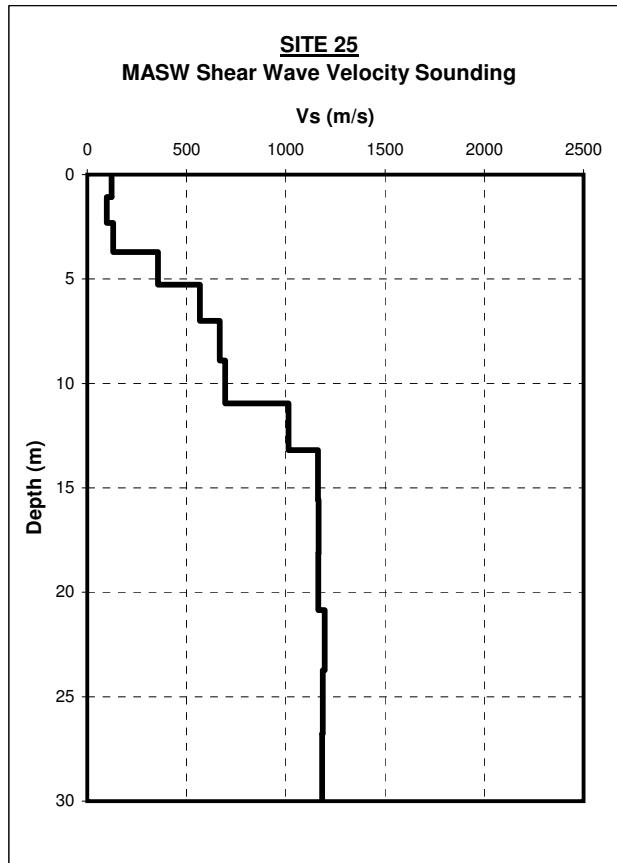
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	319312	4997246

Vs30 (m/s)	484.9
Class :	C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 4 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



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Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	173.4					
1.07	172.9	1.07	1.07	0.006178	0.006178	173.4
2.31	357.4	1.24	2.31	0.007152	0.013330	173.1
3.71	409.2	1.40	3.71	0.003920	0.017250	215.0
5.27	993.4	1.57	5.27	0.003827	0.021077	250.3
7.01	1144.9	1.73	7.01	0.001742	0.022820	307.0
8.90	1189.2	1.90	8.90	0.001656	0.024475	363.7
10.96	1241.8	2.06	10.96	0.001733	0.026208	418.3
13.19	1281.8	2.23	13.19	0.001792	0.028000	471.0
15.58	1324.5	2.39	15.58	0.001865	0.029865	521.6
18.13	1353.7	2.55	18.13	0.001929	0.031794	570.3
20.85	1395.9	2.72	20.85	0.002009	0.033803	616.9
23.74	1509.9	2.88	23.74	0.002066	0.035869	661.7
26.79	1643.0	3.05	26.79	0.002020	0.037889	707.0
30.00	2181.4	3.21	30.00	0.001956	0.039845	752.9

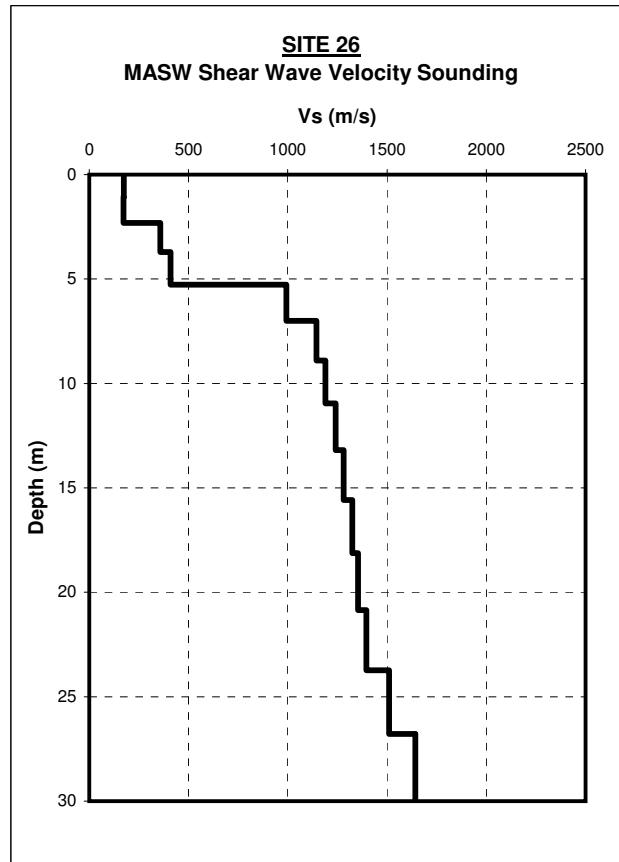
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	319774	5001316

Vs30 (m/s)	752.9
Class :	C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	169.3					
1.07	106.8	1.07	1.07	0.006330	0.006330	169.3
2.31	144.6	1.24	2.31	0.011578	0.017908	128.9
3.71	194.3	1.40	3.71	0.009688	0.027595	134.4
5.27	305.7	1.57	5.27	0.008058	0.035653	147.9
7.01	411.3	1.73	7.01	0.005661	0.041314	169.6
8.90	486.2	1.90	8.90	0.004609	0.045923	193.8
10.96	1175.8	2.06	10.96	0.004238	0.050161	218.5
13.19	1303.2	2.23	13.19	0.001893	0.052054	253.3
15.58	1331.4	2.39	15.58	0.001834	0.053888	289.1
18.13	1355.6	2.55	18.13	0.001919	0.055807	324.9
20.85	1371.4	2.72	20.85	0.002006	0.057813	360.7
23.74	1383.8	2.88	23.74	0.002103	0.059917	396.2
26.79	1445.2	3.05	26.79	0.002204	0.062120	431.2
30.00	1671.3	3.21	30.00	0.002224	0.064344	466.2

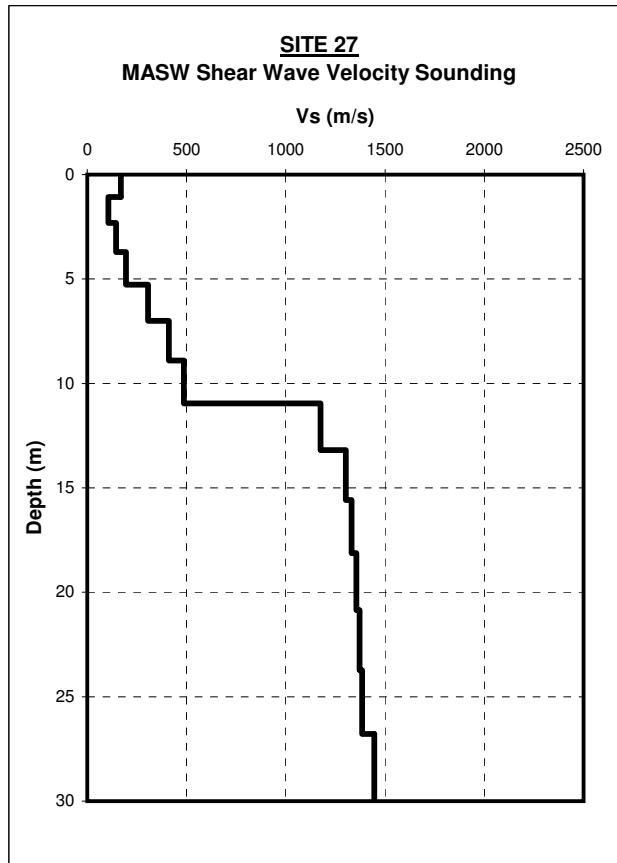
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	319664	4996999

Vs30 (m/s)	466.2
Class :	C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 4-5 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	177.6					
1.07	130.5	1.07	1.07	0.006035	0.006035	177.6
2.31	131.2	1.24	2.31	0.009473	0.015508	148.8
3.71	161.8	1.40	3.71	0.010677	0.026185	141.6
5.27	419.9	1.57	5.27	0.009679	0.035864	147.1
7.01	550.7	1.73	7.01	0.004122	0.039986	175.2
8.90	942.8	1.90	8.90	0.003442	0.043428	205.0
10.96	1115.0	2.06	10.96	0.002185	0.045613	240.3
13.19	1146.6	2.23	13.19	0.001996	0.047609	277.0
15.58	1140.0	2.39	15.58	0.002085	0.049694	313.5
18.13	1160.8	2.55	18.13	0.002241	0.051935	349.1
20.85	1212.8	2.72	20.85	0.002343	0.054278	384.2
23.74	1236.6	2.88	23.74	0.002379	0.056657	418.9
26.79	1353.1	3.05	26.79	0.002466	0.059122	453.1
30.00	1671.8	3.21	30.00	0.002376	0.061498	487.8

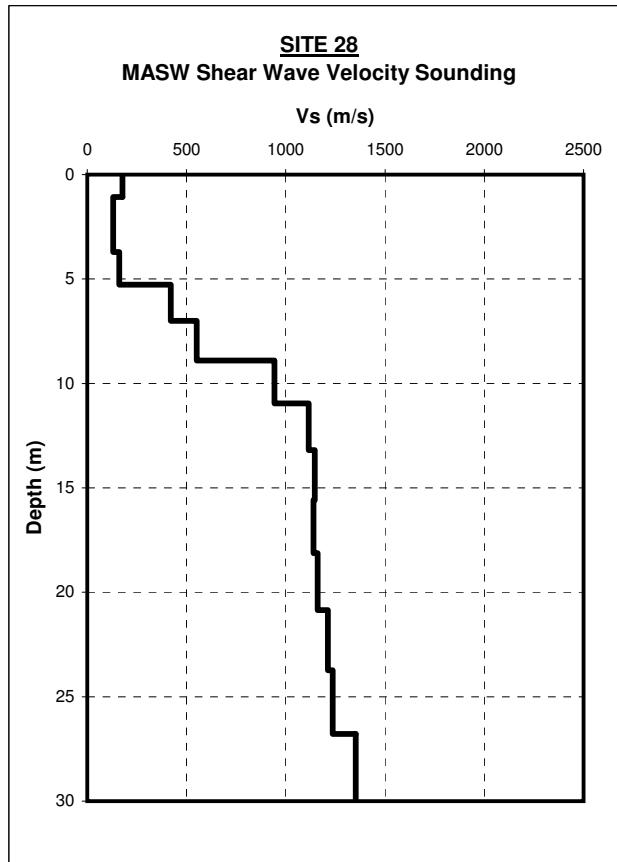
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	319665	4997492

Vs30 (m/s)	487.8
Class :	C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 5 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	93.3					
1.07	204.7	1.07	1.07	0.011483	0.011483	93.3
2.31	129.0	1.24	2.31	0.006040	0.017523	131.7
3.71	208.3	1.40	3.71	0.010863	0.028386	130.7
5.27	510.6	1.57	5.27	0.007517	0.035903	146.9
7.01	704.0	1.73	7.01	0.003390	0.039293	178.3
8.90	778.8	1.90	8.90	0.002693	0.041986	212.0
10.96	1383.9	2.06	10.96	0.002646	0.044631	245.6
13.19	1416.3	2.23	13.19	0.001608	0.046239	285.2
15.58	1599.9	2.39	15.58	0.001688	0.047927	325.0
18.13	1605.6	2.55	18.13	0.001597	0.049524	366.1
20.85	1614.0	2.72	20.85	0.001694	0.051218	407.1
23.74	1623.7	2.88	23.74	0.001787	0.053005	447.8
26.79	1648.4	3.05	26.79	0.001878	0.054883	488.1
30.00	2254.3	3.21	30.00	0.001950	0.056833	527.9

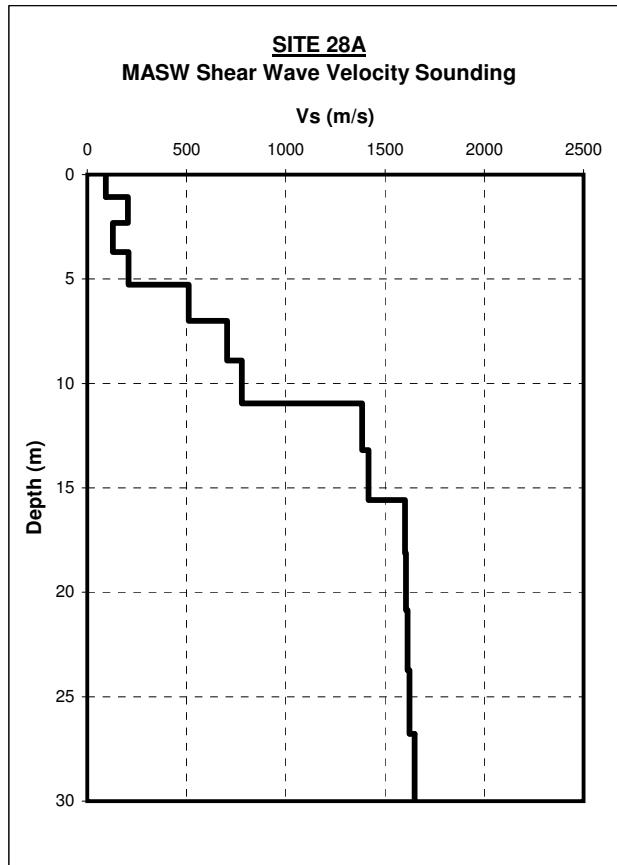
Location

Sounding: X (m) Y (m)
 MTM/Nad83 319414 4997499

Vs30 (m/s) **527.9**
Class : **C**

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 4-5 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



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Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	240.4					
1.07	184.6	1.07	1.07	0.004456	0.004456	240.4
2.31	372.4	1.24	2.31	0.006698	0.011154	206.9
3.71	529.1	1.40	3.71	0.003763	0.014917	248.6
5.27	519.6	1.57	5.27	0.002960	0.017877	295.1
7.01	867.3	1.73	7.01	0.003331	0.021208	330.3
8.90	1135.6	1.90	8.90	0.002186	0.023393	380.5
10.96	1164.9	2.06	10.96	0.001814	0.025208	434.8
13.19	1307.3	2.23	13.19	0.001910	0.027118	486.3
15.58	1339.0	2.39	15.58	0.001828	0.028946	538.1
18.13	1355.7	2.55	18.13	0.001908	0.030854	587.7
20.85	1389.3	2.72	20.85	0.002006	0.032860	634.6
23.74	1415.2	2.88	23.74	0.002076	0.034937	679.4
26.79	1632.7	3.05	26.79	0.002155	0.037092	722.2
30.00	1737.2	3.21	30.00	0.001969	0.039060	768.0

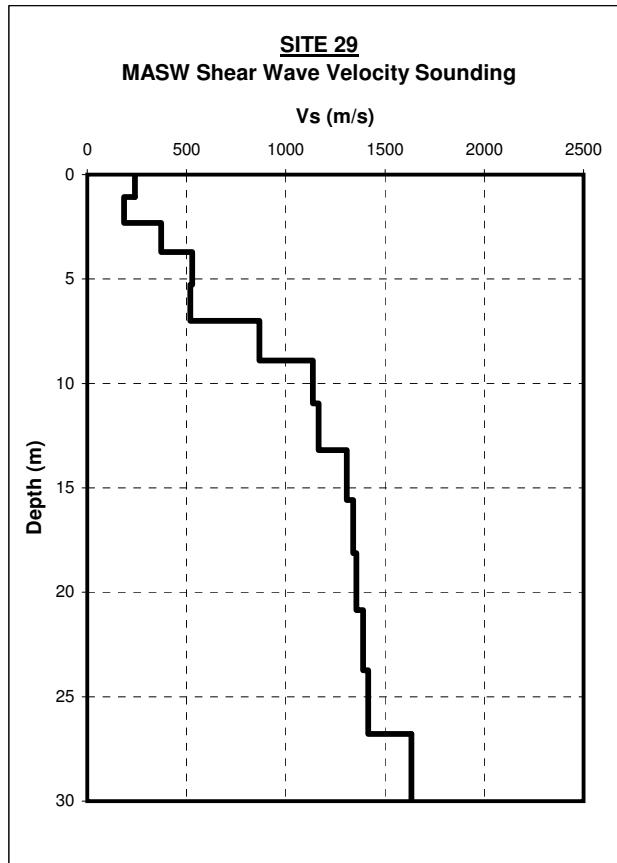
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	319828	5002096

Vs30 (m/s)	768.0
Class :	B

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The site class B can be considered only if there is less than 3 meters of overburden between the rock surface and the bottom of the mat foundation (cf. CNBC 2005 ; Commentary J ; Sentence 100).



Groupe ABS / Wind Energy Converters (WEC) / Saint-Valentin, Qc

Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	170.6					
1.07	240.6	1.07	1.07	0.006281	0.006281	170.6
2.31	233.5	1.24	2.31	0.005137	0.011418	202.1
3.71	1055.2	1.40	3.71	0.006000	0.017419	212.9
5.27	1300.4	1.57	5.27	0.001484	0.018903	279.0
7.01	1385.4	1.73	7.01	0.001331	0.020234	346.2
8.90	1480.9	1.90	8.90	0.001368	0.021602	412.1
10.96	1732.5	2.06	10.96	0.001391	0.022993	476.7
13.19	1684.0	2.23	13.19	0.001284	0.024278	543.2
15.58	1635.5	2.39	15.58	0.001419	0.025697	606.2
18.13	1601.8	2.55	18.13	0.001562	0.027259	665.2
20.85	1630.6	2.72	20.85	0.001698	0.028957	720.1
23.74	1699.2	2.88	23.74	0.001769	0.030726	772.5
26.79	1935.6	3.05	26.79	0.001795	0.032521	823.7
30.00	3419.6	3.21	30.00	0.001661	0.034181	877.7

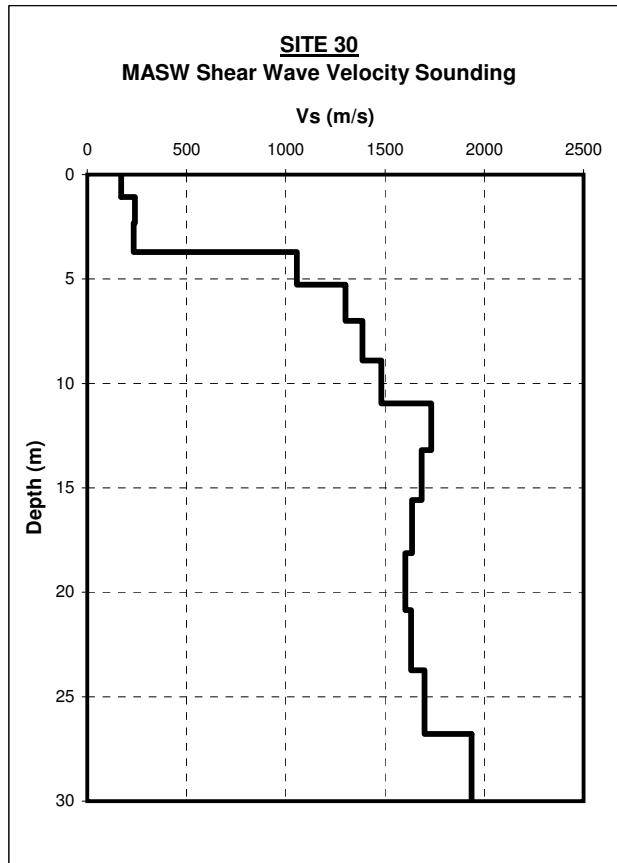
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	320091	5001646

Vs30 (m/s)	877.7
Class :	B

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The site class B can be considered only if there is less than 3 meters of overburden between the rock surface and the bottom of the mat foundation (cf. CNBC 2005 ; Commentary J ; Sentence 100). As 10BH-30 shows, the bedrock is at 6.5 meters deep, the class C should be considered.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	179.1					
1.07	108.4	1.07	1.07	0.005981	0.005981	179.1
2.31	135.5	1.24	2.31	0.011408	0.017389	132.7
3.71	159.1	1.40	3.71	0.010337	0.027726	133.8
5.27	213.7	1.57	5.27	0.009840	0.037566	140.4
7.01	327.1	1.73	7.01	0.008100	0.045666	153.4
8.90	433.4	1.90	8.90	0.005794	0.051461	173.0
10.96	782.7	2.06	10.96	0.004754	0.056215	195.0
13.19	1185.5	2.23	13.19	0.002843	0.059058	223.3
15.58	1261.5	2.39	15.58	0.002016	0.061074	255.0
18.13	1276.8	2.55	18.13	0.002025	0.063100	287.4
20.85	1316.2	2.72	20.85	0.002130	0.065230	319.7
23.74	1354.6	2.88	23.74	0.002192	0.067421	352.1
26.79	1391.3	3.05	26.79	0.002251	0.069673	384.5
30.00	1451.5	3.21	30.00	0.002310	0.071983	416.8

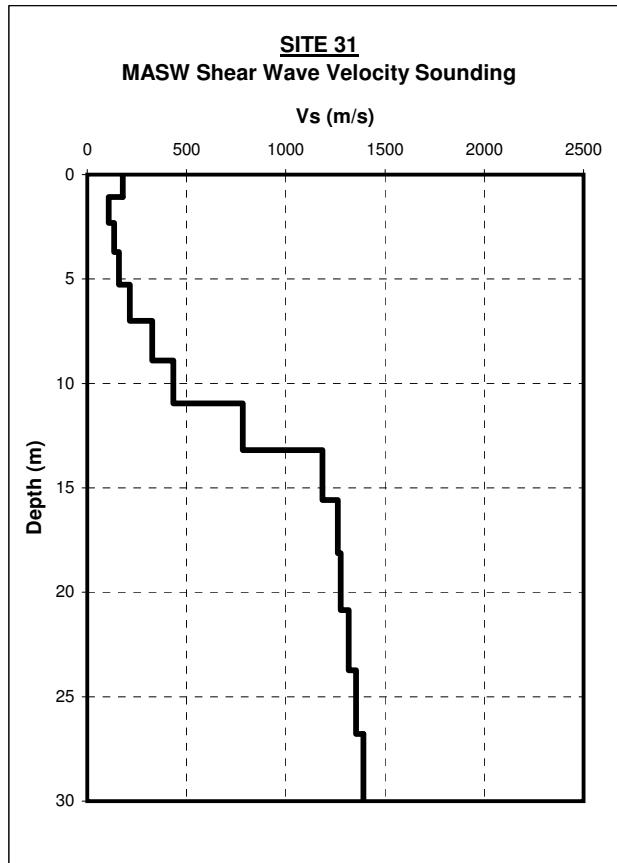
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	320095	4997479

Vs30 (m/s)	416.8
Class :	C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 4-7 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	154.1					
1.07	141.3	1.07	1.07	0.006953	0.006953	154.1
2.31	235.3	1.24	2.31	0.008751	0.015705	146.9
3.71	225.3	1.40	3.71	0.005956	0.021660	171.2
5.27	237.4	1.57	5.27	0.006949	0.028609	184.4
7.01	347.9	1.73	7.01	0.007290	0.035899	195.1
8.90	437.4	1.90	8.90	0.005448	0.041347	215.3
10.96	1201.9	2.06	10.96	0.004711	0.046058	238.0
13.19	1245.1	2.23	13.19	0.001851	0.047910	275.2
15.58	1271.9	2.39	15.58	0.001920	0.049830	312.6
18.13	1302.3	2.55	18.13	0.002009	0.051838	349.8
20.85	1327.2	2.72	20.85	0.002088	0.053927	386.7
23.74	1356.1	2.88	23.74	0.002173	0.056100	423.1
26.79	1384.4	3.05	26.79	0.002249	0.058349	459.1
30.00	1444.1	3.21	30.00	0.002322	0.060671	494.5

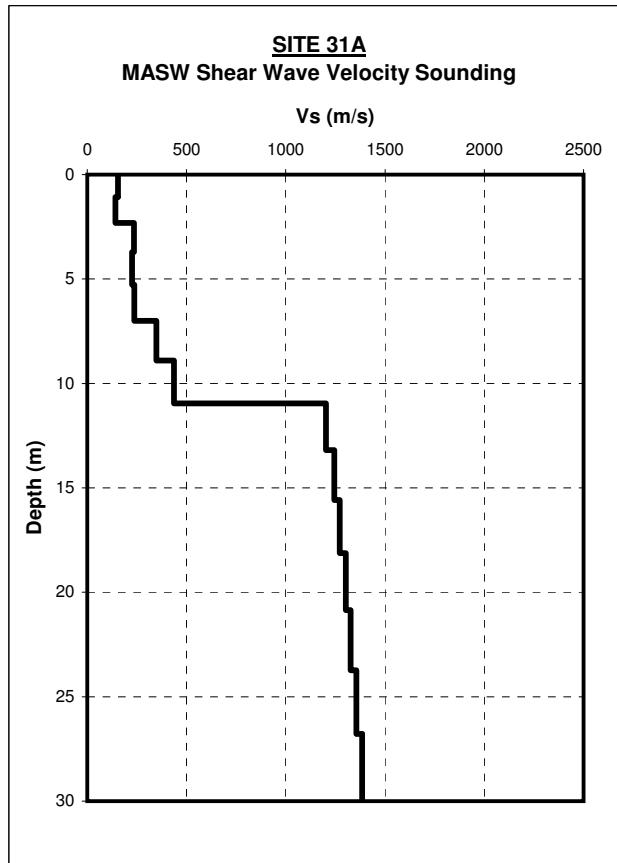
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	319926	4997484

Vs30 (m/s)	494.5
Class :	C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs values for the first 2-4 meters are abnormally low. This could be related to a soil with a liquefaction potential. An adequate geotechnical assessment should be made to ensure that the site class remains C, or be re-classified as a F.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	257.5506					
1.07	201.0363	1.07	1.07	0.004160	0.004160	257.6
2.31	273.5122	1.24	2.31	0.006149	0.010310	223.8
3.71	455.2144	1.40	3.71	0.005123	0.015432	240.3
5.27	770.9427	1.57	5.27	0.003440	0.018872	279.5
7.01	1383.861	1.73	7.01	0.002245	0.021117	331.7
8.90	1520.026	1.90	8.90	0.001370	0.022487	395.8
10.96	1539.346	2.06	10.96	0.001356	0.023842	459.7
13.19	1569.83	2.23	13.19	0.001446	0.025288	521.5
15.58	1593.021	2.39	15.58	0.001523	0.026811	581.0
18.13	1628.209	2.55	18.13	0.001604	0.028414	638.1
20.85	1656.517	2.72	20.85	0.001670	0.030085	693.1
23.74	1683.846	2.88	23.74	0.001741	0.031826	745.8
26.79	1707.615	3.05	26.79	0.001811	0.033637	796.3
30.00	1738.884	3.21	30.00	0.001882	0.035520	844.6

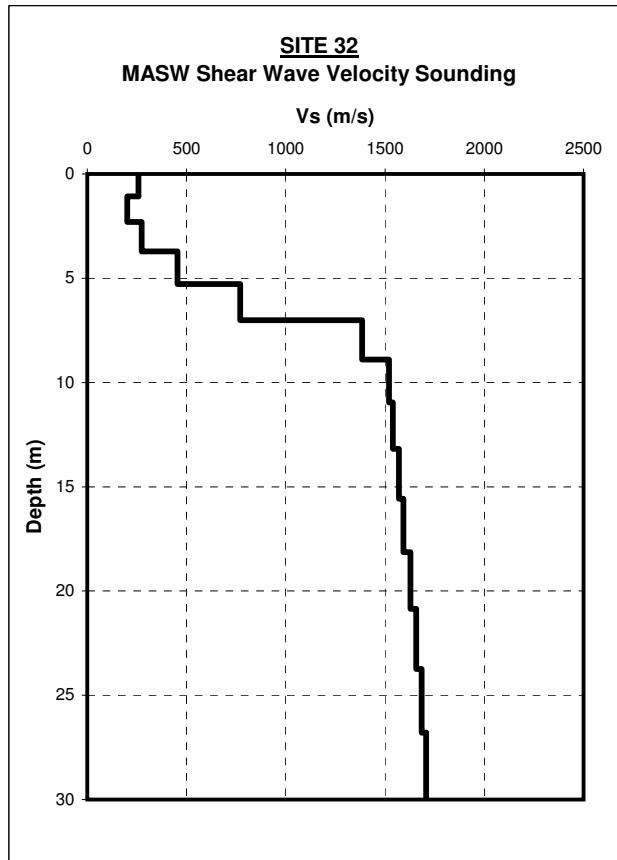
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	320241	5002214

Vs30 (m/s)	844.6
Class :	B

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The Vs sounding was resolved from the surface to 26 meters deep. The lower portion up to 30 meters deep was extrapolated for the calculation needs.
- 3- The site class B can be considered only if there is less than 3 meters of overburden between the rock surface and the bottom of the mat foundation (cf. CNBC 2005 ; Commentary J ; Sentence 100). As 10BH-32 shows, the bedrock is at 6.4 meters deep, the class C should be considered.



Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	230.8					
1.07	239.7	1.07	1.07	0.004642	0.004642	230.8
2.31	392.9	1.24	2.31	0.005159	0.009801	235.5
3.71	385.5	1.40	3.71	0.003566	0.013367	277.5
5.27	784.2	1.57	5.27	0.004062	0.017429	302.6
7.01	985.2	1.73	7.01	0.002207	0.019636	356.8
8.90	1226.4	1.90	8.90	0.001924	0.021560	412.8
10.96	1340.3	2.06	10.96	0.001680	0.023240	471.7
13.19	1378.3	2.23	13.19	0.001660	0.024901	529.6
15.58	1410.7	2.39	15.58	0.001734	0.026635	584.8
18.13	1526.8	2.55	18.13	0.001811	0.028446	637.4
20.85	1630.8	2.72	20.85	0.001781	0.030227	689.8
23.74	1737.0	2.88	23.74	0.001769	0.031996	741.8
26.79	2102.6	3.05	26.79	0.001756	0.033752	793.6
30.00	2288.3	3.21	30.00	0.001529	0.035280	850.3

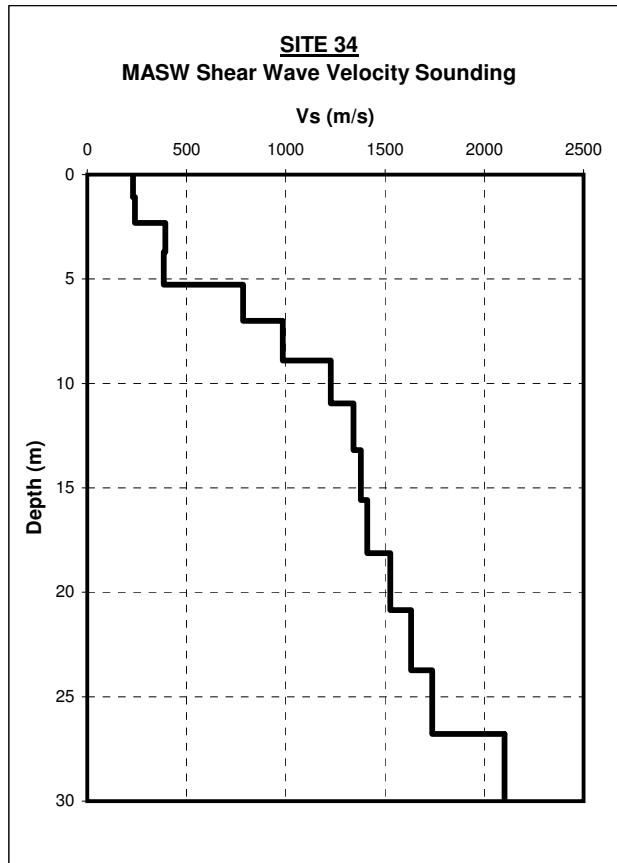
Location

Sounding: X (m) Y (m)
MTM/Nad83 319415 5002922

Vs30 (m/s) 850.3
Class : B

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The site class B can be considered only if there is less than 3 meters of overburden between the rock surface and the bottom of the mat foundation (cf. CNBC 2005 ; Commentary J ; Sentence 100). As 10BH-34 shows, the bedrock is at 5.1 meters deep, the class C should be considered.



Groupe ABS / Wind Energy Converters (WEC) / Saint-Valentin, Qc

Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	262.7					
1.07	237.5	1.07	1.07	0.004079	0.004079	262.7
2.31	334.5	1.24	2.31	0.005206	0.009285	248.6
3.71	308.7	1.40	3.71	0.004189	0.013473	275.3
5.27	382.7	1.57	5.27	0.005073	0.018546	284.4
7.01	554.0	1.73	7.01	0.004522	0.023068	303.7
8.90	706.1	1.90	8.90	0.003422	0.026490	336.0
10.96	1497.9	2.06	10.96	0.002918	0.029408	372.7
13.19	1513.0	2.23	13.19	0.001486	0.030894	426.8
15.58	1521.8	2.39	15.58	0.001580	0.032473	479.7
18.13	1525.0	2.55	18.13	0.001679	0.034152	530.9
20.85	1547.1	2.72	20.85	0.001783	0.035936	580.2
23.74	1569.3	2.88	23.74	0.001864	0.037800	627.9
26.79	1676.0	3.05	26.79	0.001943	0.039743	674.0
30.00	2150.4	3.21	30.00	0.001918	0.041661	720.1

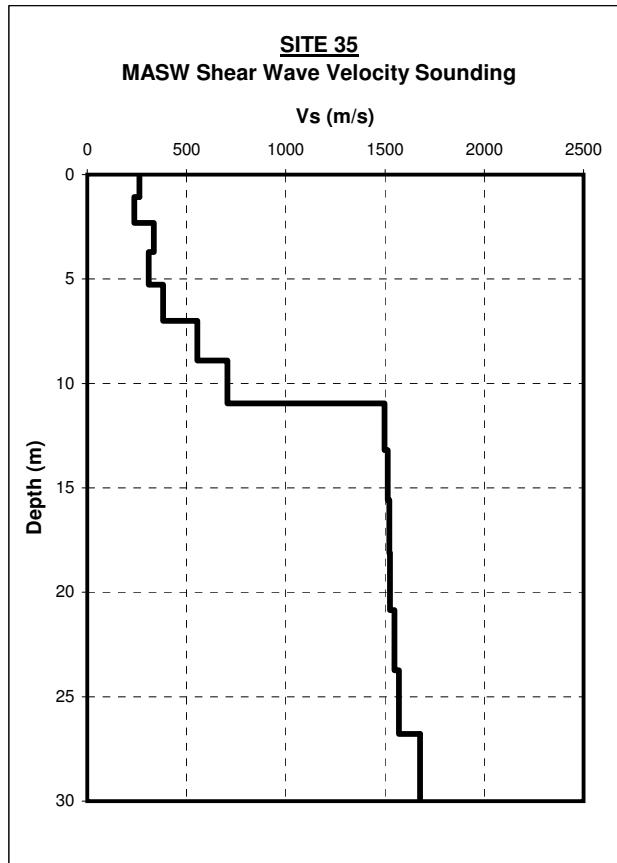
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	319169	5002673

Vs30 (m/s)	720.1
Class :	C

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.



Groupe ABS / Wind Energy Converters (WEC) / Saint-Valentin, Qc

Depth (m)	Vs (m/s)	Thickness (m)	Cumulated thickness (m)	Delay for med. Vs (s)	Cumulated delay (s)	Average Vs at given depth (m/s)
0.00	292.2					
1.07	203.0	1.07	1.07	0.003666	0.003666	292.2
2.31	204.9	1.24	2.31	0.006090	0.009756	236.5
3.71	805.7	1.40	3.71	0.006839	0.016595	223.5
5.27	1466.0	1.57	5.27	0.001944	0.018539	284.5
7.01	1584.1	1.73	7.01	0.001181	0.019720	355.3
8.90	1602.7	1.90	8.90	0.001197	0.020916	425.6
10.96	1662.1	2.06	10.96	0.001286	0.022202	493.7
13.19	1677.1	2.23	13.19	0.001339	0.023541	560.2
15.58	1677.1	2.39	15.58	0.001425	0.024966	623.9
18.13	1677.1	2.55	18.13	0.001523	0.026489	684.5
20.85	1832.1	2.72	20.85	0.001622	0.028111	741.8
23.74	1999.8	2.88	23.74	0.001574	0.029685	799.6
26.79	1999.8	3.05	26.79	0.001525	0.031210	858.2
30.00	1999.8	3.21	30.00	0.001607	0.032818	914.1

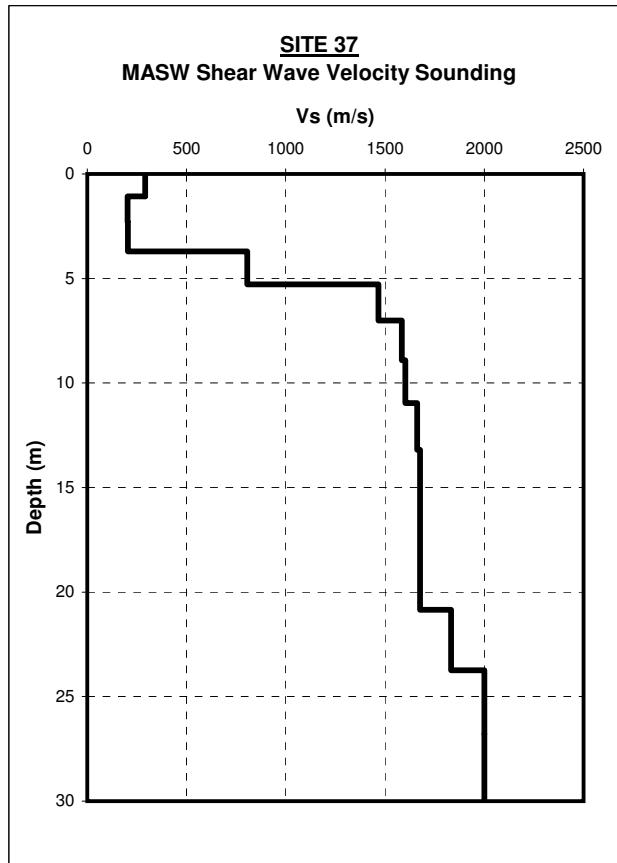
Location

Sounding:	X (m)	Y (m)
MTM/Nad83	318483	5001515

Vs30 (m/s)	914.1
Class :	B

NOTES :

- 1- The Vs values express estimated in-situ shear wave velocities; they were not corrected for the vertical effective overburden stress.
- 2- The site class B can be considered only if there is less than 3 meters of overburden between the rock surface and the bottom of the mat foundation (cf. CNBC 2005 ; Commentary J ; Sentence 100). As 10BH-37 shows, the bedrock is at 7.8 meters deep, the class C should be considered.



TRANSALTA CORPORATION

Geotechnical study – Construction of wind energy converters
Terrains located in the vicinity of the town of St-Valentin in Quebec

June 11, 2010
O/F : G1-09-1532

Appendix F

Rock samples photos



Photography 1 : 10BH-30



Photography 2 : 10BH-32



Photography 3 : 10BH-32



Photography 4 : 10BH-26

**Photography 5 : 10BH-26****Photography 6 : 10BH-16**

**Photography 7 : 10BH-16****Photography 8 : 10BH-05**

**Photography 9 : 10BH-05****Photography 10 : 10BH-09**



Photography 11 : 10BH-09



Photography 12 : 10BH-07



Photography 13 : 10BH-07



Photography 14 : 10BH-18



Photography 15 : 10BH-18



Photography 16 : 10BH-21

**Photography 17 : 10BH-21****Photography 18 : 10BH-20**

**Photography 19 : 10BH-29****Photography 20 : 10BH-29**



Photography 21 : 10BH-04



Photography 22 : 10BH-04



Photography 23 : 10BH-06



Photography 24 : 10BH-06

**Photography 25 : 10BH-08****Photography 26 : 10BH-11**



Photography 27 : 10BH-11



Photography 28 : 10BH-12



Photography 29 : 10BH-12



Photography 30 :10BH-14



Photography 31 : 10BH-14



Photography 32 : 10BH-25



Photography 33 : 10BH-25

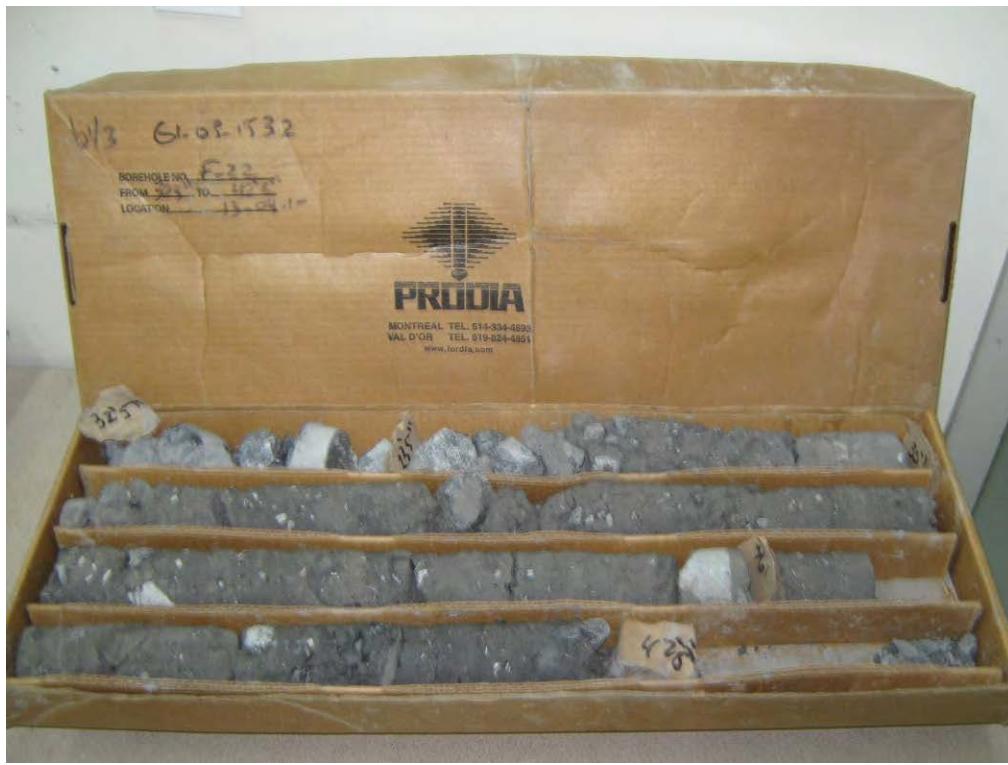


Photography 34 : 10BH-34

**Photography 35 : 10BH-34****Photography 36 : 10BH-35**



Photography 37 : 10BH-35



Photography 38 : 10BH-22



Photography 39 : 10BH-22



Photography 40 : 10BH-22

**Photography 41 : 10BH-31****Photography 42 : 10BH-31**

**Photography 43 : 10BH-31A****Photography 44 : 10BH-31A**

**Photography 45 : 10BH-28****Photography 46 : 10BH-28**



Photography 47 : 10BH-37



Photography 48 : 10BH-37

**Photography 49 : 10BH-27****Photography 50 : 10BH-27**

**Photography 51 : 10BH-23****Photography 52 :10BH-23**

TRANSALTA CORPORATION

Geotechnical study – Construction of wind energy converters
Terrains located in the vicinity of the town of St-Valentin in Quebec

June 11, 2010
O/F : G1-09-1532

Appendix G

Miscellaneous documents

TEST PIT AND BORING LOG REPORT EXPLANATORY NOTE

Soil description

Each layer of subsoil is described following the terminology listed below. Granular soil compactness is defined by the standard penetration index value "N" and cohesive soil consistency is defined by the undisturbed shear strength (Cu).

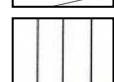
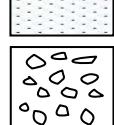
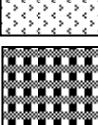
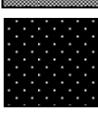
Depth, elevation and scale

The depth of the various stratigraphic layers is based upon the ground surface of the corresponding test pit or borehole. All elevations can be arbitrary or geodesic, the reference level always being indicated. The elevation and depth scale is always indicated in meters.

Soil classification

Clay	< 0,002 mm
Silt	0,002 - 0,08 mm
Sand	0,08 - 0,4 mm
	medium
	coarse
Gravel	1,0 - 5,0 mm
	fine
Cobbles	5,0 - 10,0 mm
	coarse
Boulders	10,0 - 80,0 mm
Cobbles	80,0 - 300,0 mm
Boulders	> 300,0 mm

Stratigraphy symbols

Clay		Rock	
Silt		Organic soil	
Sand		Concrete	
Gravel		Crushed stone	
Cobbles and Boulders		Asphalt	

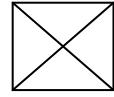
Terminology and proportions

" traces "	< 10%
" some "	10 - 20%
Adjective (sandy...)	20 - 35%
" and "	> 35%

Granular soils

Compactness	Standard penetration index " N " (blow counts / 300 mm)
Very loose	< 4
Loose	4 - 10
Compact	10 - 30
Dense	30 - 50
Very dense	> 50

Soil state

Disturbed		Intact	
-----------	--	--------	---

Cohesive soils

Consistency	Shear strength " Cu " (kPa)
Very soft	< 12
Soft	12 - 25
Firm	25 - 50
Stiff	50 - 100
Very stiff	100 - 200
Hard	> 200

ABBREVIATIONS

Samples	Split spoon	CF
	Thin wall tube (Shelby)	TM
	Helical auger	TR
	Coring drill	CR

In situ and

laboratory tests

Plasticity index	Hydrometer test	S
	Grain size analysis	G

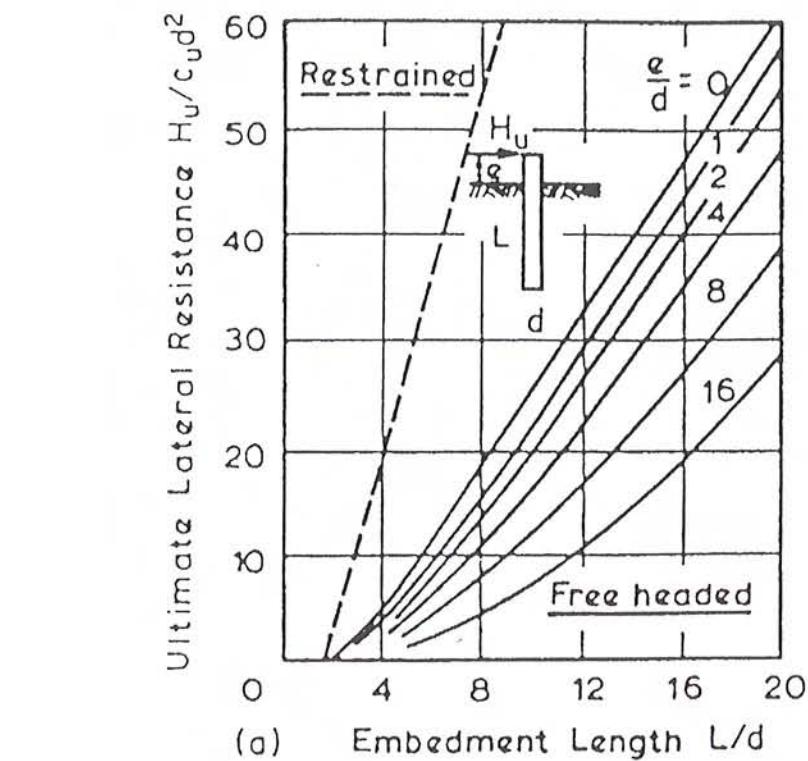
Liquid limit " W _L "	Plasticity index	IP	Water content	W
	Liquid limit	W _L	Unit weight	γ
	Plastic limit	W _P	Consolidation	C

Sensitivity	Atterberg limit	A	Swedish fall cone	CS
S _t = Cu/Cu _R			Hydraulic conductivity	K
			Refusal	R

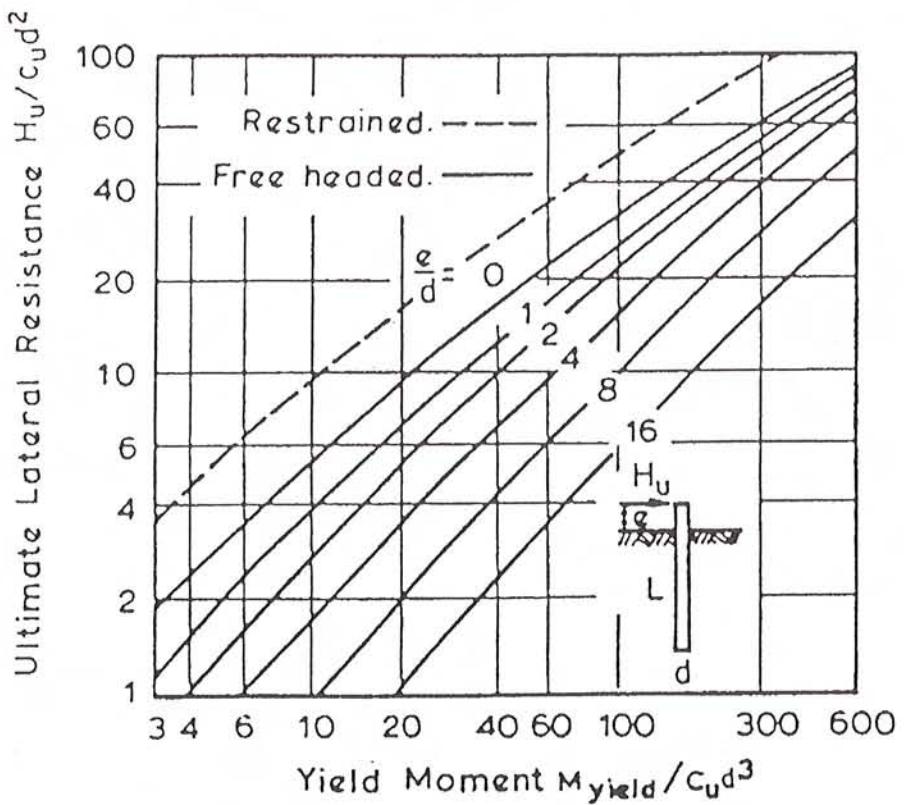
Low	< 30%	< 2		
Medium	30 - 50%	2 - 4		
High	> 50%	4 - 8		

8 - 16

> 16

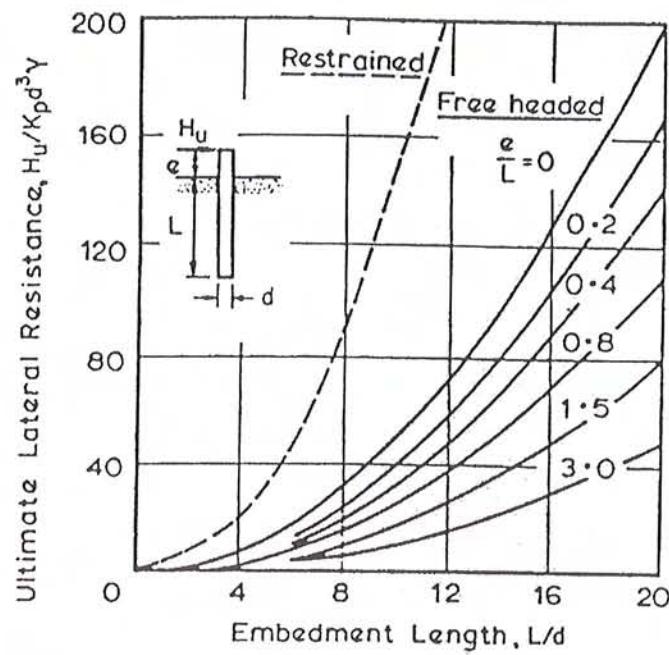


a) Short Pile

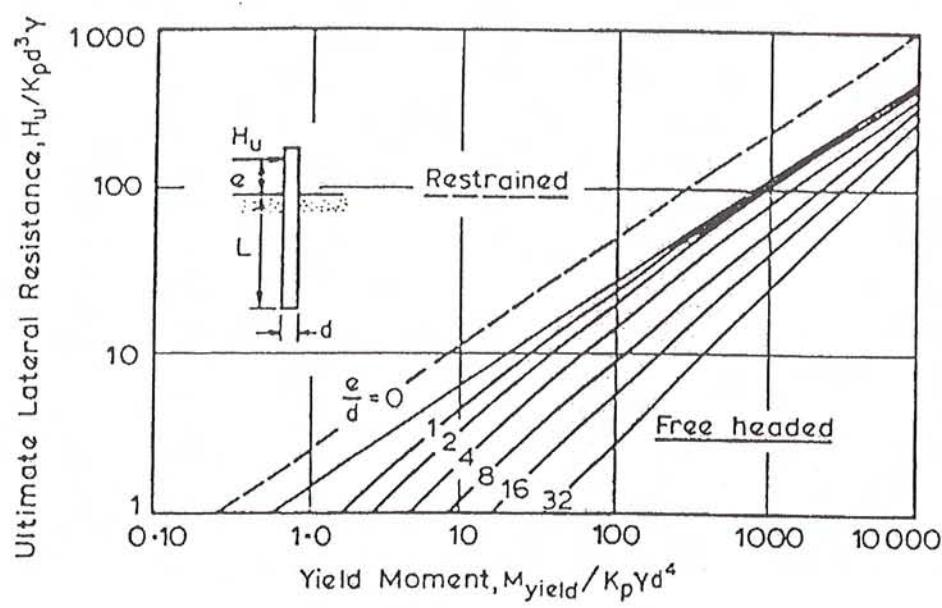


b) Long Pile

FIGURE 18.10 Ultimate lateral resistance of piles in cohesive soils (after Broms, 1964a)



a) Short Pile

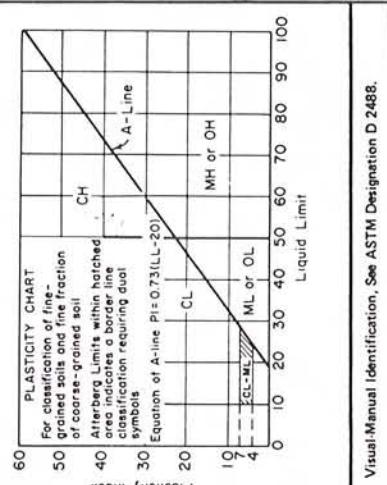


b) Long Pile

FIGURE 18.9 Ultimate lateral resistance of piles in cohesionless soils (after Broms, 1964b)

Figure 37-1 Unified soil classification system.

MAJOR DIVISIONS	GROUP SYMBOLS	TYPICAL NAMES	CLASSIFICATION CRITERIA					
			SILTS AND CLAYS	SANDS	GRAVELS	FINE-GRAINED SOILS	COURSE-GRAINED SOILS	50% or more passing 0.075 mm (No. 200) sieve
	GW	Well graded gravels and gravel sand mixtures, little or no fines						
	GP	Poorly graded gravels and gravel sand mixtures, little or no fines						
	GM	Silty gravels, gravel sand silt mixtures						
	GC	Clayey gravels, gravel sand clay mixtures						
	SW	Well graded sands and gravelly sands, little or no fines						
	SP	Poorly graded sands and gravelly sands, little or no fines						
	SM	Silty sands, sand-silt mixtures						
	SC	Clayey sands, sand-clay mixture						
	ML	Inorganic silts, very fine sands, rock flour, silty or clayey fine sands						
	CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays						
	OL	Organic silts and organic silty clays of low plasticity						
	MH	Inorganic silts, micaceous or diatomaceous fine sands or silts, elastic silts						
	CH	Inorganic clays of high plasticity, fat clays						
	OH	Organic clays of medium to high plasticity						
	PT	Pearl, muck and other highly organic soils						



Visual Manual Identification, See ASTM Designation D 2488.

Fundamentdatenblatt
für geotechnische Nachweise
Foundation data sheet
for geotechnical calculations**TÜV NORD**
21. NOV. 2006Reviewed by comparing calculation
~~0000169412/8 E 1~~

Reviewed

Hamburg,

Chr. Hering
Expert of
TÜVNORD SysTec GmbH & Co.KGTurmtyp: **E-82/BF/83/17/01**
tower type:Typenklasse: Windzone 4, GK I (DIBt-Richtlinie)
type class: WTGS class II A (IEC-/NVN-/EN-Richtlinie)Fundamenttyp: **Tiefgründung - Kreisringfundament**
mit Auftrieb - Ø 15,60m – 36 Pfähle
Auftragsnr.: 2790-06 vom 23.05.2006foundation type: **pile foundation – circular ringfoundation**
with buoyancy - Ø 15,60m – 36 piles
order number: 2790-06 dated 23.05.2006Datum: 04.09.2006
date: Rev. 1.1 / 31.10.2006 OLENERCON GmbH
Dreekamp 5
D – 26605 Aurich / Germany
www.enercon.de

Author: Dipl.-Ing. O. Lehmann

Approved: Dipl.-Ing. (FH) M. Schacknies

*Oberingenieur**M. Schacknies*

Document information:		Translator / date:	Revisor / date:	Reference:
Author/ date:	OL / 04.09.2006			
Department:	WRD-K			
Approved / date:	MS / 04.09.2006			
Revision / date:	1.1 / 31.10.2006			
				OL / 31.10.2006
				WRD-04-FDB_E-82_BF_83_17_01_TGMa_Rev1_1-ger.doc

- **Pfahlkräfte für geotechnische Nachweise**
Loads of the pile for geotechnical calculations

maximale Druckkraft maximum compressive force	- 1.275 kN
maximale Zugkraft maximum tensile force	324 kN

alle Lasten mit Teilsicherheitsbeiwert $\gamma_F = 1,0$
 all loads with partial safety factor $\gamma_F = 1,0$

- **Pfahlgeometrie / pile geometry**

Pfahllänge length of the piles		16,00 m
Pfahlanzahl number of piles		Pfahlneigung pile inclination
Total	24	4:1 nach außen 4:1 outwards
	12	10:1 nach innen 10:1 inwards
Pfahlquerschnitt pile cross section	Quadrat quadrat	45 cm/45 cm

Die Pfähle müssen wegen der Zugbeanspruchung mindestens 5,00 m in den ausreichend tragfähigen Baugrund einbinden.

In consequence of tension in the piles, they must bind 5,00 m into the better ground.

- **Drehfedersteifigkeit / rocking spring stiffness**

Für die Fundamenteinspannung zwischen Fundament und Baugrund ist eine Mindestdrehfedersteifigkeit von $k_{\phi,dyn} = 100.000 \text{ MNm/rad}$ (**dynamische Bodenkennwerte**) bzw.

$k_{\phi,stat} = 25.000 \text{ MNm/rad}$ (**statische Bodenkennwerte**) für das Gesamtssystem (Turm und Gründung inkl. Pfahlsystem) einzuhalten.

Eine dynamische Mindestdrehfedersteifigkeit des Pfahlsystems von $k_{\phi,dyn} = 300.000 \text{ MNm/rad}$ (**dynamische Bodenkennwerte**) ist einzuhalten.

The minimum value of rocking spring stiffness for clamping between foundation and soil must be $k_{\phi,dyn} = 100.000 \text{ MNm/rad}$ (dynamic soil parameter) as well as $k_{\phi,stat} = 25.000 \text{ MNm/rad}$ (static soil parameter) for the total system (tower and foundation incl. piles system).

The minimum value of rocking spring stiffness for the piles system must be $k_{\phi,dyn} = 300.000 \text{ MNm/rad}$ (dynamic soil parameter).

- **Zulässige Schieflage / permissible tilting**

Maximal zulässige Schieflage infolge Baugrundsetzung in 20 Jahren bezogen auf den Pfahlkreisdurchmesser.

Maximum allowed tilting due to settlement of the foundation soil in 20 years relating to the pile circle diameter.

$\Delta s \leq 40 \text{ mm}$


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- **Lastangaben für den inneren Tragsicherheitsnachweis der Pfähle**
Loads for the dimensioning for the internal force of the piles

maximale Druckkraft <i>maximum compressive force</i> (Pfahloberkante / top of pile)	- 1.577 kN	Einspannmoment in Platte <i>Clamping moment into plate</i>	40,0 kNm
maximale Zugkraft <i>maximum tensile force</i> (Pfahloberkante / top of pile)	440 kN	Max. Moment im Verlauf des Pfahls <i>Max. moment in middle of the pile</i>	27,0 kNm

alle Lasten mit Teilsicherheitsbeiwerten
all loads with partial safety factors

Folgende seitliche Bettung des Pfahls ist einzuhalten (Tiefe bezogen auf UK Fundament)..
The following bedding modulus of the pile has to be considered (depth relates to the bottom of the foundation).

Tiefe depth	E_s, stat
0,00 m – 4,50 m	0,0 MN/m ²
4,50 m – 7,50 m	1,0 MN/m ²
7,50 m – 10,50 m	2,0 MN/m ²
10,50 m – 16,00 m	4,0 MN/m ²

- **Lasten an der Fundamentunterkante**

(inkl. Fundamenteigengewicht $\gamma = 25 \text{ kN/m}^3$ und Bodenauflast $\gamma = 18 \text{ kN/m}^3$ im Trockenzustand)
Loads at the bottom of foundation
(incl. foundation dead weight $\gamma = 25 \text{ kN/m}^3$ and soil weight $\gamma = 18 \text{ kN/m}^3$ for dry conditions)

Lastfall <i>load case</i>	F_{xy} [kN]	F_z [kN]	M_{xy} [kNm]	M_z [kNm]
DLC 1.0	570	-13.787 mit Auftrieb / with buoyancy	37.024	1.750
		-19.425 ohne Auftrieb / without buoyancy		
DLC 6.2	850	-13.787 mit Auftrieb / with buoyancy	61.370	1.860
		-19.425 ohne Auftrieb / without buoyancy		

alle Lasten mit Teilsicherheitsbeiwert $\gamma_F = 1,0$
all loads with partial safety factor $\gamma_F = 1,0$

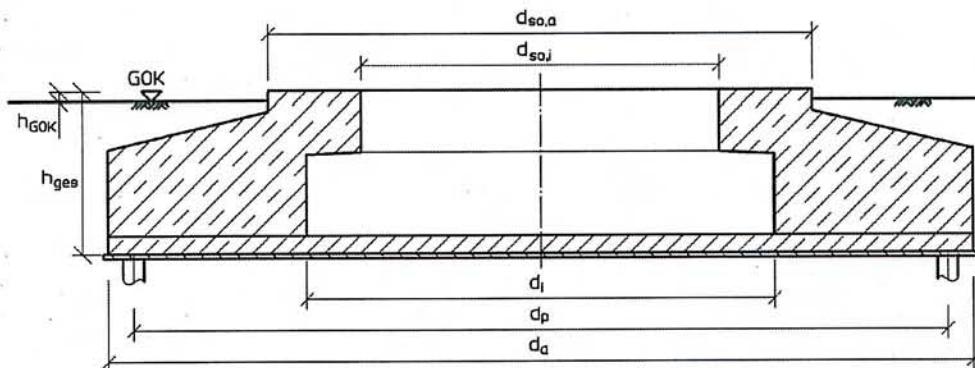
Lastfall <i>load case</i> ($\gamma_{\text{aero}}/\gamma_{\text{masse}}$)	F_{xy} [kN]	F_z [kN]	M_{xy} [kN]	M_z [kNm]
DLC 6.2 (1.10/1.35) ohne Auftrieb <i>without buoyancy</i>	1.070	-25.934	68.274	1.640
DLC 6.2 (1.10/1.00) mit Auftrieb <i>with buoyancy</i>	1.070	-13.787	68.274	1.640

alle Lasten mit Teilsicherheitsbeiwerten
all loads with partial safety factors

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Department:	MS / 04.09.2006	Reference:	Z. NOV. 2006
Approved / date:	1.1 / 31.10.2006		
Revision / date:			

Fundamentgeometrie / geometry of foundation

Außendurchmesser <i>outer diameter</i>	da	15,60 m
Innendurchmesser <i>inner diameter</i>	di	6,90 m
Sockeldurchmesser, außen <i>base diameter, outside</i>	dso _a	8,70 m
Sockeldurchmesser, innen <i>base diameter, outside</i>	dso _i	4,80 m
Pfahlkreisdurchmesser <i>diameter of the pile circle</i>	dp	14,80 m
Fundamenthöhe <i>foundation height</i>	hges	3,20 m
Differenz Fundamentoberkante - GOK <i>difference top of foundation – top ground surface</i>	hgok	0,20 m
Betongüte und Volumen <i>Concrete and quantity</i>	C 30/37	440 m ³
Betonstahl und Gewicht <i>Concrete steel and weight</i>	BSt 500 S (A)	40,8 t


Bemerkungen / remarks

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TÜV NORD
21. NOV. 2006

Fundamentdatenblatt
für geotechnische Nachweise
Foundation data sheet
for geotechnical calculations

Turmtyp: **E-82/BF/83/17/01**
tower type:

Typenklasse: Windzone 4, GK 1 (DIBt-Richtlinie)
type class: WTGS class II A (IEC-/NVN-/EN-Richtlinie)

Fundamenttyp: **Flachgründung - Kreisringfundament**
mit Auftrieb - Ø 16,80m
Auftragsnr.: 2790-06 vom 16.05.2006

foundation type: **shallow foundation – circular ringfoundation**
with buoyancy - Ø 16,80m
order number: 2790-06 dated 16.05.2006

Datum: 04.09.2006
date: Rev. 1.0

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Reviewed by comparing calculation

Reviewed

Hamburg

Chr. Hering

Expert of

TÜVNORD SysTec GmbH & Co.KG

TÜV NORD

24. NOV. 2006

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Oliver Lehmann

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- **Lasten an der Fundamentunterkante für geotechnische Nachweise**
(inkl. Eigengewicht Fundament und Bodenauflast $\gamma = 18 \text{ kN/m}^3$ im Trockenzustand)
Loads at the bottom of foundation for geotechnical calculations
(incl. dead weight foundation and soil weight $\gamma = 18 \text{ kN/m}^3$ for dry conditions)

Lastfall load case	F_{xy} [kN]	F_z [kN]	M_{xy} [kNm]	M_z [kNm]
DLC 1.0	570	-13.911 mit Auftrieb / with buoyancy	36.825	1.750
		-19.674 ohne Auftrieb / without buoyancy		
DLC 6.2	850	-13.911 mit Auftrieb / with buoyancy	61.073	1.860
		-19.674 ohne Auftrieb / without buoyancy		

alle Lasten mit Teilsicherheitsbeiwert $\gamma_F = 1,0$
all loads with partial safety factor $\gamma_F = 1,0$

- **Aufzunehmende Bodenpressung / minimum required bearing pressure**

Der anstehende Baugrund muss mindestens eine Bodenpressung von $\sigma = 242 \text{ kN/m}^2$ aufnehmen können.

Minimum required bearing pressure is $\sigma = 242 \text{ kN/m}^2$.

- **Drehfedersteifigkeit / rocking spring stiffness**

Für die elastische Fundamenteinspannung zwischen Fundament und Baugrund sind folgende Bodenkennwerte einzuhalten.

The following soil parameters of rocking spring stiffness for clamping between foundation and soil must be meet.

$$k_{\varphi, \text{dyn}} = 100.000 \text{ MNm/rad}$$

Nichtbindiger Boden / cohesionless soil: $E_{\text{oed}, \text{dyn}} = 180 \text{ MN/m}^2 (\nu = 0,35)$

$$k_{\varphi, \text{stat}} = 25.000 \text{ MNm/rad}$$

Nichtbindiger Boden / cohesionless soil: $E_{\text{oed}, \text{stat}} = 45 \text{ MN/m}^2 (\nu = 0,35)$

Die erforderlichen dynamischen Steifemodule ($E_{\text{oed}, \text{dyn}}$) bzw. statischen Steifemodule ($E_{\text{oed}, \text{stat}}$) ergeben sich in Abhängigkeit von Fundamentgeometrie und Querdehnzahl.

The minimum values of dynamic modulus of stiffness ($E_{\text{oed}, \text{dyn}}$) respectively of static modulus of stiffness ($E_{\text{oed}, \text{stat}}$) are calculated in dependence on foundation geometry and Poisson's ratio.

Für Kreisfundamente gilt:

For circular foundations:

$$k_{\varphi} = \frac{8 \cdot G \cdot r^3}{3 \cdot (1 - \nu)}$$

G = Schubmodul / shear modulus

r = Radius / radius

$$E_{\text{oed}} = k_{\varphi} \cdot \frac{3}{4} \cdot \frac{1}{r^3} \cdot \frac{(1 + \nu) \cdot (1 - \nu)^2}{1 - \nu - 2 \cdot \nu^2}$$

ν = Querdehnzahl / Poisson's ratio

- **Zulässige Schiefstellung / permissible tilting**

Maximal zulässige Schiefstellung infolge Baugrundsetzung in 20 Jahren bezogen auf den Fundamentdurchmesser.

Maximum allowed tilting due to settlement of the foundation soil in 20 years relating to the foundation diameter.

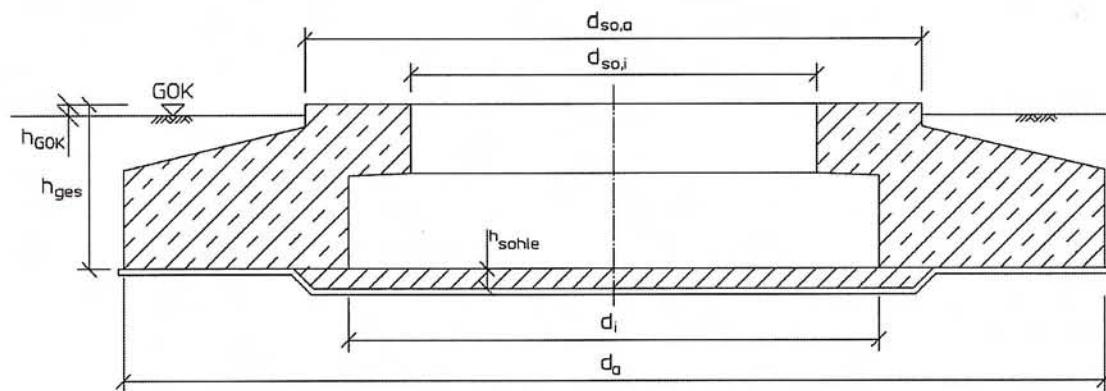
$\Delta s \leq 40 \text{ mm}$

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TEV NORD
24. NOV. 2006

Fundamentgeometrie
geometry of foundation

Außendurchmesser <i>outer diameter</i>	da	16,80 m
Innendurchmesser <i>inner diameter</i>	di	6,90 m
Sockeldurchmesser, außen <i>base diameter, outside</i>	d _{so,a}	8,70 m
Sockeldurchmesser, innen <i>base diameter, outside</i>	d _{so,i}	4,80 m
Fundamenthöhe <i>foundation height</i>	h _{ges}	2,85 m
Differenz Fundamentoberkante - GOK <i>difference top of foundation – top ground surface</i>	hgok	0,20 m
Fundamentsohle <i>foundation sole plate</i>	h _{sohle}	0,30 m
Betongüte und Volumen (Fundament) <i>Concrete and quantity (foundation)</i>	C 30/37	426 m ³
Betonstahl und Gewicht (Fundament) <i>Concrete steel and weight (foundation)</i>	BSt 500 S (A)	35,8 t
Betongüte und Volumen (Fundamentsohle) <i>Concrete and quantity (foundation sole plate)</i>	C 25/30 WU	21 m ³
Betonstahl und Gewicht (Fundamentsohle) <i>Concrete steel and weight (foundation sole plate)</i>	BSt 500 S (A)	1,6 t


Bemerkungen / remarks

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TÜV NORD
 24. NOV. 2006

Fundamentdatenblatt

für geotechnische Nachweise

Foundation data sheet

for geotechnical calculations

Turmtyp: **E-82/BF/83/17/01**
tower type:

Typenklasse: Windzone 4, GK I (DIBt-Richtlinie)
type class: WTGS class II A (IEC-/NVN-/EN-Richtlinie)

Fundamenttyp: **Flachgründung - Kreisringfundament**
ohne Auftrieb - Ø 14,20m
Auftragsnr.: 2790-06 vom 19.05.2006

foundation type: **shallow foundation - circular ringfoundation**
without buoyancy - Ø 14,20m
order number: 2790-06 dated 19.05.2006

Datum: 04.09.2006
date: Rev. 1.0

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Reviewed by comparing calculation

Reviewed

Hamburg

Chr. Hering

Expert of

TÜVNORD SysTec GmbH & Co.KG

TÜV NORD
28. NOV. 2006

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- **Lasten an der Fundamentunterkante für geotechnische Nachweise**
(inkl. Eigengewicht Fundament und Bodenauflast $\gamma = 18 \text{ kN/m}^3$ im Trockenzustand)
Loads at the bottom of foundation for geotechnical calculations
(incl. dead weight foundation and soil weight $\gamma = 18 \text{ kN/m}^3$ for dry conditions)

Lastfall load case	F_{xy} [kN]	F_z [kN]	M_{xy} [kNm]	M_z [kNm]
DLC 1.0	570	-15.772	36.825	1.750
DLC 6.2	850	-15.772	61.073	1.860

alle Lasten mit Teilsicherheitsbeiwert $\gamma_F = 1,0$

all loads with partial safety factor $\gamma_F = 1,0$

- **Aufzunehmende Bodenpressung / minimum required bearing pressure**
Der anstehende Baugrund muss mindestens eine Bodenpressung von $\sigma = 412 \text{ kN/m}^2$ aufnehmen können.
Minimum required bearing pressure is $\sigma = 412 \text{ kN/m}^2$.

- **Drehfedersteifigkeit / rocking spring stiffness**

Für die elastische Fundamenteinspannung zwischen Fundament und Baugrund sind folgende Bodenkennwerte einzuhalten.

The following soil parameters of rocking spring stiffness for clamping between foundation and soil must be meet.

Nichtbindiger Boden / cohesionless soil:	$k_{\phi,\text{dyn}} \geq 100.000 \text{ MNm/rad}$
	$E_{\text{oed},\text{dyn}} = 260 \text{ MN/m}^2 (\nu = 0,30)$

Nichtbindiger Boden / cohesionless soil:	$k_{\phi,\text{stat}} \geq 25.000 \text{ MNm/rad}$
	$E_{\text{oed},\text{stat}} = 65 \text{ MN/m}^2 (\nu = 0,30)$

Die erforderlichen dynamischen Steifemodule ($E_{\text{oed},\text{dyn}}$) bzw. statischen Steifemodule ($E_{\text{oed},\text{stat}}$) ergeben sich in Abhängigkeit von Fundamentgeometrie und Querdehnzahl.

The minimum values of dynamic modulus of stiffness ($E_{\text{oed},\text{dyn}}$) respectively of static modulus of stiffness ($E_{\text{oed},\text{stat}}$) are calculated in dependence on foundation geometry and Poisson's ratio.

Für Kreisfundamente gilt:
For circular foundations:

$$k_\phi = \frac{8 \cdot G \cdot r^3}{3 \cdot (1-\nu)}$$

$$E_{\text{oed}} = k_\phi \cdot \frac{3}{4} \cdot \frac{1}{r^3} \cdot \frac{(1+\nu) \cdot (1-\nu)^2}{1-\nu-2 \cdot \nu^2}$$

G = Schubmodul / shear modulus

r = Radius / radius

ν = Querdehnzahl / Poisson's ratio

- **Zulässige Schiefstellung / permissible tilting**

Maximal zulässige Schiefstellung infolge Baugrundsetzung in 20 Jahren bezogen auf den Fundamentdurchmesser.

Maximum allowed tilting due to settlement of the foundation soil in 20 years relating to the foundation diameter.

$\Delta s \leq 40 \text{ mm}$

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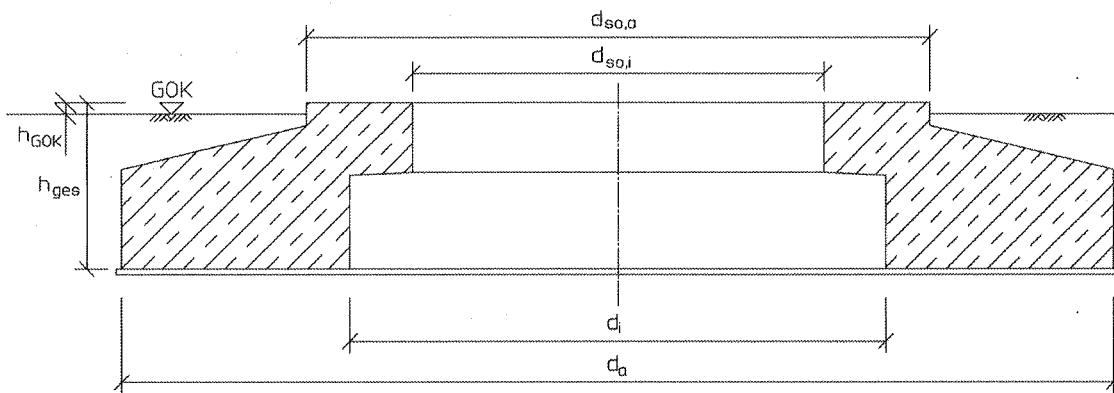
Reference:

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28. NOV. 2006

Fundamentgeometrie
geometry of foundation

Außendurchmesser <i>outer diameter</i>	da	14,20 m
Innendurchmesser <i>inner diameter</i>	di	6,90 m
Sockeldurchmesser, außen <i>base diameter, outside</i>	dso,a	8,70 m
Sockeldurchmesser, innen <i>base diameter, outside</i>	dso,i	4,80 m
Fundamenthöhe <i>foundation height</i>	hges	2,85 m
Differenz Fundamentoberkante - GOK <i>difference top of foundation – top ground surface</i>	hgok	0,20 m
Betongüte und Volumen (Fundament) <i>Concrete and quantity (foundation)</i>	C 30/37	300 m ³
Betonstahl und Gewicht (Fundament) <i>Concrete steel and weight (foundation)</i>	BSt 500 S (A)	30,4


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